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THE ENGINEER'S
COMMON-PLACE BOOK
OF
PRACTICAL REFERENCE.

—
THIRD EDITION, IMPROVED.
—

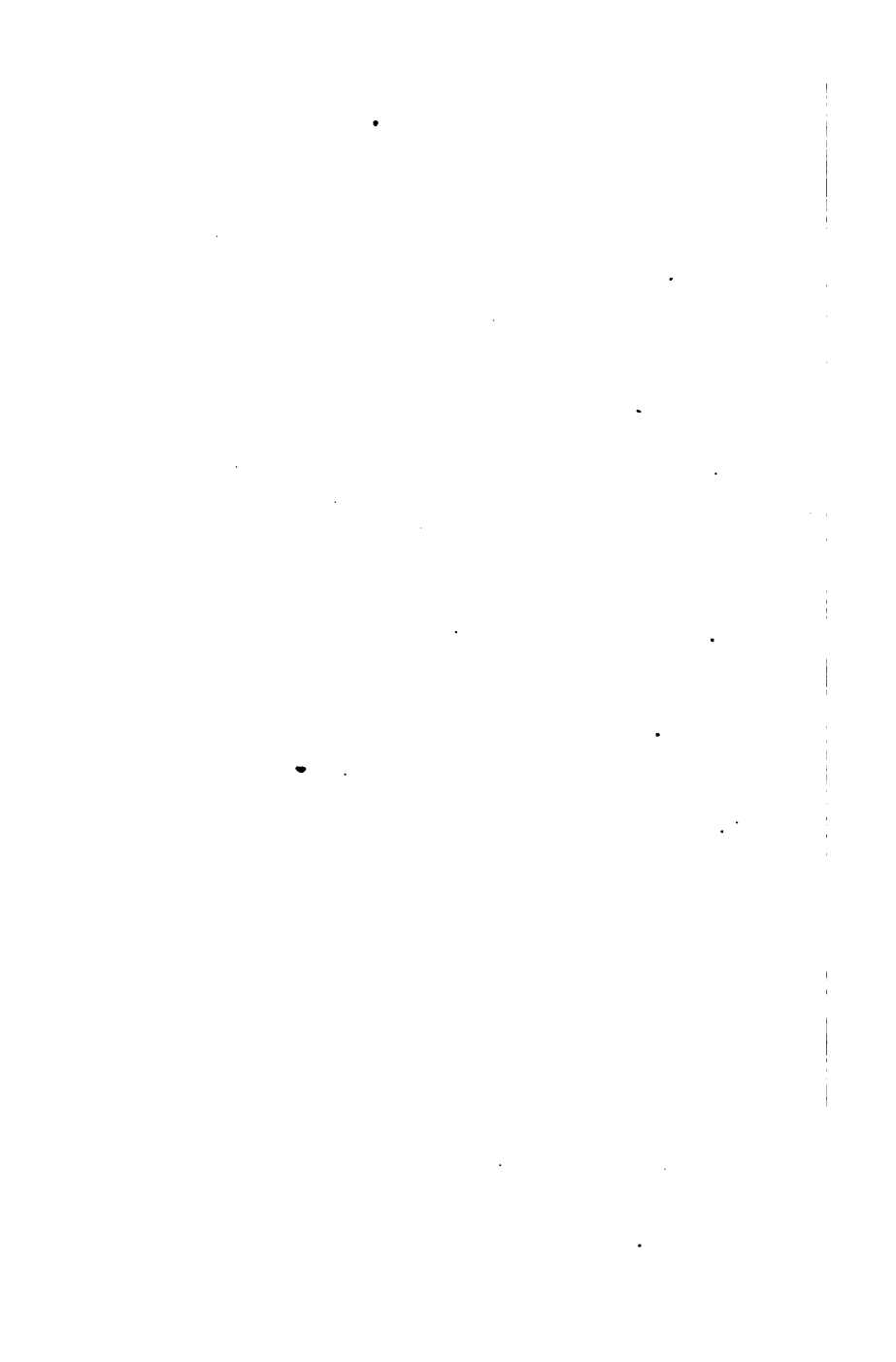
BY WILLIAM TEMPLETON.
—

With Four Lithographic Illustrations.

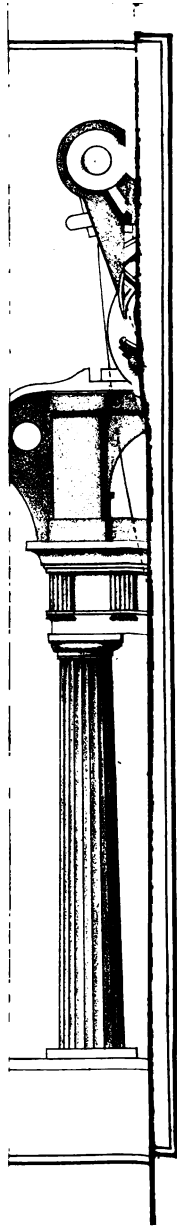
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THE ENGINEER'S
COMMON-PLACE BOOK
OF
PRACTICAL REFERENCE,
CONSISTING OF
PRACTICAL RULES AND TABLES
FAMILIARLY ADAPTED TO
FACTORY AND MARINE STEAM-ENGINES.

TO WHICH IS ADDED,
EXTENSIVE TABLES OF CIRCUMFERENCES, SQUARES, CUBES, AND AREAS
OF CIRCLES; SQUARE AND CUBE ROOTS OF NUMBERS, WITH
THEIR DIFFERENCES, FOR FACILITATING
FRACTIONAL CALCULATIONS;
SUPERFICIES AND SOLIDITIES OF SPHERES, &c., &c., WITH OTHER
USEFUL TABLES, EQUALLY ADAPTED TO PRACTICAL PURPOSES.

BY WILLIAM TEMPLETON.

*Author of "The Millwright and Engineer's Pocket Companion," and
"Locomotive Engine Popularly Explained."*

THIRD EDITION, IMPROVED.

WITH LITHOGRAPHIC ILLUSTRATIONS.



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PREFACE.

WHEN a new edition of any work is presented to the public, it is generally expected to bring along with it some new claim to public estimation, without which its merits could not be recognised, and, consequently, because of retaining the old title, it would, in all probability, be deemed nothing more than a mere reprint of the original work.

In compliance with this feeling, the author of the Common-place Book begs to submit this edition to the notice of the public, the work having not only been diligently revised, but almost entirely re-written, and matter of much importance added, with a view of creating a more general interest in the minds of junior engineers, and other individuals, whether immediately connected with the profession, or about to study the popular principles and advantageous management of the steam-engine.

When the work was first undertaken, it was written in some measure to induce to algebraic investigations from practical results; rules thus deduced being considered not only more elucidative, but also more general in application, and more easily borne in mind; however, in testing this by public opinion, I have been taught the reverse, for which reason I have withdrawn all formula and substituted instead, rules in the most simple arithmetical form.

The locomotive department has also been with-

drawn, because although the locomotive be an engine, or machine on the non-condensing principle, its construction and mode of working are so complex, that nothing less than a volume entirely devoted to its own peculiarities could possibly do that justice which the merits of the machine demand; and this having already been completed, it is hoped that in the two combined, much useful information for reference will be found on common-place subjects relative to steam and the steam-engine by those to whom it is addressed.

But still farther to enhance the value of the work, a number of very elaborate tables have been added, in order to evade, as much as possible, any loss of time or tendency to inaccuracy in making calculations, in which, unavoidably, the circle and the square require taking into account in a comparative form; such as superficial contents of a circle in square inches or in square feet, the cubic contents of cylinders and of spheres, the ratios of circles and squares, the ratios of spheres and cubes, &c., &c., with other tables of equal importance; hence, it is presumed, that, taking the work as a whole, it will be found not only an important compendium of practical matter relative to the steam-engine, but also an advantageous store of useful reference for the abbreviation of mathematical investigations for practical purposes by men of business in general.

March, 1848.

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THE PRACTICAL

ENGINEER'S COMMON-PLACE BOOK, &c.

ALGEBRAIC SIGNS.

AS APPLIED IN MECHANICAL CALCULATIONS.

| | | |
|---|---|--|
| = | Sign of Equality, and signifies equal to | as 3 added to 4 = 7. |
| + | Addition | plus, or more.....5 + 3 = 8. |
| - | Subtraction | minus, or less8 - 3 = 5. |
| × | Multiplication | multiplied by8 × 3 = 24. |
| ÷ | Division | divided by...24 ÷ 4 = 6, or $\frac{24}{4}$ = 6. |
| :: :: | Proportion | that 2 is to 3 as 4 is to 6. |
| √ | Square Root } | Evolution, or the extraction of roots, |
| $\sqrt[3]{}$ | Cube root } | thus, $\sqrt{64} = 8$, and $\sqrt[3]{64} = 4$. |
| 4^2 | to be squared } | Involution, or the raising of powers, |
| 4^3 | to be cubed } | thus, $4^2 = 16$, and $4^3 = 64$. |
| $3 + 5 \times 4 = 32$ |that 3 plus 5 multiplied by 4 = 32. | |
| $\sqrt{5^2 - 3^2} = 4$ | ...5 squared, minus 3 squared, the square root of the remainder = 4. | |
| $\sqrt[3]{\frac{20 \times 12}{30}}$ | = 2...20 multiplied by 12, and divided by 30, the cube root of the quotient = 2. | |
| $\frac{24 \times 6 + 12 \times 3 \times 4}{12}$ | = 60...24 multiplied by 6, and 12 multiplied by 3, added together, multiplied by 4 and divided by 12, the quotient = 60. | |
| $\frac{A V Q}{n l}$ | = d...that A, V, and Q, multiplied together, and divided by n multiplied by l, the quotient = d. | |
| $\frac{P - p \times d}{W}$ | = D... P minus p multiplied by d, and divided by W = D | |
| $S = \frac{V [(q M + F) D + p d^2 l]}{m P D}$ | ...q multiplied by M, plus F, and multiplied by D, plus p, multiplied by d squared, and by l, the whole sum multiplied by V, and divided by the product of m P D, the quotient = S. | |

IMPERIAL STANDARD MEASURES.

1. MEASURE OF LENGTH.

Inches.

| | | | | | |
|-------------|------------|------------|------------------|------------|---------|
| 12 | 1 foot. | | | | |
| 36 | 3 | 1 yard. | | | |
| 198 | 16½ | 5½ | 1 pole or perch. | | |
| 7920 | 660 | 220 | 40 | 1 furlong. | |
| 63360 | 5280 | 1760 | 320 | 8 | 1 mile. |

The French metre or Standard measure of length = 39.371 in.

SPECIAL MEASURES OF LENGTH.

Nautical Measure.

| | |
|-----------------|--|
| 1 nautical mile | = 6082.66 ft. |
| 3 miles | = 1 league. |
| 20 leagues | = 1 degree. |
| 360 degrees | = earth's cir. |
| 6 feet | = 1 fathom, used in measuring ropes, chains, &c. |

Land Measure.

| | |
|--------------|---------------|
| 7.92 inches | = 1 link. |
| 100 links | = 1 chain. |
| 80 chains | = 1 mile. |
| 69.121 miles | = 1 geo. deg. |

A Table of the common fractional parts of an inch and a foot, with their corresponding decimals.

| Fractions of an inch. | Decimals. | Fractions of an inch. | Decimals. | Fractions of a foot or inches. | Decimals. |
|--------------------------------|-----------|-------------------------------|-----------|--------------------------------|-----------|
| $\frac{1}{8}$ & $\frac{1}{16}$ | = .96875 | $\frac{3}{8}$ & $\frac{1}{4}$ | = .46875 | 11 | = .9166 |
| $\frac{1}{4}$ & $\frac{1}{8}$ | = .9375 | $\frac{5}{8}$ & $\frac{1}{2}$ | = .4375 | 10 | = .8333 |
| $\frac{3}{8}$ & $\frac{1}{4}$ | = .90625 | $\frac{7}{8}$ & $\frac{3}{4}$ | = .40625 | 9 | = .75 |
| | = .875 | $\frac{1}{2}$ | = .375 | 8 | = .6666 |
| $\frac{5}{8}$ & $\frac{3}{4}$ | = .84375 | $\frac{1}{4}$ & $\frac{1}{2}$ | = .34375 | 7 | = .5833 |
| $\frac{3}{4}$ & $\frac{1}{2}$ | = .8125 | $\frac{1}{8}$ & $\frac{1}{4}$ | = .3125 | 6 | = .5 |
| $\frac{7}{8}$ & $\frac{3}{4}$ | = .78125 | $\frac{1}{4}$ & $\frac{1}{2}$ | = .28125 | 5 | = .4166 |
| $\frac{1}{2}$ | = .75 | $\frac{1}{8}$ | = .25 | 4 | = .3333 |
| $\frac{5}{8}$ & $\frac{3}{4}$ | = .71875 | $\frac{1}{8}$ & $\frac{1}{2}$ | = .21875 | 3 | = .25 |
| $\frac{3}{4}$ & $\frac{1}{2}$ | = .6875 | $\frac{1}{8}$ & $\frac{1}{4}$ | = .1875 | 2 | = .1666 |
| $\frac{7}{8}$ & $\frac{3}{4}$ | = .65625 | $\frac{1}{8}$ & $\frac{1}{2}$ | = .15625 | 1 | = .0833 |
| $\frac{1}{4}$ | = .625 | $\frac{1}{8}$ | = .125 | $\frac{1}{2}$ | = .07291 |
| $\frac{5}{8}$ & $\frac{3}{4}$ | = .59375 | — $\frac{3}{8}$ | = .09375 | $\frac{1}{4}$ | = .0625 |
| $\frac{3}{4}$ & $\frac{1}{2}$ | = .5625 | — $\frac{1}{4}$ | = .0625 | $\frac{1}{8}$ | = .0528 |
| $\frac{7}{8}$ & $\frac{3}{4}$ | = .53125 | — $\frac{1}{8}$ | = .03125 | $\frac{1}{16}$ | = .04166 |
| $\frac{1}{8}$ | = .5 | | | $\frac{1}{32}$ | = .03125 |
| | | | | $\frac{1}{64}$ | = .02083 |
| | | | | $\frac{1}{128}$ | = .01041 |

Inches.

| | | | |
|---------|-------|-------|--|
| 144 | | 1 | square foot. |
| 1296 | | 9 | 1 square yard. |
| 39204 | | 2721 | 301 1 square pole. |
| 1568160 | | 10890 | ... 1210 40 1 rood. |
| 6272640 | | 43660 | 4840 160 4 1 acre. |

Land Measure.

62.7264 square inches = 1 square link,
10000 " = 1 " chain, and
10 square chains = 1 acre.

General Measure of Solidity.

1728 cubic inches = 1 cubic foot.
27 cubic feet = 1 cubic yard.
42 cubic feet = 1 ton of shipping.

| Cubic Inches. | Water lbs. av. | |
|------------------|-------------------|--|
| 8.665 | $\frac{1}{4}$ | 1 gill. |
| 34.659 | $\frac{1}{2}$ | 4 ... 1 pint. |
| 69.318 | $\frac{3}{4}$ | 8 ... 2 ... 1 qrt. |
| 277.274 | 1 | 32 ... 8 ... 4 ... 1 gal. |
| 554.548 | 2 | 64 ... 16 ... 8 ... 2 ... 1 peck. |
| 2218.19 | 8 | 256 ... 64 ... 32 ... 8 ... 1 bushl. |
| 17745.5 | 64 | 2048 ... 512 ... 256 ... 64 ... 32 ... 8 ... qr. |

The peck, bushel, and quarter, are used for dry goods only.

| | | | | |
|---|---------------------|---|-------|--------------|
| 1 | gallon of sea water | = | 10.32 | lbs. avoird. |
| 1 | " oil | = | 9.32 | " |
| 1 | " proof spirits | = | 9.3 | " |
| 1 | bushel of wheat | = | 60 | " |
| 1 | " barley | = | 47 | " |
| 1 | " oats | = | 38 | " |

The old ale gallon contained 282 cubic inches ; and

The old wine gallon 231.

The French litre, or standard measure of capacity for liquids, contains 61.028 cubic inches, or about .453 of our imperial gallon.

5. IMPERIAL MEASURE OF CAPACITY FOR COALS, CULM, LIMES, FRUIT, &c.

| | |
|-----------------------|---|
| 351.9375 cubic inches | 1 gallon. |
| 703.875 | 2 ... 1 peck. |
| 2815 5 | 8 ... 4 ... 1 bushel. |
| 4.888 cubic feet | 24 ... 12 ... 3... 1 sack. |
| 58.656 | 288 ... 144 ... 36 .. 12... 1 chaldron. |

In and about London coals are sold by the cwt., ton, &c., but in Yorkshire, and many other places, they are sold by the bag, and estimated as follows:—

1 bag = 2 bushels, and weighs about 140lbs.
16 bags = 1 ton, and 24 bags = 1 chaldron, or 30 cwt.

A keel of coals at Newcastle is 21 tons 4 cwt., and a chaldron of 53 cwt. A chaldron of coals in London is 28½ cwt.

6. AVOIRDUPOIS WEIGHT.

| | |
|--------------|--|
| Troy Grains. | 1 dram. |
| 27.34375 | 16... 1 ounce. |
| 437.5 | 256... 16... 1 lb. |
| 7000 | 3584 .. 224... 14... 1 stone. |
| 98000 | 7168... 448... 28.. 2... 1 quarter. |
| 196000 | 28672... 1792... 112... 8... 4... 1 cwt. |
| 784000 | 57344... 35840... 2240... 160.. 80... 20... 1 ton. |
| 1568000 | |

The French gramme, or standard measure of weight, equal 15.434 troy grains, and the kilogramme 2.20486 lbs. avoirdupois.

About 426 cubic inches of cast iron = 1 cwt.

| | | | |
|---------------------|---|------------|----------|
| 8520 | " | or | |
| nearly 5 cubic feet | | | = 1 ton. |
| 13 | " | of stone | = 1 ton. |
| 23 | " | sand | = 1 ton. |
| 29 | " | coal | = 1 ton. |
| 38 | " | tallow | = 1 ton. |
| 39 | " | oil | = 1 ton. |
| 40 | " | timber | = 1 ton. |
| 36 | " | com. water | = 1 ton. |
| 35 | " | sea water | = 1 ton. |

SPECIFIC GRAVITIES.

13

Table of Specific Gravities.

| NAMES OF BODIES. | Weight of a cubic foot in lbs. | Weight of a cubic in. in ounces. | Number of cubic inches in a lb. | Weight of a cubic inch in lbs. |
|----------------------|---|---|--|---|
| Copper, cast | 549.25 | 5.086 | 3.146 | .3178 |
| Copper, sheet..... | 557.18 | 5.159 | 3.103 | .3225 |
| Brass, cast | 524.75 | 4.852 | 3.223 | .3037 |
| Iron, cast..... | 454.43 | 4.203 | 3.802 | .263 |
| Iron, bar..... | 476.93 | 4.410 | 3.623 | .276 |
| Lead | 709.00 | 6.456 | 2.437 | .4103 |
| Steel, soft | 489.56 | 4.527 | 3.530 | .2833 |
| Steel, hard | 488.50 | 4.517 | 3.537 | .2827 |
| Zinc, cast..... | 449.37 | 4.156 | 3.845 | .26 |
| Tin, cast | 455.75 | 4.215 | 3.790 | .2636 |
| Bismuth | 619.50 | 5.710 | 2.789 | .3585 |
| Gun metal | 549.00 | 5.077 | 3.147 | .3177 |
| Sand..... | 95.00 | .878 | 18.190 | .055 |
| Coal | 78.12 | .722 | 22.120 | .0452 |
| Brick | 125.00 | 1.156 | 13.824 | .0723 |
| Stone, paving..... | 151.00 | 1.396 | 11.443 | .0873 |
| Marble | 171.37 | 1.585 | 10.083 | .0991 |
| Glass | 180.00 | 1.664 | 9.600 | .1042 |
| Tallow | 59.06 | .546 | 29.258 | .0342 |
| Cork..... | 15.00 | .138 | 115.200 | .0087 |
| Oak | 60.62 | .561 | 28.505 | .0351 |
| Pine, pitch | 41.25 | .382 | 41.890 | .024 |
| Ash | 47.50 | .440 | 36.370 | .0275 |
| Spirits, proof | 57.93 | .536 | 29.828 | .0335 |
| Mercury | 848.00 | 7.851 | 2.037 | .4908 |

A Table of the specific gravity of water at different temperatures, that at 62 being taken as unity.

| | | | |
|-------|---------|-------|---------|
| 70°F. | .99913 | 52°F. | 1.00076 |
| 68 | .99936 | 50 | 1.00087 |
| 66 | .99958 | 48 | 1.00095 |
| 64 | .99980 | 46 | 1.00102 |
| 62 | 1. | 44 | 1.00107 |
| 58 | 1.00035 | 42 | 1.00111 |
| 56 | 1.00050 | 40 | 1.00113 |
| 54 | 1.00064 | 38 | 1.00115 |

Note. The difference of temperatures between 62° and 42°, where water attains its greatest density, will vary the bulk of a gallon rather less than the third of a cubic inch.

WATER.

Water, in an aëiform state, constitutes the steam-engine a moving power; consequently to the practical engineer some knowledge of the chemical and mechanical properties of water must be not only interesting, but of considerable importance in other points of view.

Water, or oxide of hydrogen, is a fluid composed of two elementary bodies, or gases, viz., oxygen and hydrogen, the union of which are so compact that its compressibility with the utmost application of force is so small, that in practice it is with propriety termed generally an incompressible fluid.

Proportions of the gases are the following:—

| | WEIGHT. | BULK. |
|------------------|---------|-------|
| Oxygen | 8 | 1 |
| Hydrogen..... | 1 | 2 |
| Equivalents..... | 9 | 3 |

Or one cubic inch consists of

| | GRAINS. | CUBIC INCHES. |
|---------------|---------|---------------|
| Oxygen | 224.46 | 662 |
| Hydrogen..... | 28.06 | 1325 |
| | 252.52 | 1987 |

Water, when pure, is transparent, colourless, tasteless, odorless, and not liable to spontaneous change; liquid at the common temperature of our atmosphere; assuming a solid form at 32° Faht., and a gaseous state at 212°, but returning unaltered to its liquid state on resuming any degree of heat between these points; dissolves numerous vegetable, animal, and mineral substances; is decomposed in many cases of chemical action, affording oxygen or hydrogen to the substances which affect it.

Clean iron and zinc at a red heat possess the property of decomposing water when in the state of highly rarefied steam; the oxygen uniting with the metal, a solid metallic crust is formed on the surface, and the hydrogen set at liberty; one volume of oxygen, or from five to

six of atmospheric air, mixed with two of hydrogen, render the mixture inflammable, and on the approach of a flame, red-hot iron, or the electric spark, the whole is kindled at the same instant, a flash of light passes through the mixture, followed by a violent explosion, the result of which is steam at 212° Faht., and ultimately pure water.

But water, as it exists in nature, contains various saline or earthy matters; as muriate of soda, or common salt, sulphate of lime, carbonate of lime, muriate of magnesia, oxide of iron, &c., accumulated in flowing through the different strata of rocks and minerals, constituting mineral or hard water, by which it is considerably reduced in value for the purposes of a steam-engine. Rain and snow waters are the purest natural waters we possess, and are generally employed as the standard of comparison for the densities of other bodies.

Specific gravity of pure rain water = 1, or one cubic foot at a mean temperature of the atmosphere = 1000 ounces.

Ten pounds of rain or distilled water, at 62° Faht., equal the standard gallon, or measure of capacity. And one cubic inch, at 62° Faht. = 252.458 grains.

Mineral waters of every description are more or less injurious to a boiler; and, unless very frequently changed, become in a state of saturated solution, in consequence of which earthy matters are deposited, and an incrustation formed on the surface of the iron, preventing the free passage of caloric; hence, the plates get red hot, and render the boiler in danger of being destroyed.

Mineral waters are generally divided into four classes, namely, the *acidulous*, the *sulphureous*, *chalybeate*, and *saline*.

Acidulous waters contain carbonic acid in its free state, or in combination in excess with a base; also, very frequently muriate of soda, and some of the earthy carbonates; however, it is the free carbonic acid that

imparts to them their particular properties. These waters are easily distinguished by their slightly acid taste, and sparkling appearance when poured from one vessel to another, both of which properties they lose by boiling, or standing exposed to the air for any short length of time.

Sulphureous waters contain sulphureted hydrogen, also alkaline, earthy sulphates, and muriates; they are very readily distinguished by their odour, and by causing a piece of silver, when immersed in them, to acquire a dark colour.

Chalybeate waters are those which have iron as an ingredient; they are known by their peculiar taste, and by their becoming black when mixed with an infusion of nutgalls; but they are of different kinds; sometimes the iron is combined with sulphuric acid,—more frequently it is in union with carbonic acid.

Saline waters are those which contain the saline ingredients generally found in mineral waters, but which have not carbonic acid in excess, and are free from sulphureted hydrogen and iron, or contain them in very trifling quantities. Saline waters may be subdivided into four kinds, namely—alkaline waters, or those which contain alkali in its free state, or combined with carbonic acid, and which render the vegetable blues green; hard waters, or those which combine carbonate or sulphate of lime; salt waters, or those in which muriate of soda abounds; purgative waters, or those which contain principally sulphate of magnesia.

To ascertain the properties of any water, the following experiments may be resorted to:—

1. Evaporate a drop on a flat slip of glass, holding it before the fire, or above a small lamp or candle. Small rings only appear where the water rested, if it contained only a minute quantity of foreign matter; but a crust is seen if it be loaded with saline or earthy matter, and the crust has an ochry tint if *iron* be present.

2. Pour some of the water into a wine glass, and add a solution of litmus; it will be reddened if any free acid matter be present.

3. Mix another portion with a little soap; a curdy matter appears if it abound with earthy matter.

Sea water contains of saline and *earthy* matter in every 100 parts,

| | |
|--------------------------|------|
| Common salt..... | 2.66 |
| Sulphate of soda..... | .466 |
| Muriate of lime..... | .199 |
| Muriate of magnesia..... | .991 |

4.316 parts of

saline and earthy matter. Average specific gravity 1028. Hence the necessity of frequently renewing the water in marine engine boilers at sea, by the usual process of *blowing out*; that is, by a little extra feed the boilers are allowed to fill, say, from four to six inches above the regular height, and the overcharged water blown out by the force of the steam, through a cock in the bottom of the boiler, at least once every two hours.

MECHANICAL PROPERTIES OF WATER.

1. Fluid bodies in general exert an equal force or pressure in every direction, namely, upwards, downwards, sideways, and oblique, and fluids always tend to a level; hence, any quantity of water, however small, may be made to balance and support any quantity, however large.

2. The weight of water, or any other fluid body, is as the quantity; but the pressure is as the perpendicular height.

3. The pressure on the sides of any vessel containing a fluid is equal to the length of the side multiplied by half the square of the depth.

4. The centre of pressure, and also the centre of percussion, in a fluid, is two-thirds of the depth from the surface.

5. The quantity of water discharged through an orifice in equal times, but under different heads, is nearly as the corresponding heights of the different heads of water; hence,

The square root of the depth in feet \times by the falling surface in inches

Area of the orifice \times 3.7

the time required in seconds.

Maximum density of water 42° Faht.

Freezing point 32° Faht., at which point it has expanded $\frac{1}{7}$ of its original bulk.

62.5 lbs. avoirdupois = the weight of 1 cubic foot.

.03617 = 1 " inch.

.434 = 1 lineal ft. lin. sq.

49.1 = 1 cylindrical foot.

.02842 =1 " inch.

.341 = 1 lin. ft. 1 in. dia.

11.2 imperial galls. = 1 cwt.

224. = 1 ton.

1.8 cubic feet. = 1 cwt.

35.84 = 1 ton.

1 cubic foot of water = $6\frac{1}{4}$ imperial gallons, and

1 cylindrical foot = about 5.

The content of any vessel in cubic feet \times by 6.232 }
 Or " " inches \times by .003607 } =
 imperial gallons.

Any number of imperial gallons

Any two dimensions of a cistern in feet \times by 6.232
 third dimension in feet. = the

Any number of imperial gallons

Any two dimensions of a cistern in inches \times by .003607
 = the third dimension in inches.

The length of a cylinder in feet \times by the
 square of the diameter in feet, and by 4.895...
 The length of a cylinder in feet \times by the
 square of the diameter in inches and by 0.34
 The length of a cylinder in inches \times by the
 sq. of the diameter in inches and by .002832

} = Imp. gallons.

any number of gallons a cylinder is required to
 contain \times by 354

 by the length in inches
 the diameter of the cylinder in inches.

Any number of gallons a cylinder is required to
 contain \times by 354

 by the square of the diameter in inches
 the length of the cylinder in inches.

The cube of the diameter of a sphere in inches \times by .001888 = imperial gallons.

The velocity of water in feet per minute \times by the square of a pump's diameter in inches, and by .034 = imperial gallons discharged per minute.

The velocity of water in feet per minute \times by the square of a pump's diameter in inches, and by .0005454 = cubic feet discharged per minute.

OF STEAM, OR RAREFIED WATER.

When water in a boiler is subjected to the action of fire, it imbibes the heat or caloric that the fire imparts, and sooner or later acquires a degree of temperature at which ebullition takes place, and particles of steam arise through the surface of the water, hence designated the *boiling point*; but the degree of temperature at which this takes place is entirely governed by the density of the fluid pressing on the surface of the water, thus, in a vacuum water boils at about 98° Faht. ; under com-

mon atmospheric pressure, at 212° ; and to produce steam at $2\frac{1}{2}$ lbs. per square inch, requires a temperature of 220° , &c., as in the following table :—

| Temperature in degrees of Fahr. | Force in lbs. per | | | Temperature in degrees of Fahr. | Force in lbs. per | | |
|------------------------------------|-------------------|-----------------------|-------------------|------------------------------------|-------------------|-----------------------|-------------------|
| | Square Inch. | Inches of Mercury. | Feet of Water. | | Square Inch. | Inches of Mercury. | Feet of Water. |
| 220 | 2.5 | 5.15 | 5.76 | 240 | 10 | 20.60 | 23.05 |
| 222 | 3 | 6.18 | 6.91 | 245.5 | 12 | 24.72 | 27.64 |
| 223.5 | 3.5 | 7.21 | 8.07 | 251 | 15 | 30.90 | 34.57 |
| 225 | 4 | 8.24 | 9.22 | 260 | 20 | 41.20 | 46.10 |
| 227 | 4.5 | 9.27 | 10.37 | 268 | 25 | 51.50 | 57.62 |
| 228 | 5 | 10.30 | 11.52 | 275 | 30 | 61.80 | 69.15 |
| 230 | 5.5 | 11.33 | 12.68 | 282 | 35 | 72.12 | 86.67 |
| 231.5 | 6 | 12.36 | 13.82 | 288 | 40 | 82.41 | 92.20 |
| 233 | 6.5 | 13.39 | 14.98 | 294 | 45 | 92.70 | 103.72 |
| 234 | 7 | 14.42 | 16.14 | 299 | 50 | 103.00 | 115.25 |
| 235 | 7.5 | 15.45 | 17.28 | 304 | 55 | 113.31 | 126.77 |
| 236 | 8 | 16.48 | 18.44 | 309 | 60 | 123.60 | 138.80 |

Steam contains about five times the quantity of heat to that of boiling water; it is transparent and colourless until it comes in contact with the atmosphere, it then assumes a dense white mass, the caloric which maintained its gaseous form is therein absorbed, and hence, in consequence, its properties as steam are eventually destroyed.

The principal properties of steam, relative to the steam-engine, are the following :—

1. Elasticity, or the power that it has to return to its original form, after being made to deviate by some external force.

2. Expansibility, or the increase of bulk which it undergoes by the recession of its particles from one another, so that it occupies a greater space, while its weight remain the same.

3. Condensation, or the causing of the mass to occupy less space, by means of the closer approach of its particles through the abstraction of heat.

Table exhibiting various properties of steam.

| Elastic force in atmospheres. | Elastic force in lbs. per sq. inch. | Degrees of heat. | Difference of temperature. | Volume in cubic feet, water being 1. | Velocity into a vacuum in feet per sec. |
|-------------------------------|-------------------------------------|------------------|----------------------------|--------------------------------------|---|
| 1 | 14.7 | 212°F | | 1711 | 1566 |
| 2 | 29.4 | 250.52 | 38.50°F | 905 | 1610 |
| 3 | 44.1 | 275.18 | 24.66 | 623 | 1638 |
| 4 | 58.8 | 293.72 | 18.54 | 479 | 1658 |
| 5 | 73.5 | 308.84 | 15.12 | 394 | 1674 |
| 6 | 88.2 | 320.36 | 11.52 | 331 | 1688 |
| 7 | 102.9 | 331.70 | 11.34 | 288 | 1700 |
| 8 | 117.6 | 341.96 | 10.26 | 255 | 1710 |
| 9 | 132.3 | 350.78 | 8.82 | 229 | 1720 |
| 10 | 147.0 | 358.88 | 8.10 | 209 | 1729 |
| 12 | 176.4 | 374.00 | 15.12 | 190 | 1742 |
| 15 | 180.5 | 392.86 | 18.86 | 135 | 1765 |
| 20 | 294.0 | 418.45 | 25.59 | 111 | 1786 |
| 30 | 441.0 | 457.16 | 38.71 | 77 | 1823 |
| 50 | 735.0 | 510.60 | 53.44 | 42 | 1873 |

Hence, from this table it will be inferred, that as such small accessions of heat produce so rapid an increase of elastic force, small abstractions of heat from highly rarified steam, will also reduce its elasticity in an equal degree, so that high pressed steam is more readily diminished in bulk by the application of cold, than steam of less density; that is, it can be more readily reduced in its pressure to any certain proportion of the pressure it had before; thus rendering to the purposes of the steam-engine properties of very economical interest, because by admitting only a small quantity to enter the cylinder through being sooner stopped off, and from thence, by its expansive force, continue the motion of the piston to the end of the stroke, the advantage of which is according to the results as estimated by the following rule:—

C B

C

Divide the length of the stroke of the piston in a steam engine, by the distance the dense steam has been admitted into the cylinder, previous to its being cut off, and find the hyperbolic logarithm of the quotient, to which add 1, and the sum is the ratio of the gain.

EXAMPLE.—Suppose an engine, with a stroke of 6 feet, and the steam cut off when the piston has moved through 2, required the ratio of gain by uniform and elastic force,

$$\begin{aligned} 6 \div 2 &= 3; \text{ hyperbolic logarithm of } 3 = 1.0986 \\ + 1 &= 2.0986 \text{ ratio of effect; that is, supposing} \\ &\text{the whole effect of the steam to be 3, the effect of} \\ &\text{the steam being cut off at one-third of the stroke,} \\ &= 2.0986. \end{aligned}$$

But steam produced from water-holding salts, or other impurities in solution, is not of equal density to that produced from pure water, although both be of equal temperatures: thus, from experiment and practice, the steam produced from common water, at 212° Faht., will support a column of mercury 30 inches in height; whereas steam from sea water, at an equal temperature, will support no more of an equal column than $22\frac{1}{2}$ inches. In like manner, the steam from common water, at 220° Faht., will support a column of mercury 35 inches in height; and that from sea water, at an equal temperature, only $26\frac{1}{2}$ inches: hence the great propriety of obtaining water so pure as possible for the generation of steam.

OF THE STEAM-ENGINE, THE BOILER, &c.

The Steam-engine is a machine calculated expressly for the purpose of rendering steam available, as a motive power, to the purposes of machinery; its forms are numerous, but its principles, as a moving cause, depend entirely on that of water in a state of rarification by heat.

Water, in its natural state, is an incompressible fluid, but combined with caloric, or the matter of heat, it is changed, and becomes an elastic transparent vapour of great force.

The Boiler or vessel containing the water to which the heat is applied, and in which the steam is generated, is commonly of wrought or plate iron, sometimes of copper, but in form no peculiarity is required otherwise than what compulsion dictates, viz., capacity, best form for strength, and a sufficiency of heating surface, to distribute properly the caloric through the water.

There is perhaps nothing which tends more to the inefficiency of a boiler than the want of sufficient capacity—inequality of pressure, frequent priming, and unnecessary waste of fuel, are amongst the common evils resulting therefrom; but unfortunately, practice, in various instances, forbids that amount of capacity which is laid down as a general rule, (*viz., one cubic yard to each horse-power, two-thirds of which to be occupied by water,*) as may not unfrequently be seen in those of marine boilers, locomotives, &c., the defective results of which, in many instances, not being easily construed.

With respect to a sufficiency of heating surface proportionate to the boiler's capacity, or more properly to the quantity of water that must be boiled off in a given time, much discrepancy of opinion still continue to induce dispute; but no doubt a great portion of this may exist, because of parties not being sufficiently explicit in distinguishing between the amount of horizontal and that of vertical or side surface, the efficiency of the former being called, 1, that of the latter is little more than one-half; hence the propriety of giving inclination inwards to the plates of all flues, not only to approximate that of horizontal surface, but also to effect a more ready access to the surface of the water, the caloric or particles of steam generated underneath.

When the horizontal heating surface of a boiler only,

is taken into account, *nine* square feet to each horse-power is considered a sufficiently productive surface; but when the whole heating surface of whatever description is included, not less than *fourteen* square feet to each horse-power can confidently be relied upon, unless the expansive principles in the cylinder of the engine be carried out to a considerable extent.

The dimensions expressed as above, are for engines of customary nominal power, and with about *one* square foot of fire bar to each *fourteen* square feet of heating surface; but the following rules are more intimately adapted, because, to suit the various peculiarities of engines, and the various densities of steam required.

But, in the construction of boilers generally, much attention ought to be paid to the avoiding of thin films of water where the action of the fire is great, because it is neither consistent with safety, nor can there be the proper quantities of steam generated proportionately to the surface exposed, unless under an extraordinary degree of pressure. Also, convex surfaces, exposed to the action of the steam, unless properly supported, ought strenuously to be avoided. Large water spaces, concave surfaces, or straight plates with the butt edges upwards and securely stayed, with ample steam room, are the chief requisites to be attended to.

1. *To determine the proper quantity of heating surface a boiler ought to contain, for an engine with a cylinder of a given capacity, and steam of any density, as in the following table.*

RULE.—Multiply the area of the piston in square feet, by its velocity in lineal feet per minute, and by the decimal equivalent in the last column of the following table, opposite the required density of steam in the first column, and the product is the heating surface of the boiler in square feet.

EXAMPLE.—Required the amount of effective heating

surface for the boiler of an engine, the area of whose piston is 9 square feet, its velocity 192 feet per minute, and the density of the steam 5lbs. per square inch above the pressure of the atmosphere.

$$192 \times 9 \times .3328 = 575 \text{ square feet of heating surface.}$$

NOTE.—By effective heating surface is meant horizontal surfaces over fire, flame, or heated air; vertical or side surfaces requiring about $1\frac{1}{2}$ feet to equal 1 of horizontal surface.

2. *To determine the proper dimensions for a waggon-shaped boiler, the amount of effective heating surface being given.*

RULE.—The bottom surface equal half the whole surface.

The length equal twice the square root of bottom surface.

The width equal one-fourth the length; and

The height equal one-third the length.

EXAMPLE.—Required the dimensions for a boiler of the waggon form, that shall present an effective heating surface of 175 square feet.

$$\text{Bottom surface} = 175 \div 2 = 87.5 \text{ square feet.}$$

$$\text{Length} = \sqrt{87.5} \times 2 = 18.72 \text{ feet.}$$

$$\text{Width} = 18.72 \div 4 = 4.68 \text{ feet.}$$

$$\text{Height} = 18.72 \div 3 = 6.24 \text{ feet.}$$

3. *To determine the dimensions for a cylindrical boiler.*

RULE.—Extract the square root of 1.34 times the effective heating surface in square feet, and twice the root equal the boiler's circumference in feet; also the circumference equal the length.

EXAMPLE.—Required the diameter and length of a cylindrical boiler, with an effective heating surface of 86 square feet.

$$\sqrt{86 \times 1.34} = 10.74 \times 2 = 21.48 \text{ feet circumference, or 6 feet 10 inches diameter; and 21.48 feet in length.}$$

Practical Table of steam properties, by which to estimate the effects of the steam-engine, &c.

| Force in lbs. per square inch above the atmosphere. | Temperature in degrees of Fahrenheit. | Increase of temperature required to produce the increase of force. | Volumes of steam produced from 1 of water. | Cubic inches of water to produce a cubic foot of steam. | Decimal equivalents for facilitating the calculations of boiler surface, &c. |
|---|---------------------------------------|--|--|---|--|
| 2.5 | 220° | — | 1496 | 1.14 | .2507 |
| 3 | 222 | 2° | 1453 | 1.18 | .2581 |
| 4 | 225 | 5 | 1366 | 1.25 | .2745 |
| 5 | 228 | 8 | 1282 | 1.33 | .2925 |
| 6 | 231 | 11 | 1228 | 1.41 | .3054 |
| 7 | 234 | 14 | 1174 | 1.47 | .3194 |
| 8 | 236 | 16 | 1127 | 1.52 | .3328 |
| 9 | 238 | 18 | 1084 | 1.58 | .3459 |
| 10 | 240 | 20 | 1044 | 1.64 | .3592 |
| 12 | 245 | 25 | 973 | 1.80 | .3854 |
| 15 | 251 | 31 | 883 | 1.93 | .4247 |
| 20 | 260 | 40 | 767 | 2.23 | .4889 |
| 25 | 268 | 48 | 678 | 2.52 | .5531 |
| 30 | 275 | 55 | 609 | 2.81 | .6158 |
| 35 | 282 | 62 | 553 | 3.09 | .6781 |
| 40 | 288 | 68 | 506 | 3.38 | .7411 |
| 45 | 294 | 74 | 468 | 3.66 | .8013 |
| 50 | 299 | 79 | 435 | 3.93 | .8621 |
| 55 | 304 | 84 | 407 | 4.20 | .9211 |
| 60 | 309 | 89 | 382 | 4.48 | .9816 |

APPENDAGES TO BOILERS.

THE SAFETY VALVE.

A safety valve is properly a loaded circular disc covering an opening in the top or upper side of a steam boiler, for the purpose of prevention by escape any unnecessary or unsafe accumulation of steam in the boiler by the intensity of the fire whilst the engine is not at work, or otherwise.

Safety valves generally are loaded either directly or by the action of a lever with a weight or spring balance attached. When the weight is acting immediately upon the valve, without the intervention of a lever, the amount of weight in lbs., divided by the area of the valve in inches equal the direct pressure on each inch of the boiler; but if a lever is applied, the principle of the lever must be taken into account, and in practice the following various points of action and effect are the chief that require the particular notice of the practical engineer.

The lever being moveable round a pin as an axis at one end, and resting upon the valve as a fulcrum at some proportionate distance, tends to press down the valve less or more, according to the lever's length and general magnitude, the effect of which is designated the *action* of the lever upon the valve, the amount of which is very easily ascertained by simply attaching to the lever a spring balance by a piece of twine or otherwise, but immediately above the centre of the valve, and observing the index when gently lifted by hand, hence the amount of weight indicated, and added to the weight of the valve, are a constant quantity which must be subtracted or added, as the nature of the calculation may require.

Again, when a lever is applied to a valve where a weight is to be attached, the lever may be of any length whatever; but where a spring balance is to be applied, the lever ought to be of the following proportion—viz., the distance from the lever's centre of rotation to the centre of the valve equal the diameter of the valve, and the distance from the lever's centre of rotation to the spring balance as many times the diameter of the valve as there are square inches in its area; hence, the exact pressure upon each square inch of the boiler is always indicated by the spring balance, plus the action of the lever and weight of the valve.

To estimate properly the various amounts of effect by a lever and weight, or spring balance, acting upon a safety valve.

Suppose, for a general example, that the diameter of the valve = 6 inches, or 28.27 square inches area.

The required pressure per square inch = 12 lbs., or 339.24 lbs. total pressure on valve.

Length of lever $26\frac{1}{2}$ inches.

Distance from centre of rotation to centre of valve 4 inches.

Action of lever and weight of valve together $9\frac{1}{2}$ lbs.; then,

1. To find what weight will be required to produce that pressure at a given distance, say 19 inches from the centre of rotation.

$$\frac{339.24 - 9.5 \times 4}{19} = 69.4 \text{ lbs. suspended on the lever.}$$

2. When the weight to be placed upon the lever is given, and other peculiarities as above, to find at what distance from the centre of rotation, that weight must be placed to produce the pressure required.

$$\frac{339.24 - 9.5 \times 4}{69.4} = 19 \text{ inches distant from lever's centre of rotation.}$$

3. The weight, with its distance from the lever's centre of rotation being given, and also from the same point to the centre of the valve, to find what is the effective pressure at that point; action of lever and weight of valve included.

$$\frac{69.4 \times 19}{4} = 329.65 + 9.5 = 339.15 \text{ lbs. Total amount of pressure upon the valve.}$$

4. Suppose a spring balance attached at the end of the lever, (which in our present example is $26\frac{1}{2}$ inches from the centre of rotation, other peculiarities as before,) and the tendency of the steam to raise the valve equal any given quantity, say 339.24 lbs. to find what weight ought to be indicated by the spring balance.

$$\frac{339.24 - 9.5 \times 4}{26.5} = 49.772 \text{ lbs. indicated by the spring balance.}$$

5. The total amount of force tending to raise a safety valve, also the distance of valve's centre to centre of lever's rotation being given, to find what length of lever is necessary to equipoise the required pressure, by a certain indicated weight upon the spring balance.

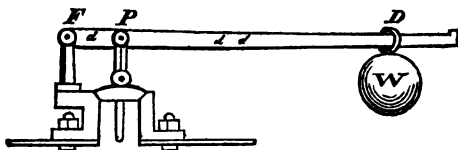
$$\frac{339.24 - 9.5 \times 4}{49.772} = 26.5 \text{ inches, the distance between the spring balance and lever's centre of rotation.}$$

TO FIND THE PROPER DIAMETER FOR A SAFETY VALVE.

RULE.—Multiply the bottom surface of the boiler, or surface immediately exposed to the action of the fire, in feet, by the multiplier opposite to the pressure in lbs. on each square inch of the safety valve, and the square root of the product is the valve's diameter in inches at the narrowest part. If the boiler is to have two safety valves, then the square root of half the product equals the diameter of each.

| Pressure in lbs. per square inch. | Multipliers. |
|--------------------------------------|--------------|
| 3 | .356 |
| 4 | .363 |
| 5 | .348 |
| 6 | .344 |
| 7 | .339 |
| 8 | .336 |
| 10 | .329 |
| 12 | .321 |

| Pressure in lbs. per square inch. | Multipliers. |
|--------------------------------------|--------------|
| 15 | .315 |
| 20 | .305 |
| 25 | .293 |
| 30 | .289 |
| 35 | .282 |
| 40 | .275 |
| 45 | .270 |
| 50 | .264 |



NOTE.—In the above section of a valve with a lever, let F denote the fulcrum, P the whole pressure upon the valve, D the distance of the weight from F, d the distance between F and P, $d d$ the distance between F and D, W the weight upon the lever, and p the action of the lever upon the valve.

$$\text{Then 1. } \frac{P - p \times d}{d d} = W.$$

$$2. \frac{P - p \times d}{W} = D.$$

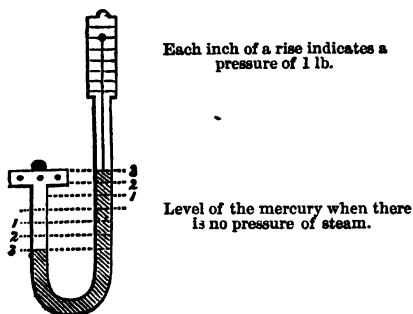
$$3. \frac{W \times d d}{d} + p = P.$$

THE STEAM GAUGE

Is an indicator of conspicuous reference, by which the density or force of steam in the boiler may be at all times ascertained, this being an object of the strictest importance, because, through laxity of attention, a vacuum might be formed in the boiler, or the steam might be of considerably greater elastic force than required, although escaping partially by the safety valve; hence the steam gauge is a general test for the regulation of the fire. Again, if by any means the safety valve become fastened, and a superabundant force of steam accumulated, the mercury may be driven out of the tube, by which extra indication is given, and ultimately the steam gauge become of itself a means of diminishing the force of the steam, in proportion to the dimensions or bore of the tube of which it is formed.

The common construction of a steam gauge is an inverted syphon, or bent tube of wrought iron, one end of which may be attached to the boiler or steam pipe to suit convenience, a hole having been previously made for the free emission of the steam to a counterpoise of

mercury for the purpose in the tube, the other end of which is open to the atmosphere ; but the action of the column of mercury may appear more plain by means of the following section :



The steam depresses the mercury in the short tube, consequently causes it to rise in the longer one ; 2 inches of mercury is a counterpoise to 1 lb. pressure of steam, therefore a rise of 1 inch in the long tube indicates a force equal to 1 lb. per square inch in the boiler.

A FLOAT

Is as requisite for ascertaining the height of the water in a boiler as a glass gauge is for the height of the steam, but can only be properly applied in a land or fixed engine boiler. The float may be of either *stone, iron, copper*, or any other body that will not be destroyed by the heat of the water or force of the steam ; hence, a float may be made so heavy as to sink in the water, consequently a counterpoise is required ; or it may be made so buoyant that it will neither be steady in the boiler, sink to the depth required, nor will it fall by its own gravity when the water is getting low, therefore additional weight must be attached, and in either case the float immersed about $\frac{2}{3}$ ds of its thickness or depth.

RULE 1.—*When too heavy*, subtract the weight of the water displaced from the weight of the float; the remainder is the counterpoise required.

RULE 2.—*When too buoyant*, subtract the weight of the float from the weight of the water displaced; and the remainder is the weight that must be added to the float.

NOTE.—The weight must either be inside the float, or otherwise attached, clear of the surface of the water.

EXAMPLE 1.—Required the weight necessary to counterpoise a float of paving stone, 14 inches diameter, $2\frac{1}{4}$ inches thick, and immersed two-thirds of its thickness in fresh water;

say, the weight of stone and rod attached = $30\frac{1}{2}$ lbs.

then, $\frac{14^2 \times .7854 \times 2.25 \times 2}{3} = 230.9$ inches of water displaced.

1 inch of water = .03617 lbs. avoirdupois; hence,
 $230.9 \times .03617 = 8.35$ lbs. of water displaced, and
 $30.5 - 8.35 = 22.15$ lbs. required for a counterpoise.

EXAMPLE 2.—Suppose a float to consist of a concave copper ball, 12 inches diameter outside, and weigh with rod attached $7\frac{1}{4}$ lbs.; required the weight that must be added inside, so that the ball may remain immersed half its depth in fresh water.

$\frac{12^3 \times .5236 \times .03617}{2} = 16.36$ lbs. of water displaced,

and $16.36 - 7.25 = 9.11$ lbs. that must be added to the float.

GAUGE COCKS AND GLASS TUBES

Are intended to show the height of water in a boiler where a float cannot properly be applied, such as those of *marine and locomotive engines*, but require particularly strict attention under the following circumstances;—namely, *all new boilers, boilers immediately after being cleaned, and marine boilers in passing from fresh to salt*

water, or from salt to fresh, more especially water holding earthy and other matters in solution; in either case the water, when steam is up, becomes frequently in a state of complete fermentation, the boiler appears to contain more than a sufficient quantity of water, when in reality there may not be *solid* water, as it is termed, at the first cock, which ought not to be less than from three to four inches above the top of the highest flue. Putting a few pounds of tallow in a marine boiler, previous to getting up steam, or firing light, when fermentation, or *priming*, as it is frequently called, is likely to occur, are the usual modes of prevention; but the same applied to locomotive boilers, in many instances increase the fermentation in place of lessening it, and there is not any means, that I am aware of, that will prevent it efficiently, otherwise than by frequently blowing out, and by such means clear the boiler of every foreign substance that may have been deposited therein.

It must also be here impressed upon the mind of every individual to whom the care of a steam-engine is entrusted, the very great necessity of a constant sufficiency of water in the boiler, for a volume of steam suddenly formed is attended with considerably *greater danger* than an excess of steam regularly accumulated, as the safety valve will allow part to escape during its formation, and also give warning of its progression, but the valve cannot act so instantly and efficiently as is required if steam be suddenly generated, which, I have no doubt, is the case where some of the plates of a boiler are red hot when the engine is started, and if not the cause of an immediate *explosion*, may be the means of materially injuring the boiler, and render it incapable of withstanding, in safety, the pressure of steam required.

THE FEED PIPE AND FEED PUMP.

Boilers are supplied with water in two distinct forms, namely, by the gravity of the water alone, and by means of a force pump applied to the engine.

C B

D

When a boiler is supplied by the gravity of the water, the pipe attached to the top of the boiler, containing the column of water, is designated the *feed pipe*, the one from the pump being only for the purpose of conveying the water to the top of the feed pipe, the height of which requires to be at least $2\frac{1}{2}$ feet above the surface of the water in the boiler for every pound pressure on a square inch of the safety valve.

To ascertain the capacity of the feed pump.

If the exact consumption and waste of steam, imperfections of the pump, leakages of the boiler, &c., could be properly ascertained, the pump's capacity could easily be determined, but this being impossible, its dimensions can only be regulated by being made sufficiently large not only to keep up the quantity of water which is constantly required, but also to be enabled to meet the greatest contingencies in all ordinary cases of the engine's working: hence observe the following

RULE.—Multiply the area of the piston in feet by its velocity, also in feet per minute, and by three times the quantity of water in a cubic foot of steam, at the required pressure in lbs. per square inch;—divide the product by the length of the pump's stroke in inches multiplied by the number per minute, and the quotient is the pump's area in inches. Or, divide the product by its area, multiplied by the number of strokes per minute, and the quotient is the length of stroke.

EXAMPLE 1.—Required the diameter of feed pump for an engine whose cylinder is 2-feet diameter, length of stroke 4 feet, and making 27 revolutions per minute, or the velocity of the piston equal 216 feet, the pressure of steam equal 4 lbs. per square inch, and the length of the pump's stroke equal 18 inches.

The quantity of water in a cubic foot of steam at 4 lbs. per square inch equal 1.25 cubic inches, (see Table, page 26,) and $1.25 \times 3 = 3.75$.

The area of a cylinder 2 feet diameter = 3.14.

$$18 \times 27 = 486. \quad \text{Hence } \frac{3.14 \times 216 \times 3.75}{486}$$

= 5.23 inches area, or nearly 2.6 inches diam.

2.—Suppose the engine as above described, and existing under similar circumstances of velocity, pressure, &c., but the area of the pump given equal 5.23 inches, required the length of stroke.

$$5.23 \times 27 = 141.21. \quad \text{And } \frac{3.14 \times 216 \times 3.75}{141.21}$$

= 18 inches length of stroke.

NOTE.—The suction and delivering pipes to any pump ought not to be less than two-thirds of the pump's diameter; and in the delivering pipe to the boiler, in high-pressure engines, particularly locomotives, a small cock should be inserted, so as to allow the steam and air which accumulates in the pipes to escape, otherwise the boiler is frequently prevented from being regularly supplied.

OF THE STEAM ENGINE GENERALLY.

Steam engine is a term of general application to all machines in which the steam or vapour of water is the motive power; hence, the usually familiar distinctions, namely, low pressure, or condensing engines; high pressure, or non-condensing; rotatory, which may be either the one or the other; and locomotives, in which steam of great density is required; but, although these distinctions be made for practical convenience, the principles of all are the same.

OF THE CYLINDER.

The cylinder, in whatever denomination of engine, is that in which the motion is produced. It is by the cylinder's capacity that the power of the engine is ascertained; and it is by the length of the stroke, in a great measure, that the piston's velocity is determined; hence, some of the various properties and proportions that cylinders and pipes bear in relation to each other may be

found useful in other respects, besides those immediately connected with the cylinder of a steam engine.

1. A cylinder in its diameter is the most capacious of all plain figures, or contains the greatest area within the same perimeter or outline.

2. The ratio of the diameter is to its circumference as 1 to 3.1416; twice the diameter contains twice the circumference; hence the piston of a large engine has less rubbing surface, or less friction, in proportion to its power, than a small one.

3. The areas of circles are to each other as the squares of their diameters, or as .7854 to 1'. A circle twice the diameter contains four times the area. Hence,

Suppose the circumference and area of a circle be required, the diameter of which is 20 inches.

$$20 \times 3.1416 = 62.832 \text{ inches circumference.}$$

$$20^2 \times .7854 = 314.16 \quad ,, \quad \text{area.}$$

Again, suppose the circumference and area of a circle be required, the diameter of which is 40 inches.

$$40 \times 3.1416 = 125.664 \text{ inches, or twice } 62.832.$$

$$\text{And } 40^2 \times .7854 = 1256.64 \quad ,, \quad \text{or four times } 314.16.$$

The whole capacity of a cylinder equal the product of the area multiplied by the perpendicular height.

Because also, of all circles being in proportion to each other as the squares of their diameters, any number of smaller pipes may be made equal to one of the whole dimensions, and *vice versa*.

Thus, suppose the diameter of a pipe equal 8 inches, required the diameters of two pipes, that shall, united, be of equal area.

$$8^2 = 64 \text{ and } \sqrt{\frac{64}{2}} = 5.65 \text{ inches, the diameter of each.}$$

$$\text{Or, } 5.65^2 \text{ \&c. } \times 2 = \sqrt{64} = 8 \text{ inches.}$$

Not unfrequently, a cylinder, or cylindrical vessel, is required whereby to contain the greatest cubical capacity, and bounded by the least possible superficial surface,—to compute which, observe the following

RULE.—Multiply the given capacity by 2.56, and the cube root of the product equal the diameter, and half the diameter is the depth, in equal terms of unity.

Thus, suppose a vessel of a cylindrical form be required, whose capacity shall equal 600 cubic feet, its bounding surface to be of the least possible dimensions.

$$\sqrt[3]{600 \times 2.56} = 11.5379 \text{ feet diameter.}$$

$$\text{And } 11.5379 \div 2 = 5.76895 \text{ ,, depth.}$$

Again, suppose the vessel is to be constructed with two ends, like that of a cylindrical boiler.

RULE.—Divide four times the required capacity by 3.1416, and the cube root of the quotient equal both the length and diameter, in equal terms of unity.

$$\text{Thus, } \sqrt[3]{\frac{600 \times 4}{3.1416}} = 9.142 \text{ feet in length, and also in diameter.}$$

THE PISTON, AND ITS PROPER VELOCITY.

The velocity of an engine is properly understood as the space passed through by the piston in any given time, whereby to produce a maximum of useful effect; the shorter the stroke, practically, the greater the number of revolutions in any given time, but consequently of diminished power; and the longer the stroke, practically, the greater the velocity, and of course the greater the power, providing the steam can be constantly maintained at a sufficient density; hence, because to the varying purposes to which engines are being constantly applied, it is not of unfrequent occurrence that to the production of equally beneficial effects, when a short stroke must of necessity be introduced, to augment the cylinder's diameter, in order to compensate for diminished velocity.

To determine what is the proper velocity for the piston of a steam engine.

RULE.—Multiply the logarithm of that fraction of the stroke through which the dense steam has been ad-

mitted, by 2.3, to the product of which add 7; multiply the sum by the distance in feet the piston has travelled when the steam is cut off, and 120 times the square root of the product equal the proper velocity for the piston, in feet per minute.

EXAMPLE.—Suppose the steam to be cut off in a 6 feet stroke when the piston has travelled $\frac{1}{3}$ rd of the length, required its proper velocity.

Common logarithm of 3 = 0.47712.1

$$\begin{array}{r}
 2.3 \times \\
 = 1.0973783 \\
 .7 \quad + \\
 = 1.7973783 \\
 \text{feet} \quad 2 \times \\
 \sqrt{3.5947566} = 1.89 \&c. \times 120 \\
 = 226.8 \text{ feet velocity per} \\
 \text{minute.}
 \end{array}$$

Table of nominal velocities at various lengths of strokes.

| STATIONARY ENGINES. | | | MARINE ENGINES. | | | HIGH PRESSURE ENGINES. | | |
|-------------------------------|--------------------|------------------------------|-------------------------------|--------------------|------------------------------|-------------------------------|--------------------|------------------------------|
| Length of stroke in ft. & in. | Number per minute. | Velocity in feet per minute. | Length of stroke in ft. & in. | Number per minute. | Velocity in feet per minute. | Length of stroke in ft. & in. | Number per minute. | Velocity in feet per minute. |
| 1 9 | 46 | 161 | 2 0 | 42 | 168 | 1 0 | 80 | 160 |
| 2 0 | 42 | 168 | 2 3 | 39 $\frac{1}{2}$ | 177 $\frac{1}{2}$ | 1 3 | 70 | 175 |
| 2 3 | 38 | 171 | 2 6 | 38 | 190 | 1 6 | 62 | 186 |
| 2 6 | 35 | 175 | 3 0 | 32 | 192 | 1 9 | 55 | 192 $\frac{1}{2}$ |
| 2 9 | 32 | 176 | 3 3 | 29 $\frac{1}{2}$ | 193 $\frac{1}{2}$ | 2 0 | 50 | 200 |
| 3 0 | 30 | 180 | 3 6 | 27 $\frac{1}{2}$ | 194 $\frac{1}{2}$ | 2 3 | 46 | 207 |
| 3 3 | 28 $\frac{1}{2}$ | 185 $\frac{1}{2}$ | 4 0 | 24 $\frac{1}{2}$ | 196 | 2 6 | 42 $\frac{1}{2}$ | 212 $\frac{1}{2}$ |
| 3 6 | 27 | 189 | 4 3 | 23 $\frac{1}{2}$ | 199 $\frac{1}{2}$ | 2 9 | 39 $\frac{1}{2}$ | 217 $\frac{1}{2}$ |
| 3 9 | 26 | 195 | 4 6 | 22 $\frac{1}{2}$ | 202 $\frac{1}{2}$ | 3 0 | 37 | 222 |
| 4 0 | 25 | 200 | 4 9 | 21 $\frac{1}{2}$ | 204 $\frac{1}{2}$ | 3 3 | 35 | 228 $\frac{1}{2}$ |
| 4 3 | 24 | 204 | 5 0 | 21 | 210 | 3 6 | 33 | 231 |
| 4 6 | 23 | 207 | 5 6 | 19 $\frac{1}{2}$ | 214 $\frac{1}{2}$ | 3 9 | 31 | 232 $\frac{1}{2}$ |
| 5 0 | 21 $\frac{1}{2}$ | 215 | 5 9 | 19 | 218 $\frac{1}{2}$ | 4 0 | 29 $\frac{1}{2}$ | 236 |
| 5 6 | 20 | 220 | 6 0 | 18 $\frac{1}{2}$ | 222 | 4 6 | 27 | 243 |
| 6 0 | 19 | 228 | 6 6 | 17 $\frac{1}{2}$ | 224 $\frac{1}{2}$ | 5 0 | 24 $\frac{1}{2}$ | 247 $\frac{1}{2}$ |
| 7 0 | 17 $\frac{1}{2}$ | 245 | 7 0 | 16 $\frac{1}{2}$ | 231 | 5 6 | 23 | 253 |
| 8 0 | 16 | 256 | 7 6 | 15 $\frac{1}{2}$ | 232 $\frac{1}{2}$ | 6 0 | 22 | 254 |



These are to be considered as the velocities of engines having the application of their power in the usual form. Sometimes the motion is communicated by a lever or half beam, and having the power transmitted from somewhere between the fulcrum and the piston, or end of the lever, in which case the velocity of the piston must be increased proportionally in accordance with the following

RULE.—Multiply the velocities in the table by the length of the lever in feet between fulcrum and piston, and divide the product by the distance between the fulcrum and connecting rod, the quotient is the velocity of the piston in feet per minute.

EXAMPLE.—Suppose a marine engine of this description, with a $3\frac{1}{2}$ feet stroke, length of lever 11 feet, and the connecting rod attached $2\frac{1}{2}$ feet from the piston, required the piston's velocity.

By the table, a 3 feet 6 inches stroke = $194\frac{1}{4}$ feet velocity per minute, and $11 - 3.5 = 8.5$;
 then $\frac{194.25 \times 11}{8.5} = 251.3$ feet, the velocity required.

Of the power or effect of an engine, in the usual form.

Expansibility or increase of bulk being one of the properties of steam, and of the utmost importance in the steam-engine, it is necessary, previous to the attaining an amount of its power, to premise by elucidation of the steam's expansive principles.

In the starting of an engine, the steam has to overcome the friction and inertia of the whole mass ; but after being in motion the impetus it has acquired continues it in that state for a time, independently of the action of the steam, friction being only now to be overcome ; hence if the steam continue to act as forcibly as at first, it will communicate additional motion to the piston, and will, therefore, perform its stroke with

accelerated velocity ; but if the supply of steam is cut off at any part of the stroke, the remainder requires to be effected, partly by the impetus the piston has already acquired, and partly by the expansive property of the steam, its force becoming less just in proportion as the space it occupies increases, thus the motion is in a great measure equalized, the action of the steam in full strength sets it in motion, and the small and decreasing force requisite to continue the motion at a uniform rate is furnished by the expansion of that steam ; and the advantage gained by thus economizing the steam increases, in proportion to its density, and to its being sooner cut off.

To determine the amount of uniform elastic force by expansibility.

RULE.—Divide the length of the stroke in inches by the distance also in inches, that the dense steam has been admitted, and divide the force of the steam in lbs. per square inch by the quotient. Find the logarithm of the first quotient to which add 1 ; multiply the sum by the last quotient, and the product is the uniform force of the steam in lbs. per square inch.

EXAMPLE.—Let the greatest elastic force of steam in the cylinder of an engine equal 48 lbs. per square inch, and let it be cut off from entering the cylinder when the piston has moved $4\frac{1}{2}$ inches, the whole stroke being 18 ; required an equivalent force of the steam throughout the whole stroke.

$$18 \div 4.5 = 4, \text{ and } 48 \div 4 = 12.$$

$$\text{Hyperbolic logarithm of } 4 + 1 = 2.38629.$$

$$\text{Then, } 2.38629 \times 12 = 28.635 \text{ lbs. per square inch, of uniform elastic force.}$$

NOTE.—The uniform force will be on the square, or circular inch, accordingly as the pressure on the piston is taken in square or circular inches.

Table of Hyperbolic Logarithms.

| No. | Log. | No. | Log. | No. | Log. | No. | Log. |
|-----------------|-----------|-----------------|-----------|-----|-----------|-----|-----------|
| 1 $\frac{1}{2}$ | .2231435 | 5 $\frac{1}{2}$ | 1.7491998 | 15 | 2.7080502 | 33 | 3.4965075 |
| 1 $\frac{3}{4}$ | .4054651 | 6 | 1.7917594 | 16 | 2.7725887 | 34 | 3.5263605 |
| 1 $\frac{5}{8}$ | .5596157 | 6 $\frac{1}{4}$ | 1.8325814 | 17 | 2.8332133 | 35 | 3.5553480 |
| 2 | .6931472 | 6 $\frac{1}{2}$ | 1.8718021 | 18 | 2.8903717 | 36 | 3.5835189 |
| 2 $\frac{1}{4}$ | .8109302 | 6 $\frac{3}{4}$ | 1.9095425 | 19 | 2.9444389 | 37 | 3.6109179 |
| 2 $\frac{1}{2}$ | .9162907 | 7 | 1.9459101 | 20 | 2.9957322 | 38 | 3.6375861 |
| 2 $\frac{3}{4}$ | 1.0116008 | 7 $\frac{1}{4}$ | 1.9810014 | 21 | 3.0445224 | 39 | 3.6635616 |
| 3 | 1.0986123 | 7 $\frac{1}{2}$ | 2.0149030 | 22 | 3.0910424 | 40 | 3.6888794 |
| 3 $\frac{1}{4}$ | 1.1186549 | 7 $\frac{3}{4}$ | 2.0476928 | 23 | 3.2354942 | 41 | 3.7135720 |
| 3 $\frac{1}{2}$ | 1.2527629 | 8 | 2.0794415 | 24 | 3.1780538 | 42 | 3.7376696 |
| 3 $\frac{3}{4}$ | 1.3217558 | 8 $\frac{1}{4}$ | 2.1420661 | 25 | 3.2188758 | 43 | 3.7612001 |
| 4 | 1.3862943 | 8 $\frac{1}{2}$ | 2.1972245 | 26 | 3.2580965 | 44 | 3.7841896 |
| 4 $\frac{1}{4}$ | 1.4469189 | 9 | 2.2512917 | 27 | 3.2958368 | 45 | 3.8066624 |
| 4 $\frac{1}{2}$ | 1.5040774 | 9 $\frac{1}{4}$ | 2.3025851 | 28 | 3.3322045 | 46 | 3.8286414 |
| 4 $\frac{3}{4}$ | 1.5581446 | 10 | 2.3978952 | 29 | 3.3672958 | 47 | 3.8501476 |
| 5 | 1.6094379 | 11 | 2.4849066 | 30 | 3.4011973 | 48 | 3.8712010 |
| 5 $\frac{1}{4}$ | 1.6582280 | 12 | 2.5649493 | 31 | 3.4339872 | 49 | 3.8918203 |
| 5 $\frac{1}{2}$ | 1.7047481 | 13 | 2.6390573 | 32 | 3.4657359 | 50 | 3.9120230 |

To determine the proper diameter of a cylinder for an engine of a required power ; Or, to ascertain the power of an engine having a cylinder of a given diameter.

RULE 1.—Multiply 33,000 by the number of horses' power required, and divide the product by the piston's velocity in feet per minute, multiplied by the uniform force of the steam per circular inch, minus 7.85 lbs., and the square root of the quotient equal the cylinder's diameter in inches.

2.—Multiply the square of the cylinder's diameter in inches, by the uniform force of the steam in lbs. per circular inch, minus 7.85 lbs., and by the velocity of the piston in feet per minute; divide the product by 33,000, and the quotient is the amount in horses' power that the engine is equal to.

EXAMPLE 1.—Required the diameter of the cylinder for a condensing engine of 14.4 horses' power, and also the weight on each square inch of the safety valve, in

order to produce steam of 13.37 lbs. uniform elastic force, the steam to be cut off from the cylinder when the piston has moved through 32 inches of its stroke, velocity of the piston 216 feet per minute, resistance and friction 7.85 lbs. per circular inch, or 5.52 lbs. of effective, or uniform force, hence—

$$\frac{33000 \times 14.4}{216 \times 5.52} = \frac{475200}{1192} = \sqrt{400} = 20 \text{ inches diameter.}$$

Again,—Suppose the stroke equal 4 feet, or 48 inches, — $48 \div 32 = 1.5$, and hyperbolic logarithm of 1.5 = 0.40546, to which add 1, = 1.40546; then, $\frac{13.37 \times 1.5}{1.40546}$

= 14.28 lbs., the total force of steam in the boiler per circular inch; and 14.28—11.78, or mean pressure of the atmosphere = 2.5 lbs. effective elastic force or weight upon each circular inch of the safety valve.

EXAMPLE 2.—Suppose it be required to ascertain the effective power of a condensing engine, the following particular requisites of estimation being given, namely, cylinder, 20 inches in diameter; stroke 4 feet, or 216 feet velocity per minute; weight on each circular inch of the safety valve $2\frac{1}{2}$ lbs, or 14.28 lbs., atmospheric pressure included; steam cut off from the cylinder when the piston has passed through 32 inches of its stroke; resistance and friction 7.85 lbs. per circular inch; what is the useful effect of the engine in horses' power.

$$\begin{aligned} 48 \div 32 &= 1.5 \text{ and } 14.28 \div 1.5 = 9.52. \text{—The hyper-} \\ &\text{bolic logarithm of 1.5 plus 1.} = 1.40546 \times 9.52 \\ &= 13.37 \text{ lbs. per circular inch of uniform elastic} \\ &\text{force, and } 13.37 - 7.85 = 5.52 \text{ lbs. of effective} \\ &\text{force; hence,} \\ \frac{20^2 \times 5.52 \times 216}{33000} &= \frac{476928}{33000} = 14.4 \text{ horses' power.} \end{aligned}$$

NOTE.—Condensing engines are governed in a great measure by the amount of vacuum obtained, the mercury in the barometer

attached to the condenser ranging between 24 and 28 $\frac{1}{2}$, or at an average of 26 $\frac{1}{2}$ inches; hence, the mean pressure of the atmosphere being 14.7 lbs. per square inch, and equal to a column of mercury 30 inches in height,—30:14.7::26.25:12.86 lbs. and 14.7—12.86=1.84 or nearly 2 lbs. per square inch remaining under, or acting as a resistance to the piston, besides 8 lbs. per square inch, by which to overcome the friction and inertia of the engine, making the total about 10 lbs. per square inch, or 7.85 lbs. per circular inch on the piston.

In high pressure or non-condensing engines the resistance and friction remain nearly a constant quantity, viz. 18 lbs. per square inch, or 14.1 lbs. per circular inch, including the resistance of the atmosphere.

By an indicator, I am perfectly aware that the above quantities for resistance and friction in a well constructed engine would be found too much; but as the contention generally lays on the purchasing side, it is considered better to let the rules remain so, and if disagreement should still exist, decide by the indicator.

EXAMPLE 3.—What is the power of a non-condensing engine, having a cylinder of 9 inches diameter, a stroke of 2 feet, or 200 feet velocity per minute, and a pressure of steam in the boiler of 40 lbs. per square inch, atmospheric pressure included, the steam to be stopped off from the piston at half stroke, and the resistance, friction, &c. 18 lbs. per square inch, or 14.1 lbs. per circular inch on the piston's area?

40 lbs. per square inch = 31.4 lbs. per circular inch,

$\frac{24}{12} = 2$, and $\frac{31.4}{2} = 15.7$, The hyperbolic logarithm

of 2 plus 1 = 1.693 \times 15.7 = 26.6 lbs. uniform force of the steam per circular inch, and 26.6 — 14.1 = 12.5 lbs. effective force on each circular inch of the piston;

hence, $\frac{9^2 \times 12.5 \times 200}{33000} = 6.1$ horses' power.

EXAMPLE 4.—Let it be required to construct a non-condensing engine of 6.1 horses' power, the uniform elastic force of steam to be 26.6 lbs. per circular inch

in the cylinder, when cut off—at half stroke, piston's velocity 200 feet per minute, resistance and friction 14.1 lbs. per circular inch; required the cylinder's diameter in inches, and also the pressure of the steam on each circular inch of the boiler above the pressure of the atmosphere.

26.6 lbs. elastic force, minus 14.1 resistance and friction, = 12.5 lbs. effective pressure per circular inch; hence,

$$\sqrt{\frac{33000 \times 6.1}{200 \times 12.5}} = 9 \text{ inches diameter.}$$

Again, $\frac{24}{12} = 2$, The hyperbolic logarithm of 2 plus 1 =

$$1.693, \text{ and } \frac{26.6 \times 2}{1.693} = 31.4 - 11.78 = 19.62$$

lbs. per circular inch, or 25 lbs. per square inch in the boiler above the pressure of the atmosphere.

The preceding may be taken as the real effect of an engine, expressed in the usual term, *horses' power*; but, there exist various nominal and approximate rules, whereby the diameter of a cylinder, or power of an engine, is determined, but governed in a great measure by competition,—one maker endeavouring to excel another, by increasing the effect of the engine and retaining the same nominal power, which is not unfrequently supposed the result of superior mechanism, or some very essential interior intricacy, although, generally, at the expense of a larger cylinder, or an increased force of steam.

However, the following are selected as those most commonly used, and what custom has rendered almost a general standard, the more so, no doubt, on account of being considered to have emanated originally from the celebrated firm of Boulton and Watt.

In this rule the steam in the boiler is supposed at a constant pressure of about 3.18 lbs. per square inch, or 2.5 per circular inch; the piston at a constant or uniform velocity of 220 feet per minute; and the effective force on the piston about 7.5 lbs. per square inch, or 5.89 lbs. per circular inch; and under such circumstances 30 circular inches are considered an equivalent to one horse power, when the beam for communicating the motion from the piston is about 3, and the connecting rod not less than 2.5 times the length of stroke.

But marine engines are generally confined, the connecting rods being seldom more than from 1.75 to twice the length of stroke, and, as a compensation for this disadvantage, the area of the piston is augmented to 31.5 circular inches to each horse power.

Again, small packets for rivers, &c., are still more confined, being often compelled to have the connecting rods not more than from 1.25 to 1.5 times the length of stroke, causing a very acute angle with the crank; in such, not fewer than 34 circular inches is considered equal to one horse power.

In high-pressure, or non-condensing engines, one-third the force of the steam is deducted for friction, resistance of the atmosphere, &c.; hence, as in condensing engines, $30 \times 5.89 = 176.7$ lbs. effective pressure equal the amount of one horse power; consequently, steam at 25 lbs. per square inch, or 19.63 lbs. per circular inch, minus $\frac{1}{3}$ rd, $= \frac{19.63 \times 2}{3} = 13.08$ lbs effective pressure on each circular inch of the piston's area, and $176.7 \div 13.08 = 13.6$ circular inches to each horse power.

Steam at 30 lbs. per square inch $= 23.56$ lbs. per circular inch, and $\frac{23.56 \times 2}{3} = 15.7$ lbs. effective pressure;

hence, $176.7 \div 15.7 = 11.3$ circular inches to each horse power.

Steam at 40 lbs. per square inch = 31.41 lbs. per circular inch, and $\frac{31.41 \times 2}{3} = 20.94$ lbs. effective pressure ;
hence $176.7 \div 20.94 = 8.5$ circular inches to each horse power.

Steam at 50 lbs. per square inch = 39.27 lbs. per circular inch, and $\frac{39.27 \times 2}{3} = 26.18$ lbs. effective pressure ;
hence, $176.7 \div 26.18 = 6.8$ circular inches to each horse power ;—and the same at any other pressure that might be required.

Ex. 1.—Required the diameter of a cylinder for a stationary condensing engine of 36 horses' power.

$$\sqrt{36 \times 30} = 32.86 \text{ inches diameter.}$$

Ex. 2.—What is the nominal power of an engine, the cylinder of which is 32.86 inches diameter ?

$$32.86^2 \div 30 = 36 \text{ horses' power.}$$

Ex. 3.—Required the diameter of the cylinder for a marine engine of 65 horses' power.

$$\sqrt{65 \times 31.5} = 45.25 \text{ inches diameter.}$$

Ex. 4.—The diameter of the cylinder of a marine engine is 45.25 inches diameter ; required the nominal power of the engine.

$$45.25^2 \div 31.5 = 65 \text{ horses' power.}$$

Ex. 5.—The force of the steam in a boiler is 30 lbs. per square inch above the pressure of the atmosphere ; if it were applied to a non-condensing engine, so as to produce a power equal to 6 horses, what must be the cylinder's diameter ?

$$\sqrt{11.3 \times 6} = 8.25 \text{ inches diameter.}$$

Ex. 6.—The diameter of the cylinder of a non-condensing engine is 8.25 inches, and the steam at 30 lbs. per square inch, required the engine's power.

$$8.25^2 \div 11.3 = 6 \text{ horses' power.}$$

A Table of the Comparative elastic force of steam on a square or circular inch of a safety valve.

| Steam with an elastic force of | lbs. on a square inch, equal | lbs. on a circular inch, and require to be maintained at a temperature of | 220° F | Steam with an elastic force of | lbs. on a square inch, equal | lbs. on a circular inch, and require to be maintained at a temperature of | 222.5° F |
|--------------------------------|------------------------------|---|--------|--------------------------------|------------------------------|---|----------|
| 2.5 | 1.96 | | 222 | 2.5 | 3.18 | | 224.5 |
| 3 | 2.35 | | 223 | 3 | 3.82 | | 226.5 |
| 3.5 | 2.75 | | 223.5 | 3.5 | 4.45 | | 228.5 |
| 4 | 3.14 | | 225 | 4 | 5.09 | | 230.5 |
| 4.5 | 3.53 | | 227 | 4.5 | 5.73 | | 232.5 |
| 5 | 3.92 | | 228 | 5 | 6.36 | | 234 |
| 5.5 | 4.32 | | 230 | 5.5 | 7.00 | | 235.5 |
| 6 | 4.71 | | 231.5 | 6 | 7.64 | | 236.5 |
| 6.5 | 5.10 | | 233 | 6.5 | 8.27 | | 238.5 |
| 7 | 5.49 | | 234 | 7 | 8.91 | | 239.5 |
| 7.5 | 5.89 | | 235 | 7.5 | 9.55 | | 241 |
| 8 | 6.28 | | 236 | 8 | 10.18 | | 242 |
| 9 | 7.06 | | 239 | 9 | 11.45 | | 244 |
| 10 | 7.85 | | 240 | 10 | 12.73 | | 247 |
| 12 | 9.42 | | 245.5 | 12 | 15.27 | | 252.5 |
| 15 | 11.78 | | 251 | 15 | 19.09 | | 259 |
| 20 | 15.71 | | 260 | 20 | 25.46 | | 270 |
| 25 | 19.63 | | 268 | 25 | 31.83 | | 278.5 |
| 30 | 23.56 | | 275 | 30 | 38.19 | | 294 |
| 35 | 27.49 | | 282 | 35 | 44.56 | | 294 |
| 40 | 31.41 | | 288 | 40 | 50.92 | | 300.5 |
| 45 | 35.34 | | 294 | 45 | 57.20 | | 306 |
| 50 | 39.27 | | 299 | 50 | 63.66 | | 309 |

The preceding questions are very conveniently computed by means of the sliding rule.

1. *By the engineer's improved sliding rule.*—Set 1 upon B to the number of circular inches allowed to a horse power upon A, and against the number of horses' power upon C is the cylinder's diameter in inches upon D; Or, against the cylinder's diameter in inches upon D is the number of horses' power upon C.

Thus, set 1 upon B to 30 upon A, and against any number of horses' power upon C is the diameter in inches upon D, for common condensing engines.

2. *By the common sliding rule.*—Set 1 upon C to the

diameter of a cylinder equal to 1 horse power upon D, and against any diameter upon D is the number of horses' power upon C; Or, against any number of horses' power upon C is the diameter of the cylinder in inches upon D.

NOTE.—The square root of *any number of circular inches to a horse power equal the diameter*;—thus $\sqrt{30}=5.47$ inches,— $\sqrt{81}=9$ inches,— $\sqrt{34}=5.8$ inches, being the diameters of cylinders of 1 horse power, for land and marine condensing engines; And $\sqrt{13.6}=3.7$ inches,— $\sqrt{11.3}=3.4$ inches,— $\sqrt{8.5}=2.9$ inches,—and $\sqrt{6.8}=2.6$ inches, or the diameter of cylinders for non-condensing engines of 1 horse power, with steam above the pressure of the atmosphere equal to 25, 30, 40, and 50 lbs. per square inch.

Ex. 1.—What diameter must a cylinder be for a condensing engine to equal 20 horses' power?

Set 1 upon B to 30 upon A, and against 20 upon C is $24\frac{1}{2}$ upon D.

When the rule is thus set, C is a line of horses' power, and D a line of diameters for cylinders corresponding to that power.

Ex. 2.—What number of horses' power will a high pressure engine be equal to when the cylinder is 12 inches diameter, and steam 30 lbs. per square inch?

Set 1 on B to 11.3 upon A, and against 12 upon D is 12.7 horses' power upon C.

Suppose the same to be required upon the common slide rule,

1.—Set 1 upon C to 5.47 upon D, and against 20 upon C is $24\frac{1}{2}$ upon D.

2.—Set 1 upon C to 3.4 upon D, and against 12 upon D is 12.7 upon C.

Table of the diameters of Cylinders for Steam Engines of Nominal horse's power.

| STATIONARY CONDENSING ENGINES. | | | MARINE ENGINES. | | | HIGH PRESSURE, OR NON-CONDENSING ENGINES. | | | | |
|--------------------------------|----------------------------------|----------------------------|------------------------|----------------------------------|----------------------------|---|---|---------|---------|---------|
| Nominal Horse's Power. | Diameter of Cylinders in inches. | Length of Strokes in Feet. | Nominal Horse's Power. | Diameter of Cylinders in inches. | Length of Strokes in Feet. | Nominal Horse's Power. | Diameters of Cylinders in inches the force of the steam being, per square inch, | | | |
| | | | | | | | 25 lbs. | 30 lbs. | 40 lbs. | 50 lbs. |
| 2 | 9 | 1½ | 10 | 20 | 2 | 1 | 3½ | 3½ | 8 | 2½ |
| 3 | 11 | 2 | 12 | 21½ | 2 | 1½ | 4½ | 4½ | 8½ | 3½ |
| 4 | 12 | 2½ | 15 | 23½ | 2½ | 2 | 5½ | 4½ | 4½ | 3½ |
| 5 | 13½ | 2½ | 16 | 24½ | 2½ | 2½ | 5½ | 5½ | 4½ | 4½ |
| 6 | 14½ | 2½ | 18 | 25½ | 2½ | 3 | 6½ | 6 | 5 | 4½ |
| 8 | 16½ | 3 | 20 | 26½ | 2½ | 3½ | 6½ | 6½ | 5½ | 4½ |
| 10 | 18 | 3½ | 25 | 28½ | 3 | 4 | 7½ | 6½ | 6 | 5½ |
| 12 | 19½ | 3½ | 30 | 31½ | 3 | 4½ | 7½ | 7½ | 6½ | 5½ |
| 14 | 21 | 3½ | 35 | 33½ | 3½ | 5 | 8½ | 7½ | 6½ | 5½ |
| 15 | 21½ | 3½ | 40 | 36½ | 3½ | 5½ | 8½ | 7½ | 6½ | 5½ |
| 16 | 22 | 4 | 45 | 37½ | 3½ | 6 | 9 | 8½ | 7½ | 6½ |
| 18 | 23 | 4½ | 50 | 39½ | 3½ | 6½ | 9½ | 8½ | 7½ | 6½ |
| 20 | 24½ | 4½ | 55 | 40½ | 4 | 7 | 10 | 9 | 7½ | 6½ |
| 22 | 25½ | 4½ | 60 | 43 | 4 | 7½ | 10 | 9½ | 8 | 7½ |
| 24 | 26½ | 4½ | 65 | 44 | 4 | 8 | 10½ | 9½ | 8½ | 7½ |
| 25 | 26½ | 5 | 70 | 46 | 4½ | 8½ | 10½ | 9½ | 8½ | 7½ |
| 26 | 27 | 5 | 75 | 46½ | 4½ | 9 | 11 | 10½ | 8½ | 7½ |
| 28 | 27½ | 5½ | 80 | 48 | 4½ | 10 | 11½ | 11 | 9 | 8½ |
| 30 | 28 | 5½ | 85 | 49 | 4½ | 11 | 12½ | 11½ | 9½ | 8½ |
| 35 | 30½ | 6 | 90 | 50 | 4½ | 12 | 13 | 12 | 10 | 9½ |
| 40 | 32½ | 6 | 95 | 52 | 4½ | 13 | 13½ | 12½ | 10½ | 9½ |
| 45 | 34½ | 6 | 100 | 52½ | 5 | 14 | 14 | 13 | 11 | 10 |
| 50 | 36 | 6½ | 110 | 55 | 5 | 15 | 14½ | 13½ | 11½ | 10½ |
| 55 | 37½ | 6½ | 115 | 56½ | 5 | 16 | 15 | 14 | 12 | 10½ |
| 60 | 39 | 6½ | 120 | 57 | 5½ | 17 | 15½ | 14 | 12½ | 10½ |
| 65 | 40½ | 6½ | 125 | 58 | 5½ | 18 | 16½ | 14½ | 12½ | 11½ |
| 70 | 41½ | 7 | 130 | 59 | 5½ | 19 | 16½ | 14½ | 13 | 11½ |
| 75 | 43 | 7 | 135 | 60 | 5½ | 20 | 16½ | 15 | 13½ | 11½ |
| 80 | 44 | 7½ | 140 | 61 | 5½ | 25 | 18 | 17 | 15 | 13½ |
| 85 | 45½ | 7½ | 145 | 62 | 5½ | 30 | 20 | 19 | 16½ | 14½ |
| 90 | 46 | 8 | 150 | 62½ | 6 | 35 | 21½ | 20½ | 17½ | 15½ |
| 95 | 47½ | 8 | 175 | 67 | 6 | 40 | 23 | 21½ | 18½ | 16½ |
| 100 | 48½ | 8 | 200 | 71 | 6½ | | | | | |
| 110 | 51 | 8 | 250 | 79 | 6½ | | | | | |

Quantity of water for feed, in gals. per minute to each horse power, equal .45 .5 .61 .75

Of the Steam Engine Indicator, its application, &c.

The properly effective power of an engine to any degree of exactitude can only be ascertained through.

the medium of an indicator; that is, an instrument by means of which the effective force of the steam on the piston and extent of vacuum in the cylinder may at all times be equally exhibited. In peculiarity of construction it is simply a small cylinder truly bored, and into which a piston is inserted and loaded by a spring of suitable elasticity to the graduated scale thereon attached.

The action of an indicator is that of describing on a piece of paper attached, a diagram or figure approximating more or less to that of a rectangle, varying of course with the merits or demerits of the engine's productive effect. The breadth or height of the diagram is the sum of the force of the steam and extent of the vacuum; the length being the amount of revolution given to the paper during the piston's performance of its stroke.

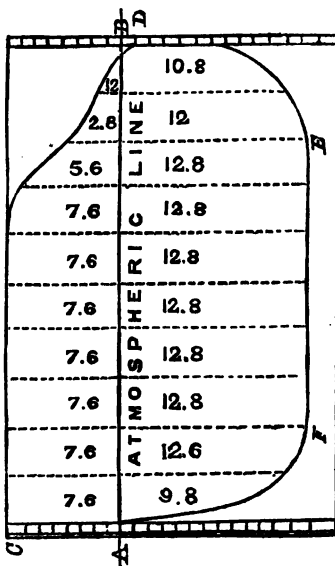
To render the indicator applicable it is commonly screwed into the cylinder cover, and the motion to the paper obtained by means of a sufficient length of small twine attached to one of the radius bars; but such application cannot always be conveniently effected, more especially in engines on the marine principle, hence, other parts of such engines, and other means whereby to effect a proper degree of motion, must unavoidably be resorted to. In those of direct action the cross head is the only convenient place of attachment; but because the length of the engine's stroke is considerably more than the movement required for the paper on the indicator, it is necessary to introduce a pulley and axle, by which means the various movements are qualified to suit each other.

When the indicator is fixed and the movement for the paper properly adjusted, allow the engine to make a few revolutions previous to opening the cock; by which means a horizontal line will be described upon the paper by the pencil attached, and denominated the atmo-

spheric line, because it distinguishes between the effect of the steam and that of the vacuum. Open the cock, and if the engine be upon the descending stroke, the steam will instantly raise the piston of the indicator, and by the motion of the paper with the pencil pressing thereon, the top side of the diagram will be formed.— At the termination of the stroke and immediately previous to its return, the piston of the indicator is pressed down by the surrounding atmosphere, consequently the bottom side of the diagram described, and by the time the engine is about to make another descending stroke, the piston of the indicator is where it first started from, the diagram being completed; hence is delineated the mean elastic action of the steam above that of the atmospheric line, and also the mean extent of the vacuum underneath it.

But in order to elucidate more clearly, by example the following diagram, taken by one of M'Naught's indicators from a marine engine, the steam being cut off after the piston had passed through two-thirds of its stroke, the graduated scale on the indicator tenths of an inch, as shown at each end of the diagram annexed.

Previous to the cock being opened, the atmospheric line A B was formed, and when opened the pencil was



instantly raised by the action of the steam on the piston to C, or what is generally termed the *starting corner*; by the movement of the paper and at the termination of the stroke the line C D was formed, showing the force of the steam and extent of expansion; from D to E show the moments of eduction; from E to F the quality of the vacuum; and from F to A the lead or advance of the valve; thus every change in the engine is exhibited, and every deviation from a rectangle, except that of *expansion* and *lead* of the valve show the extent of proportionate defect. Expansion produces apparently a defective diagram, but in reality such is not the case, because the diminished power of the engine is more than compensated by the saving in steam. Also the lead of the valve produces an apparent defect, but a certain amount must be given, as being found advantageous to the working of the engine, but the steam and eduction corners ought to be as square as possible; any rounding on the steam corner show a defect from want of lead; and rounding on the eduction corner that of the passages or apertures being too small.

To compute the power of an Engine from the Indicator Diagram.

RULE.—Divide the diagram in the direction of its length into any convenient number of equal parts, through which draw lines at right angles to the atmospheric line, add together the lengths of all the spaces taken in measurements corresponding with the scale on the indicator, divide the sum by the number of spaces, and the quotient is the mean effective pressure on the piston in lbs. per square inch.

Let the result of the preceding diagram be taken as an example. Then, the whole sum of vacuum spaces

$\pm 1220 \div 10 = 12.2$ lbs. mean effect obtained by the vacuum; and in a similar manner the mean effective pressure of steam is found to be 6.28 lbs., hence the total effective force $= 18.48$ lbs. per square inch. And supposing 2.5 lbs. per square inch be absorbed by friction, What is the actual power of the engine, the cylinder's diameter being 32 inches, and the velocity of the piston 226 feet per minute?

$18.48 - 2.5 = 15.98$ lbs. per square inch of nett available force.

Then $\frac{32^2 \times .7854 \times 15.98 \times 226}{33000} = 88$ horses' power.

The line under the diagram and parallel to the atmospheric line is $\frac{1}{8}$ ths distant, and represents the perfect vacuum line, the space between showing the amount of force with which the uncondensed steam or vapour resist the ascent or descent of the piston at every part of the stroke.

As the mean pressure of the atmosphere is 15 lbs. per square inch, and the mean specific gravity of mercury 13560, or 2.037 cubic inches equal 1 lb., it will of course rise in the barometer attached to the condenser about 2 inches for every lb. effect of vacuum, and as a pure vacuum would be indicated by 30 inches of mercury, the distance between the two lines shows whether there is or is not any amount of defect, as sometimes there is a considerable difference in extent of vacuum in the cylinder to that in the condenser.

THE CONDENSER, COLD WATER PUMP, AIR PUMP, &c.

When steam is exposed to any degree of cold, its heat is abstracted, its elastic force diminished, and, in proportion to the intensity or quantity of cold, is sooner or later destroyed by condensation, re-assuming its former state as water, by which it is reduced in bulk

nearly 2000 times ; hence its peculiar and advantageous properties in that of the condensing engine.

The usual mode of affecting condensation, whereby to produce a vacuum in the steam engine, is by an intermixture of the steam with that of cold water in a vessel conveniently communicating with the eduction valve from the cylinder, the vessel being so sufficiently formed as to defy any admission of atmospheric air, otherwise than what may be carried in by the steam and by the water, through which condensation of the steam is to be accomplished.

Water is found invariably to contain atmospheric air, and not unfrequently carbonic acid and other gases, which are not destroyed, but merely separated by the caloric or heat necessary to the formation of steam, and with it are carried into the cylinder ; hence the propriety of the Air pump, by which to remove the heated vapours that would thus accumulate in the cylinder to impede the piston's motion, and also to remove the water from the condenser, after its having performed the duty of destroying by absorption the calorific properties of the steam.

The capacity of the condenser ought to be as large as circumstances will conveniently admit, and certainly not less than one-eighth the capacity of the cylinder ; and it ought to be particularly observed in those of marine engines, that where the bottom of condenser and bottom of cylinder are nearly on the same line, care be taken in making the passage between the valves and condenser sufficiently large to contain the condensing water for one stroke of the piston, besides leaving ample communication, otherwise the connexion between the cylinder and air pump will be cut off by water of nearly 100° of heat, on account of the cylinder being twice filled with steam for each effective stroke of the air pump.

To produce the greatest amount of effect in an

engine, the condensed water ought not to exceed in temperature 100° Faht., and to obtain which requires about 30 cubic inches of water, at a mean of temperature for every cubic foot of steam at 220° , to which point it is generally reduced by expansion; but, because of imperfections, uncertainty of temperature, &c., an addition of $\frac{1}{3}$ th, or 35 cubic inches, is the quantity by which to estimate the dimensions of the cold water pump; hence is deduced the following rule.

Divide 90 times the cubical capacity of the cylinder in feet by the pump's length of stroke in inches, and the square root of the quotient equal the diameter of the pump in inches. Or, divide the quotient by the square of the pump's diameter in inches, and the quotient equal the length of stroke.

EXAMPLE.—What diameter of pump is necessary for an engine with a cylinder of 30 inches, or $2\frac{1}{2}$ feet diameter, stroke 6 feet, and the stroke of the pump to equal half the stroke of the engine, or 36 inches?

Area of cylinder = 4.9 square feet.

Then, $\frac{4.9 \times 6 \times 90}{36} = \sqrt{\frac{2646}{36}} = 8.5$ inches diameter.

Or, $\frac{2646}{8.5^2} = 36$ inches, length of stroke.

The capacity of the Air pump is governed in a great measure by the temperature of the water that can be procured for condensation; in some land engines, where water in the locality is scarce, it has of necessity to be used over and over continually; in others of the same description, water can be obtained at a very low degree of temperature, consequently a pump of less capacity is required. Water for like purposes in marine engines is of less fluctuation in temperature; but another matter of contention arise instead, namely, when the paddle wheels are in an instant brought to a greatly reduced

velocity by the shock of a sea, during which time the rush of water into the condenser is not lessened, but becomes considerably accumulated for the next or following stroke of air pump bucket; hence it will be observed that, in practice, little more than approximation can be laid down as a general rule.

To find the proper quantity of water for condensation of steam at a given temperature, the temperatures of the condensing and condensed waters being given.

RULE.—To 1000 add the temperature of the steam, and from the sum subtract the temperature of the condensed water: divide the remainder by the temperature of the condensed water, minus the temperature of the condensing water, and the quotient is the number of times that the quantity for condensation must exceed that from which the steam is formed.

EXAMPLE.—Required the ratio or quantity of water for condensation to 1 of water for the formation of steam, the temperature of the condensing water being 45°, the steam 225°, and that of condensed water 110°.

$$\frac{1000 + 225 - 110}{110 - 45} = \frac{1115}{65} = 17 \text{ times the quantity.}$$

To estimate for the capacity of Air pump, in accordance with common practice.

RULE.—Divide the capacity of the steam cylinder in circular inches by 4 or 5 times, (as necessity may require,) the stroke of air pump also in inches, and the square root of the quotient equal the pump's diameter for land engines. For marine engines take six times the air pump's stroke for a divisor.

EXAMPLE 1.—Required the diameter of an air pump for a land engine, the cylinder of which to be 20 inches diameter, the length of stroke 4 feet or 48 inches, the

stroke of the pump to be half that of the piston, and the divisor to be five times the air pump's stroke.

$$\frac{20^2 \times 48}{5 \times 24} = \sqrt{\frac{19200}{120}} = 12.649 \text{ inches diameter.}$$

EXAMPLE 2.—Suppose it be found that a marine engine, with a cylinder of 36 inches diameter, and stroke of $3\frac{1}{2}$ feet, require an air-pump 20.78 inches diameter, when the stroke of the pump is half that of the piston, but the pump having of necessity to be placed 3 inches farther from the centre of the beam or side lever, required the length of stroke when there situated, and also the diameter, to be that of an equal capacity, to the given diameter at half the stroke of the piston, the beam or levers having a radius of 5 feet, or 60 inches.

The studs for working the pump being placed 3 inches further out than half stroke, of course gives a radius of 33 inches. And as 60:42::33:23.1 inches length of stroke. Hence,

$$\frac{36^2 \times 42}{23.1 \times 6} = \sqrt{\frac{54432}{138.6}} = 19.82 \text{ inches diameter.}$$

OF THE SLIDE VALVE, ECCENTRIC, &c.

The slide valve in a steam engine is a well known contrivance by which, in conjunction with the eccentric, a continuous reciprocating movement of the piston in the cylinder is effected by the alternate admission and eduction of the steam, the principal observations and calculations connected therewith being the following:—

1. *To determine what extent of lap or cover is necessary on the steam side of a slide valve, so as to cut the steam off at any required point of the stroke.*

RULE.—Divide by the length of the piston's stroke in inches the distance the piston has to travel when the steam is cut off; multiply the square root of the quo-

C B

F

tient by half the stroke of the valve, also in inches, and from the product deduct half the lead, the remainder is the lap or cover required.

EXAMPLE.—Suppose an engine, the piston of which to have a stroke of 3 feet or 36 inches, and the steam to be cut off when the piston has moved through 23.4 inches, the travel of the valve being 5 inches, and the lead $\frac{1}{4}$ of an inch, what is the lap or cover required?

$36 - 23.4 = 12.6$ inches, the distance the piston has to travel,

And, $\sqrt{\frac{12.6}{36}} = .5916 \times 2.5$ being half the travel of valve $= 1.479 - .125$, or half the lead, $= 1.354$ inches, the lap or cover required.

2. *To find at what point of the stroke the steam will be cut off by a given lap of valve.*

RULE.—To the lap of the valve on the steam side in inches add half the lead, divide the sum by half the travel of the valve, multiply the square of the quotient by the piston's stroke in inches, and the length of the stroke, minus the last product, equal the distance the piston will have travelled when the steam is cut off.

EXAMPLE.—Let the last example be reversed.

Lap of valve 1.354 inches, half of lead .125 inches, and stroke of piston 36 inches; hence

$$\frac{1.354 + .125}{2.5} = 1.479^2 \times 36 = 12.6 \text{ and } 36 -$$

$12.6 = 23.4$ inches the piston has travelled when the steam is cut off.

3. *To determine a proper amount of lead for the slide valve of a steam engine.*

RULE.—Multiply the square of the cylinder's diameter in inches, by the number of revolutions made

by the crank shaft per minute; cut off from the right hand of the product four figures for decimals; divide the remainder by the length of the steam aperture in inches, and the quotient is the lead in inches that ought to be given to the valve.

EXAMPLE.—Suppose an engine with a cylinder of 30 inches in diameter, number of revolutions per minute, 19, and the length of steam aperture 12 inches.

$30^2 \times 19 = 17100$, and with four figures pointed off for decimals is $\frac{1.7100}{12} = .142$ parts of an inch, the lead required.

NOTE.—The travel of a slide valve equal the width of the two steam openings, plus the lap of the valve over each opening, and the length it will cover, by its movement on the cylinder, equal twice the travel of the valve, plus the distance between the two steam openings.—Observe also, that the apertures for condensing engines ought to be about $\frac{1}{4}$ th, and for non-condensing engines $\frac{1}{8}$ th of the square of the cylinder's diameter, and in all cases, as much of the area in the length as can be practically admitted.

To determine the various peculiarities of throw, travel, &c., that exist between an eccentric and slide valve, when levers intervene.

1. When the travel of the valve, the length of the lever to which the eccentric rod is attached, and the length of the lever by which motion is communicated to the valve, being given, to find the proper amount of eccentricity for the camb, or throw of eccentric.

RULE.—Multiply the travel of the valve by the length of the lever to which the eccentric rod is attached, and divide the product by the length of the lever for communicating motion to the valve, and the quotient is the throw of eccentric.

2. When the travel of the valve, the length of the lever to which the eccentric rod is attached, and also

the throw of eccentric is given, to find what must be the length of the lever for immediate communication with the valve.

RULE.—Multiply the travel of the valve by the length of the lever to which the eccentric rod is attached, and divide the product by the throw of eccentric, the quotient is the length of lever required.

3. When the throw of eccentric, length of lever for immediate communication with the valve, and travel of valve is given, to find the length of the lever to which the eccentric rod is attached.

RULE.—Multiply the throw of eccentric by the length of the lever in immediate connexion with the valve, and divide the product by the travel of the valve, the quotient is the length of lever to which the eccentric rod is attached.

4. When the throw of eccentric, and the lengths of both levers are given, to find the travel of the valve.

RULE.—Multiply the throw of eccentric by the length of the lever which is in immediate connexion with the valve, divide the product by the length of the lever to which the eccentric rod is attached, and the quotient equal the travel of the valve.

NOTE.—It must be observed that all the dimensions are in equal terms of unity, that is, if one dimension be taken in inches, all the others must also be in inches, or, if one is taken in feet, so must all the others be in feet, &c.

Then, suppose for a general example,

The travel of the valve..... = 8 inches
 Length of lever attached to eccentric rod = 6 „
 Length of lever in connexion with valve = 12 „
 Throw of eccentric = 4 „

$$\frac{8 \times 6}{12} = 4 \text{ inches, throw of eccentric.}$$

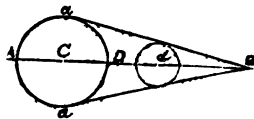
$$\frac{8 \times 6}{4} = 12 \quad \text{,, length of lever in connexion with valve.}$$

$$\frac{4 \times 12}{8} = 6 \quad \text{,, length of lever attached to eccentric rod.}$$

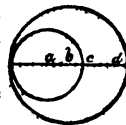
$$\frac{4 \times 12}{6} = 8 \quad \text{,, travel of valve.}$$

The throw of an eccentric, the travel of the valve, also the length of any one lever being given, to find the length of the other geometrically.

On any right line, as A B, describe a circle, A D, equal to the throw of eccentric and travel of valve, then from C as a centre, with a radius equal to the length of lever given, cut the line A B as at d, on which describe a circle equal to the throw of eccentric or travel of valve, as may be required; draw the tangents B a, B a, cutting each other in the line A B, and d B is the length of the lever as required.

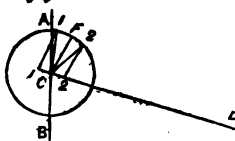


The throw of an eccentric is equal to the sum of twice the distance between the centres of formation and revolution, as a b, or to the degree of eccentricity it is made to describe, as c d.



To find the proper position for an eccentric, in relation to the crank of a steam engine, the angle of eccentric rod and travel of the valve being given.

Draw the right line A B, as the situation of the crank at commencement of the stroke; draw also the line C D, as the proper given angle of eccentric rod with the crank; then from C as centre, describe a circle equal to the travel of the valve; draw the line C F, at right angles to the line C D, draw also the lines 1, 1, and 2, 2, parallel to the



line C F, and at a distance equal to the lap and lead of the valve, draw the angular lines C 1, C 2, which are the angles of eccentric with the crank, for forward or backward motion, as may be required.

NOTE.—The lap of the valve is a certain additional breadth of its face on the steam side, more than sufficient to cover the aperture in the cylinder when the valve is at half stroke; and the lead is properly what the steam aperture is open for admission of the steam, when the piston is at the top or bottom of the cylinder, about to commence the returning stroke.

Of the Beam or Side Levers of a Steam Engine.

The beam of an engine during its motion describes a curve more or less, varying with the radius of the beam and length of the stroke, the deviation from the straight line being the versed sine of the arc described by the beam; hence the determined point for the centre of the cylinder, so that the angles of the links in the parallel motion may be rendered equal, and to effect which observe the following rule:—

To the radius, or half the length of the beam, add half the length of the stroke, multiply the sum by their difference, and from the radius subtract the square root of the product, the remainder equal the versed sine in equal terms of unity.

EXAMPLE.—What is the versed sine to the arc formed by the beam of a steam engine, the radius of the arc, or half the length of the beam being $7\frac{1}{2}$ feet, and the stroke of the piston $5\frac{1}{2}$ feet.

Half the stroke equal 2.75 feet.

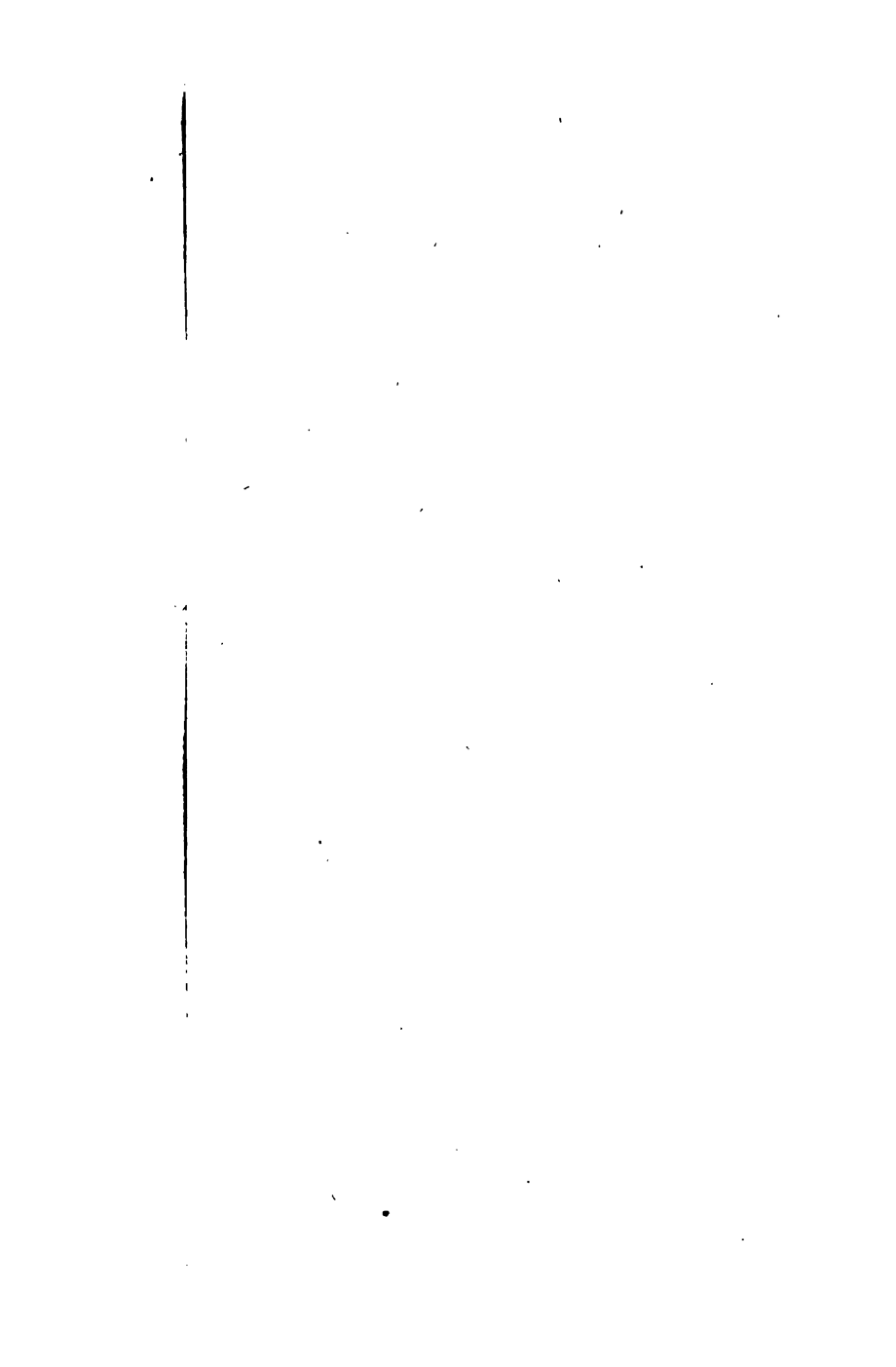
Then, $7.5 + 2.75 = 10.25$ and $7.5 - 2.75 = 4.75$,
hence, $\sqrt{10.25 \times 4.75} = 6.9775$ and $7.5 - 6.9775$
= .5225 of a foot for the versed sine, which
may be reduced to inches and parts,

Thus, .5225

$\times \frac{12}{6.27}$, because 12 inches = 1 foot.

$\times \frac{8}{2.16}$, because 8 parts = 1 inch.
2.16, or $6\frac{1}{8}$ inches nearly.

NOTE.—The length of the beam is generally made three times the length of the stroke.



NS.

FIG. 3⁴⁰. A motion that is chiefly used
in marine Engines.

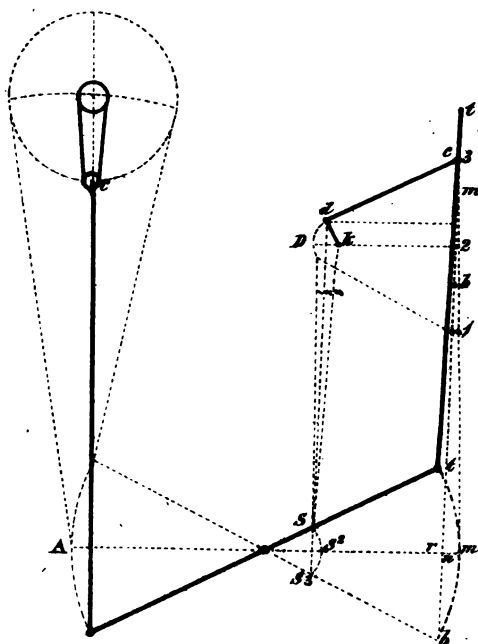


Table of versed Sines to Beams and Strokes of various lengths.

| Radius, or half the length of beam in feet. | Stroke in ft. & in. | Versed Sine in inches. | Radius, or half the length of beam in feet. | Stroke in ft. & in. | Versed Sine in inches. | Radius, or half the length of beam in feet. | Stroke in ft. & in. | Versed Sine in inches. |
|---|---------------------|------------------------|---|---------------------|------------------------|---|---------------------|------------------------|
| | | | | | | | | |
| 3 feet. | 1 6 | 1 $\frac{1}{2}$ | 6 feet. | 3 6 | 3 | 9 feet. | 5 0 | 4 $\frac{1}{2}$ |
| | 1 9 | 1 $\frac{1}{4}$ | | 4 0 | 4 | | 5 6 | 5 $\frac{1}{4}$ |
| | 2 0 | 2 | | 4 6 | 5 | | 6 0 | 6 |
| | 2 3 | 2 $\frac{1}{2}$ | | 5 0 | 6 $\frac{1}{2}$ | | 6 6 | 7 $\frac{1}{2}$ |
| 3 $\frac{1}{2}$ feet. | 2 0 | 1 $\frac{1}{2}$ | 6 $\frac{1}{2}$ feet. | 3 6 | 2 $\frac{1}{2}$ | 9 $\frac{1}{2}$ feet. | 5 0 | 4 |
| | 2 3 | 2 | | 4 0 | 3 | | 5 6 | 4 $\frac{1}{2}$ |
| | 2 6 | 2 $\frac{1}{4}$ | | 4 6 | 3 $\frac{1}{2}$ | | 6 0 | 5 $\frac{1}{4}$ |
| | 2 9 | 2 $\frac{1}{2}$ | | 5 0 | 4 | | 6 6 | 6 $\frac{1}{2}$ |
| 4 feet. | 2 3 | 2 | 7 feet. | 4 0 | 3 $\frac{1}{2}$ | 10 feet. | 5 6 | 4 $\frac{1}{2}$ |
| | 2 6 | 2 $\frac{1}{4}$ | | 4 6 | 4 | | 6 6 | 5 $\frac{1}{4}$ |
| | 2 9 | 2 $\frac{1}{2}$ | | 5 0 | 5 | | 7 0 | 6 |
| | 3 0 | 2 $\frac{3}{4}$ | | 5 6 | 6 | | | 7 $\frac{1}{2}$ |
| 4 $\frac{1}{2}$ feet. | 2 6 | 2 $\frac{1}{2}$ | 7 $\frac{1}{2}$ feet. | 4 0 | 3 $\frac{1}{2}$ | 10 $\frac{1}{2}$ feet. | 5 6 | 4 $\frac{1}{2}$ |
| | 2 9 | 2 $\frac{3}{4}$ | | 4 6 | 4 $\frac{1}{2}$ | | 6 0 | 5 $\frac{1}{2}$ |
| | 3 0 | 3 | | 5 0 | 5 $\frac{1}{2}$ | | 6 6 | 6 $\frac{1}{2}$ |
| | 3 3 | 4 $\frac{1}{2}$ | | 5 6 | 6 $\frac{1}{2}$ | | 7 0 | 7 $\frac{1}{2}$ |
| 5 feet. | 2 9 | 2 $\frac{3}{4}$ | 8 feet. | 4 6 | 4 | 11 feet. | 6 0 | 5 |
| | 3 0 | 3 | | 5 0 | 4 $\frac{1}{2}$ | | 6 6 | 5 $\frac{1}{2}$ |
| | 3 3 | 3 $\frac{1}{4}$ | | 5 6 | 5 | | 7 0 | 6 |
| | 3 6 | 4 | | 6 0 | 6 | | 7 6 | 7 $\frac{1}{2}$ |
| 5 $\frac{1}{2}$ feet. | 3 0 | 3 $\frac{1}{2}$ | 8 $\frac{1}{2}$ feet. | 4 6 | 4 $\frac{1}{2}$ | 12 feet. | 6 6 | 5 $\frac{1}{2}$ |
| | 3 3 | 4 | | 5 0 | 5 | | 7 0 | 6 $\frac{1}{2}$ |
| | 4 0 | 4 $\frac{1}{2}$ | | 5 6 | 5 $\frac{1}{2}$ | | 7 6 | 7 |
| | 4 6 | 5 | | 6 0 | 6 $\frac{1}{2}$ | | 8 0 | 8 |

OF THE PARALLEL MOTION.

The parallel motion in a steam engine is the means employed for the guidance of the piston and rod in a truly rectilinear path, when the effective power of the steam is to be transmitted through the medium of a beam or levers moving upon an axis; hence, various modifications are inevitably required, (*see Table of Parallel Motions*,) but whatever may be the form demanded by the situation, the principle remains the same, and its accuracy entirely depends upon the *radius rods* being of a proper length, for which the following approximate rule will be found sufficiently correct.

RULE.—From the radius of the beam or lever, sub-

tract the length of parallel bar, divide the square of the remainder by the length of the parallel bar, and the quotient is the length of radius rods in equal terms of unity.

EXAMPLE.—Suppose the radius or half length of a beam equal 84 inches, and the length of parallel bar 48 inches, required the length of radius rods,

$$84 - 48 = 36 \text{ and } \frac{36^2}{48} = 27 \text{ inches, length of radius rods.}$$

A Table containing the lengths of Radius Rods for Motions, with Beams and Parallel Bars of various lengths.

| 6 feet. | | 6½ feet. | | 5 feet. | | 4½ feet. | | 4 feet. | | Radius of beams in feet. | |
|----------|-----|----------|-----|---------|-----|----------|-----|---------|-----|--------------------------|------------------------|
| | | | | | | | | | | | Parallel bars in feet. |
| 33 | 33 | 33 | 33 | 21 | 21 | 21 | 21 | 21 | 21 | 2 | 0 |
| 32½ | 32½ | 32½ | 32½ | 20½ | 20½ | 20½ | 20½ | 20½ | 20½ | 1 | 4½ |
| 32 | 32 | 32 | 32 | 20 | 20 | 20 | 20 | 20 | 20 | 0 | 10½ |
| 31½ | 31½ | 31½ | 31½ | 19½ | 19½ | 19½ | 19½ | 19½ | 19½ | 0 | 6½ |
| 31 | 31 | 31 | 31 | 19 | 19 | 19 | 19 | 19 | 19 | 0 | 0 |
| 7 feet. | | | | | | | | | | | |
| 34 | 34 | 34 | 34 | 22 | 22 | 22 | 22 | 22 | 22 | 8 | 1½ |
| 33½ | 33½ | 33½ | 33½ | 21½ | 21½ | 21½ | 21½ | 21½ | 21½ | 7½ | 8 |
| 33 | 33 | 33 | 33 | 21 | 21 | 21 | 21 | 21 | 21 | 7 | 13½ |
| 32½ | 32½ | 32½ | 32½ | 20½ | 20½ | 20½ | 20½ | 20½ | 20½ | 6½ | 9 |
| 32 | 32 | 32 | 32 | 20 | 20 | 20 | 20 | 20 | 20 | 6 | 0 |
| 8 feet. | | | | | | | | | | | |
| 35 | 35 | 35 | 35 | 23 | 23 | 23 | 23 | 23 | 23 | 10 | 0 |
| 34½ | 34½ | 34½ | 34½ | 22½ | 22½ | 22½ | 22½ | 22½ | 22½ | 9½ | 8½ |
| 34 | 34 | 34 | 34 | 22 | 22 | 22 | 22 | 22 | 22 | 9 | 8 |
| 33½ | 33½ | 33½ | 33½ | 21½ | 21½ | 21½ | 21½ | 21½ | 21½ | 8½ | 11 |
| 33 | 33 | 33 | 33 | 21 | 21 | 21 | 21 | 21 | 21 | 8 | 11½ |
| 9 feet. | | | | | | | | | | | |
| 36 | 36 | 36 | 36 | 24 | 24 | 24 | 24 | 24 | 24 | 11 | 0 |
| 35½ | 35½ | 35½ | 35½ | 23½ | 23½ | 23½ | 23½ | 23½ | 23½ | 10½ | 8½ |
| 35 | 35 | 35 | 35 | 23 | 23 | 23 | 23 | 23 | 23 | 10 | 8 |
| 34½ | 34½ | 34½ | 34½ | 22½ | 22½ | 22½ | 22½ | 22½ | 22½ | 9½ | 11½ |
| 34 | 34 | 34 | 34 | 22 | 22 | 22 | 22 | 22 | 22 | 9 | 12 |
| 10 feet. | | | | | | | | | | | |
| 37 | 37 | 37 | 37 | 25 | 25 | 25 | 25 | 25 | 25 | 12 | 0 |
| 36½ | 36½ | 36½ | 36½ | 24½ | 24½ | 24½ | 24½ | 24½ | 24½ | 11½ | 8½ |
| 36 | 36 | 36 | 36 | 24 | 24 | 24 | 24 | 24 | 24 | 11 | 8 |
| 35½ | 35½ | 35½ | 35½ | 23½ | 23½ | 23½ | 23½ | 23½ | 23½ | 10½ | 11½ |
| 35 | 35 | 35 | 35 | 23 | 23 | 23 | 23 | 23 | 23 | 10 | 12 |
| 11 feet. | | | | | | | | | | | |
| 38 | 38 | 38 | 38 | 26 | 26 | 26 | 26 | 26 | 26 | 13 | 0 |
| 37½ | 37½ | 37½ | 37½ | 25½ | 25½ | 25½ | 25½ | 25½ | 25½ | 12½ | 8½ |
| 37 | 37 | 37 | 37 | 25 | 25 | 25 | 25 | 25 | 25 | 12 | 8 |
| 36½ | 36½ | 36½ | 36½ | 24½ | 24½ | 24½ | 24½ | 24½ | 24½ | 11½ | 11½ |
| 36 | 36 | 36 | 36 | 24 | 24 | 24 | 24 | 24 | 24 | 11 | 12 |
| 12 feet. | | | | | | | | | | | |
| 39 | 39 | 39 | 39 | 27 | 27 | 27 | 27 | 27 | 27 | 14 | 0 |
| 38½ | 38½ | 38½ | 38½ | 26½ | 26½ | 26½ | 26½ | 26½ | 26½ | 13½ | 8½ |
| 38 | 38 | 38 | 38 | 26 | 26 | 26 | 26 | 26 | 26 | 13 | 8 |
| 37½ | 37½ | 37½ | 37½ | 25½ | 25½ | 25½ | 25½ | 25½ | 25½ | 12½ | 11½ |
| 37 | 37 | 37 | 37 | 25 | 25 | 25 | 25 | 25 | 25 | 12 | 12 |

To obtain the proper lengths of Connecting Rods, Side Rods, &c.

1. The proper length for the connecting rod of a beam engine is the perpendicular distance between the centre of beam and centre of fly wheel shaft.

2. The proper lengths for the side rods of a lever engine is the perpendicular distance between centre of lever, and centre of piston crosshead at half stroke.

3. The proper lengths for connecting rods of direct action engines, is the distance between the centre of crank axle, and centre of piston crosshead at half stroke.

4. The proper length for an eccentric rod is the distance between the centre of fly wheel shaft, or centre of revolution, and centre of stud in traverse shaft, when the valve is at half stroke.

OF THE FLY WHEEL.

The fly wheel is a heavy circular ring, generally of cast iron, and for the purpose of equalizing the motion of the engine, by absorbing the surplus force at one part of the action to distribute it again when the action is deficient. Its diameter is from 3 to $3\frac{1}{2}$ times the length of the stroke, and for safety should not exceed, in the velocity of its rim, 12 feet per second.

Numerous rules exist amongst engineers by which to determine the proper weight for the rim of a wheel of given diameter and velocity, some of less and others of more complexity in their mode of calculation; but the following I have selected for its simplicity, and probably equal efficiency to any of those professedly of more minute investigation.

RULE.—Divide 1400 times the number of horses' power the engine is equal to, by the diameter of the wheel in feet, multiplied by the number of revolutions per minute, and the quotient is the weight of the ring or rim of the wheel in cwts.

EXAMPLE.—Required the weight proper for the rim of the fly wheel to an engine of 30 horses' power, the diameter to be 25 feet, and to make 18 revolutions per minute :

$$\frac{1400 \times 30}{25 \times 18} = \frac{42000}{450} = 93.3 \text{ cwts.}$$

The following rule from Tredgold is comparatively simple, and may be used without taking the power of the engine into account.

RULE.—Multiply 40 times the pressure on the piston in lbs. by the radius of the crank in feet,—divide the product by the cube of the radius of the wheel in feet, multiplied by its revolutions per minute, and the quotient is the sectional area of the rim in inches.

EXAMPLE.—Suppose a cylinder of 30 inches diameter, steam at 18 lbs. per square inch, radius of crank 3 feet, diameter of wheel 25 feet, velocity 18 revolutions per minute: required the sectional area of the rim.

Area of piston = 706 inches.

$$\frac{706 \times 18 \times 40 \times 3}{12.5^3 \times 18} = \frac{1524960}{35154} = 43 \text{ inches,}$$

the cross sectional area.

To determine the dimensions of the ring, suitable to a given weight in cast iron.

RULE 1.—Make the breadth in inches about equal to the square root of the weight in cwts.

2.—Add together the inside and outside diameters of the ring in inches, multiply the sum by their difference, and by .2065 for a divisor, by which divide the required weight in lbs., and the quotient is the thickness of the ring in inches. Thus,—Suppose the weight and diameter of the wheel as above; required the breadth and thickness.

$$\sqrt{93.3} = 9.7 \text{ inches, breadth of ring, or say } 9\frac{1}{2},$$

Then, $25 \times 12 = 300$ inches, and
 $93.3 \times 112 = 10449.6$ lbs.
 $300 - 19 = 281$, or inside diameter.
 $300 + 281 \times 19 \times .2065 = 2279.6$,
 And, $\frac{10449.6}{2279.6} = 4.5$ inches in thickness.

Or, if the ring be required of a cylindrical form, multiply the square root of the cross sectional area by 1.12837, and the product is the diameter. Hence,

$$\sqrt{9.5 \times 4.5 \times 1.12837} = 7.38 \text{ inches diameter.}$$

When a fly wheel is not of sufficient weight, and the momentum is to be obtained by increased velocity, to find the proper velocity required.

RULE.—Multiply the required momentum of the wheel by the given number of revolutions per minute, and divide the product by the weight of the wheel ring or rim given, the quotient equal the number of revolutions required for the wheel per minute.

EXAMPLE.—Let the weight of a fly wheel rim equal 43.3 cwt., with a velocity of 20 revolutions per minute, required the proper velocity, so that the momentum may be increased equal to 65 cwt., by using the same wheel.

$$\frac{65 \times 20}{43.3} = 30 \text{ revolutions per minute.}$$

When an engine requires a fly wheel of a known weight at a given number of revolutions per minute, to find what weight of rim will be required when the velocity is either to be increased or diminished.

RULE.—Multiply the given weight of rim, by the given velocity per minute, divide the product by the required velocity or number of revolutions per minute, and the quotient is the weight of the rim in equal terms of unity.

EXAMPLE.—Suppose the required weight for the rim of a fly wheel be 65 cwt., at 20 revolutions per minute ; but of necessity the motion is compelled to be increased to 30 revolutions per minute ; required the weight, the rim of the wheel must be equal to

$$\frac{65 \times 20}{30} = 43.3 \text{ cwt. for the weight of the rim.}$$

THE GOVERNOR, OR REGULATOR,

Is a necessary appendage attached to land or stationary engines, for the purpose of regulating the quantity of steam according to the quantity of work, and thereby causing a uniformity of motion, which otherwise would not be the case.

Governors are variously constructed, to suit the different situations in which they require to be placed, but their general principle is the same, and consists of a double pendulum attached to, and made to revolve round on a spindle by the power of the engine ; consequently, the pendulums ought to be of a certain length to correspond to a given velocity,—Or, the velocity made to correspond with pendulums of a given length, Hence, according to the nature of a pendulum, the square root of its length multiplied by the number of vibrations in a given time equal a number by which the length and number of vibrations of other pendulums are regulated ; thus, a pendulum that will vibrate seconds, or 60 in the latitude of London, is 39.1393 inches long ; and $\sqrt{39.1393 \times 60} = 375.36$, or, for the purposes of a governor, 375 ; and hence,

RULE 1.—Divide 375 by the square root of the pendulum's length, and the quotient equal the vibrations per minute, Or half the quotient equal the number of revolutions in the same time.

2.—Divide 375 by twice the number of revolutions

per minute, and the square of the quotient equal the pendulum's length in inches.

EXAMPLE 1.—Required the number of revolutions per minute for a governor with pendulums 30 inches in length.

$$\frac{375}{\sqrt{30}} = 68.5 \div 2 = 34.25 \text{ revolutions per minute.}$$

Ex. 2.—Required the length of pendulums for a governor to make 47 revolutions per minute.

$$\frac{375}{47 \times 2} = 3.99^3 = 15.92 \text{ inches in length.}$$

The motion of a governor is generally derived from the fly wheel shaft of an engine, and communicated by means of pulleys, wheels, &c.; therefore, *to find the diameter of a pulley, or number of teeth in a wheel to produce any required velocity*, observe the following

RULE.—Multiply the diameter of the pulley, or number of teeth in the wheel on the governor spindle, by the velocity of the governor, or number of revolutions per minute, and divide by the velocity or number of revolutions of the engine in the same time; the quotient is the pulley's diameter, or number of teeth in the wheel on the fly wheel shaft. Or, multiply the velocity of the engine per minute by the diameter of the pulley, or number of teeth in the wheel on the fly wheel shaft, and divide by the required velocity of the governor; the quotient is the pulley's diameter or number of teeth in the wheel on the governor spindle.

EXAMPLE.—Required the diameter of a pulley for the spindle of a governor, so that it may perform 36 revolutions per minute; velocity of the engine 22, and the pulley on the fly wheel shaft 18 inches diameter.

$$\frac{22 \times 18}{36} = 11 \text{ inches diameter.}$$

Ex. 2.—Suppose an engine and governor situated as follow :—

Velocity of the engine 34 revolutions per minute,

Velocity of the governor 52 revolutions per minute,

Diameter of pulley on fly wheel shaft 16 inches,

Diameter of pulley on intermediate shaft 12 inches,

Wheel on governor spindle 40 teeth ;

Required the number of teeth in the wheel on the intermediate shaft.

$$\frac{52 \times 40 \times 12}{34 \times 16} = 46 \text{ teeth.}$$

Ex. 3.—Again, suppose the engine and governor situated as above ; required the diameter of the pulley on the intermediate spindle.

$$\frac{34 \times 16 \times 46}{52 \times 40} = 12 \text{ inches diameter.}$$

NOTE.—The weight of the balls in lbs. ought to be about $1\frac{1}{2}$ times the length of the pendulums in inches, and the levers to the throttle valve ought to be so adjusted that the greatest angle of the pendulums with the spindle may not exceed 45 degrees.

On the proper Management of a Steam Engine.

In the duties of an engineer, one of the most important is that of properly qualified attention to the boiler, it being not only that portion of the structure from which the most dangerous consequences may arise, but it is that, also, in which the vital principle of the engine is generated and supported :—

Every individual, before being considered duly qualified to undertake the care of a steam engine, ought to be perfectly intimate with the following necessitous points connected therewith.

1.—That it is of the most essential consequence to see that every accessible portion of the boiler is kept thoroughly clean, as on this, in a great measure,

depends its entire preservation and beneficial results to the economic production of steam.

2.—That the flues or tubes be also kept clean and all tight; as a trifling leak soon destroys the boiler by oxidation, and accumulated soot prevents the generation of steam, by the prevention of heat to the water.

3.—That the mud and man-hole doors are properly situated and securely screwed up; as many accidents have occurred through apparent inattention to this important point; in some instances the cross bars have not been properly situated, in other instances the threads of the screws have been rendered imperfect by oxidation, and not renewed. But let it be one undeviating maxim, that when steam is up, if a mud-hole door leak, never attempt to screw it up, but rather wait until the boiler is empty, then see that the joint is made properly.

4.—That all cocks, or tubes, by which the quantity of water in the boiler is indicated, be free of mud or accumulation of scale, so as not, in the slightest degree, to intercept a free passage to the water.

5.—That the boiler be filled to a proper height with water, as pure as possible, that is, free from saline substances or earthy matters, both of which are exceedingly detrimental to a boiler.

6.—That the float, (if any) by which to govern the quantity of feed water admitted into the boiler, be entirely free to rise or fall by its own gravity, with any fluctuation of the water.

7.—That the safety valve is properly adjusted, and instantly buoyant, when the pressure of steam arrives at the calculated force indicated by the steam gauge.

8.—That the fire bars are kept constantly covered with the fuel, at as near as possible a uniform thickness, and the steam maintained at a proper height, observing to open the fire doors as seldom as possible.

These observations being applicable to the welfare of all boilers whatever; but further, in respect to marine boilers, where sea water is used, great attention is required on the part of the engineer on watch, to see that the feed is so set that it may, from the lowest point of water carried therein, accumulate so as to reach the top of the gauge glass twice every watch, or once every two hours, and as regularly blown out to where it began to accumulate; if this be not properly attended to, the water may become super-saturated, and a deposit of salt formed upon the plates, in which the caloric will be retained, causing them, by its detention, to become red hot; ultimately, and not without danger, the boiler may be destroyed.

In some vessels boilers are supplied with what are termed *brine pumps*, they being for the purpose of withdrawing from the boilers all water impregnated with salts, to a certain extent; but, it being found in practice that reliance cannot always be placed in them, it is prudent, and more satisfactory, to use occasionally an hydrometer, to test by the gravity of the water their qualified action.

Saturated water contains about $\frac{1}{3}$ parts of salt, but reckoning the saltiness of sea water 1. that which is in the boiler should never, if possible, exceed 4. or $\frac{4}{3}$ parts of salt.

Engineers ought also to be familiar with what steps to pursue in the case of boilers priming or fermenting, this being found frequently to take place, especially in those that are short of steam room, and, occasionally, in changing from fresh to salt water, or from salt to fresh, particularly if the water is muddy; such cases require generally a partial closing of the throttle valves, also a diminution of the supply of injection, and opening of the furnace doors. But if the priming continue to defy all such means resorted to, as in some instances.

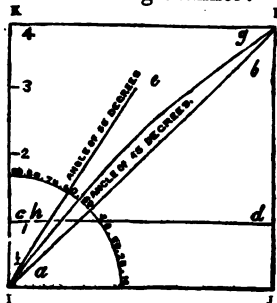
I have witnessed, then, of necessity, damp the fires with water, taking due precaution not to stand opposite the doors, whereby to catch the effects of scalding, by the rush of steam unavoidably formed in the furnace. Drawing the fires is a more preferable determination, if time can be obtained, but sometimes the diminution of water in the gauge glass is so rapid, that delay, to effect such a purpose, is unsafe. If, by neglect or otherwise, the plates of the furnaces should become red hot, through deficiency of water in the boiler, water should not, by any means, be thrown upon them whilst in that state, neither ought the safety valve to be opened, as pernicious consequences would, in all probability, be the ultimate result.

The engine of itself requires little of intricate attention, but it is necessary that every engineer should be possessed of a properly qualified knowledge of the nature and actual utility of the various parts of which the machine is composed, and also of a ready conceptive mind, formed by studious investigation and a jealous watchfulness to probable consequences likely to arise through any sudden derangement, which sometimes unavoidably takes place, and most frequently where the means of renewal or that of obtaining a proper repair is quite inaccessible. Proper attention to all the bearings is particularly necessary, so as to guard against their becoming hot, and causing to them ultimate destruction by tearing or cutting of their surfaces. Attention to all the packings is also particularly necessary, and to see that no portion of air whatever be admitted, so as to destroy the effects of the vacuum in any degree; and the temperature of the condenser, or the condensed water, ought never, if possible, to exceed 100° Fahrenheit. These remarks, and a due care to lubrication, are the chief demands that the engine requires in all ordinary cases of working.

OF THE SCREW, AS A PROPELLER.

The screw, as a mode of propelling steam vessels, is now assuming so much importance that it requires a brief notice, although the conflicting results which have been obtained by different engineers precludes the possibility at present of giving any well-ascertained proportions. This propeller is generally placed in the dead wood of the vessel, just before the rudder, and the shaft is parallel to the keel.

The most approved screws are of two kinds: that having a uniform pitch or angle, and that which has a varying angle, invented by Mr. Woodcroft. The first is set off by describing a line round a cylinder at a uniform angle to the axis. In the second, the angle is continually increasing, and is set off by Mr. Woodcroft in the following manner:—Draw a right line equal to

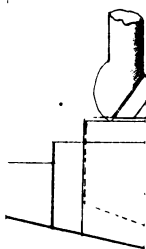


the direct length of the spiral required, as IJ , and on which describe the square $IJKL$; draw the diagonal line IL , which line will form an angle with the line IJ of 45 degrees; divide the side IK of the square into four equal parts, and through the first of which draw the line cd

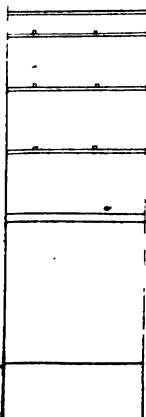
parallel to the line IJ ; from the angle I of the square draw the line Ie at an angle of 55 degrees with the line IJ , and where the line Ie intersects the horizontal line cd at the point h , it gives a point through which the segment of a circle fg must be drawn from the angle I to the angle L of the square $IJKL$. If then the paper or other medium upon which this segment of a circle fg is drawn be transferred to or rolled upon a cylinder,

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then will the line fg point out upon the cylinder the outer circumference of the spiral worm required.

To determine the proper pitch for a screw propellor, the velocity of the screw, the speed of the vessel, and assumed slip of the screw being given.

RULE.—Divide the velocity of the vessel, plus the assumed slip in feet per minute by the number of revolutions the screw is intended to make in the same time, the quotient will be the pitch of the screw in feet.

EXAMPLE.—Suppose the intended speed of a vessel to be 10 miles per hour, the expected slip 2 miles, and the revolutions of the screw 120 per minute.

10 miles per hour = 860 feet per minute, and
 2 " " " = 172 " " " then
 $120 : 860 + 172 :: 1 : 8.6$ feet, the pitch required.

To determine the amount of loss by slip, the speed of the vessel, the revolutions of the screw per minute, and the pitch of the screw being given.

RULE.—Multiply the pitch of the screw by the number of revolutions per minute, and from the product subtract 88 times the speed of the vessel in English miles per hour, and the remainder will be the loss by slip in feet per minute.

EXAMPLE.—Suppose the ascertained speed of a vessel propelled by a screw of 8.8 feet pitch is found to be 10 English miles per hour, how much is lost by slip, the screw making 120 revolutions per minute :—

$10 \times 88 = 880$ and $120 \times 8.8 = 1056$; Then, $1056 - 880 = 176$ feet per minute, or 2 miles per hour.

To ascertain the amount of helical surface in one convolution of a screw.

RULE.—Multiply the radii of the screw by the radii minus the radii of its shaft, or centre, the product is the

difference of their squares ; then multiply the difference of their squares by the constant number 3.1416, and that product by the secant of the angle of the screw, the result is the area of the helical surface in square feet.

EXAMPLE.—Suppose the radii of a screw equal 8 feet, the diameter of its centre 2 feet, and the angle of inclination 27 degrees, required the helical surface.

$8 \times 7 = 56 \times 3.1416 \times 1.1222 = 197.4458$ square feet.

The distance which a screw traverses while working in a solid, and making one revolution, is called the *pitch* ; and the difference between the pitch, and the actual distance which a vessel would proceed while the screw made one revolution, is called the *slip*.

The usual method of working the screw, is to place the ordinary marine engine in the centre of the vessel, and connect it, by spur wheels, to a horizontal shaft to which the screw is attached. This shaft is made to revolve much faster than the engines, to give a great velocity to the screw.

Mr. Grantham, of this town, has, however, adopted a plan by which the spur wheels are removed, and the engines applied direct to the screw shaft. This system offers so many advantages, and has been attended with so much success, that we have given a plate to show the mode of applying it.

Table of Approximate Rules for practical purposes.

- Diameter of a circle $\times 3.1416$ = the circumference.
 Circumference „ $\times .31831$ = the diameter.
 Diameter „ $\times .8862$ = the side of an equal square.
 Diameter „ $\times .7071$ = the side inscribed square.
 Side of a square $\times 1.128$ = the diameter of an equal circle.
 Square of diameter $\times .7854$ = the area of the circle.
 Square root of area $\times 1.12837$ = the diam. of equal circle.
 Square of the diam. of a sphere $\times 3.1416$ = convex surface.
 Cube of the diameter of a sphere $\times .5236$ = the solidity.
 Diameter of a sphere $\times .806$ = dimensions of equal cube.
 Diameter of a sphere $\times .6667$ = length of equal cylinder.
 Square inches $\times .00695$ = square feet.
 Cubic inches $\times .00058$ = cubic feet.
 Cubic feet $\times .03704$ = cubic yards.
 Circular inches $\times .00456$ = square feet.
 Cylindrical inches $\times .0004546$ = cubic yards.
 Cylindrical feet $\times .02909$ = cubic yards.
 Lineal feet $\times .00019$ = English miles.
 Lineal yards $\times .000568$ = English miles.
 Square yards $\times .0002067$ = English acres.
 Avoirdupois lbs. $\times .009$ = cwts.
 Avoirdupois lbs. $\times .00045$ = tons.
 Cubic feet $\times 6.232$ = imperial gallons.
 Cubic inches $\times .003607$ = imperial gallons.
 French metres $\times 3.281$ = English feet.
 ——— litres $\times .2202$ = imperial gallons.
 ——— grammes $\times .002205$ = avoirdupois lbs.
 ——— kilogrammes $\times 2.205$ = avoirdupois lbs.
 183.346 circular inches = 1 square foot.
 2200 cylindrical inches = 1 cubic foot.

Table of Natural Sines, Co-sines, Tangents, Co-tangents, Secants, and Co-secants, to every degree of the Quadrant.

| Deg. | Sines. | Co-sines. | Tang. | Co-tang. | Secants. | Co-sec. | Deg. |
|------|----------|-----------|----------|----------|----------|----------|------|
| 0 | .00000 | 1.00000 | .00000 | Infinite | 1.00000 | Infinite | 90 |
| 1 | .01745 | .99985 | .01746 | 57.2900 | 1.00015 | 57.2987 | 89 |
| 2 | .03490 | .99939 | .03492 | 28.6363 | 1.00061 | 28.6537 | 88 |
| 3 | .05234 | .99863 | .05241 | 19.0811 | 1.00137 | 19.1073 | 87 |
| 4 | .06976 | .99756 | .06993 | 14.3007 | 1.00244 | 14.3356 | 86 |
| 5 | .08716 | .99619 | .08749 | 11.4301 | 1.00382 | 11.4737 | 85 |
| 6 | .10453 | .99452 | .10510 | 9.51236 | 1.00551 | 9.56677 | 84 |
| 7 | .12187 | .99255 | .12278 | 8.14435 | 1.00751 | 8.20551 | 83 |
| 8 | .13917 | .99027 | .14054 | 7.11537 | 1.00983 | 7.18530 | 82 |
| 9 | .15643 | .98769 | .15830 | 6.31375 | 1.01246 | 6.39245 | 81 |
| 10 | .17365 | .98481 | .17633 | 5.67128 | 1.01543 | 5.75877 | 80 |
| 11 | .19081 | .98163 | .19438 | 5.14455 | 1.01872 | 5.24084 | 79 |
| 12 | .20791 | .97815 | .21256 | 4.70463 | 1.02234 | 4.80973 | 78 |
| 13 | .22495 | .97437 | .23087 | 4.33148 | 1.02630 | 4.44541 | 77 |
| 14 | .24192 | .97030 | .24933 | 4.01078 | 1.03061 | 4.13356 | 76 |
| 15 | .25882 | .96593 | .26795 | 3.78205 | 1.03528 | 3.86370 | 75 |
| 16 | .27564 | .96126 | .28675 | 3.48741 | 1.04030 | 3.62796 | 74 |
| 17 | .29237 | .95630 | .30673 | 3.27085 | 1.04569 | 3.42030 | 73 |
| 18 | .30902 | .95106 | .32492 | 3.07768 | 1.05146 | 3.23607 | 72 |
| 19 | .32557 | .94552 | .34433 | 2.90421 | 1.05762 | 3.07155 | 71 |
| 20 | .34202 | .93969 | .36397 | 2.74748 | 1.06418 | 2.92390 | 70 |
| 21 | .35837 | .93358 | .38386 | 2.60509 | 1.07114 | 2.79043 | 69 |
| 22 | .37461 | .92718 | .40403 | 2.47509 | 1.07853 | 2.66947 | 68 |
| 23 | .39073 | .92050 | .42447 | 2.35585 | 1.08636 | 2.55930 | 67 |
| 24 | .40674 | .91355 | .44523 | 2.24604 | 1.09464 | 2.45859 | 66 |
| 25 | .42262 | .90631 | .46631 | 2.14451 | 1.10338 | 2.36620 | 65 |
| 26 | .43837 | .89879 | .48773 | 2.05030 | 1.11260 | 2.28117 | 64 |
| 27 | .45399 | .89101 | .50952 | 1.96261 | 1.12233 | 2.20869 | 63 |
| 28 | .46947 | .88295 | .53171 | 1.88073 | 1.13257 | 2.13005 | 62 |
| 29 | .48481 | .87462 | .55431 | 1.80405 | 1.14335 | 2.06266 | 61 |
| 30 | .50000 | .86603 | .57735 | 1.73205 | 1.15470 | 2.00000 | 60 |
| 31 | .51504 | .85717 | .60086 | 1.66428 | 1.16663 | 1.94160 | 59 |
| 32 | .52992 | .84805 | .62487 | 1.60033 | 1.17918 | 1.88708 | 58 |
| 33 | .54464 | .83867 | .64941 | 1.53986 | 1.19236 | 1.83608 | 57 |
| 34 | .55919 | .82904 | .67451 | 1.48256 | 1.20622 | 1.78829 | 56 |
| 35 | .57358 | .81915 | .70021 | 1.42815 | 1.22077 | 1.74345 | 55 |
| 36 | .58778 | .80902 | .72654 | 1.37638 | 1.23607 | 1.70130 | 54 |
| 37 | .60181 | .79863 | .75355 | 1.32704 | 1.25214 | 1.66164 | 53 |
| 38 | .61566 | .78801 | .78129 | 1.27994 | 1.26902 | 1.62437 | 52 |
| 39 | .62932 | .77715 | .80978 | 1.23490 | 1.28676 | 1.58902 | 51 |
| 40 | .64279 | .76604 | .83910 | 1.19175 | 1.30541 | 1.55572 | 50 |
| 41 | .65606 | .75471 | .86929 | 1.15037 | 1.32511 | 1.52425 | 49 |
| 42 | .66913 | .74314 | .90040 | 1.11061 | 1.34561 | 1.49448 | 48 |
| 43 | .68200 | .73135 | .93251 | 1.07237 | 1.36766 | 1.46628 | 47 |
| 44 | .69466 | .71934 | .96569 | 1.03553 | 1.39012 | 1.43956 | 46 |
| 45 | .70711 | .70711 | 1.00000 | 1.00000 | 1.41421 | 1.41421 | 45 |
| Deg. | Co-sine. | Sines. | Co-tang. | Tang. | Co-sec. | Secants. | Deg. |

WEIGHT OF SQUARE BAR IRON.

79

Table containing the weight of Square Bar Iron, from 1 to 10 feet in length, and from $\frac{1}{4}$ of an inch to 6 inches square.

| Inches square. | LENGTH OF THE BARS IN FEET. | | | | | | | | | |
|-------------------|-----------------------------|---------|---------|---------|---------|---------|---------|---------|---------|----------|
| | 1 foot. | 2 feet. | 3 feet. | 4 feet. | 5 feet. | 6 feet. | 7 feet. | 8 feet. | 9 feet. | 10 feet. |
| | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. |
| $\frac{1}{4}$ in. | 0.2 | 0.4 | 0.6 | 0.8 | 1.1 | 1.3 | 1.5 | 1.7 | 1.9 | 2.1 |
| $\frac{3}{8}$ in. | 0.5 | 1.0 | 1.4 | 1.9 | 2.4 | 2.9 | 3.3 | 3.8 | 4.3 | 4.8 |
| $\frac{1}{2}$ in. | 0.8 | 1.7 | 2.5 | 3.4 | 4.2 | 5.1 | 5.9 | 6.8 | 7.6 | 8.5 |
| $\frac{5}{8}$ in. | 1.3 | 2.6 | 4.0 | 5.3 | 6.6 | 7.9 | 9.2 | 10.6 | 11.9 | 13.2 |
| $\frac{3}{4}$ in. | 1.9 | 3.8 | 5.7 | 7.6 | 9.5 | 11.4 | 13.3 | 15.2 | 17.1 | 19.0 |
| 1 in. | 2.6 | 5.2 | 7.8 | 10.4 | 12.9 | 15.5 | 18.1 | 20.7 | 23.3 | 25.9 |
| 1 1/4 in. | 3.4 | 6.8 | 10.1 | 13.5 | 16.9 | 20.3 | 23.7 | 27.0 | 30.4 | 33.8 |
| 1 1/2 in. | 4.3 | 8.6 | 12.8 | 17.1 | 21.4 | 25.7 | 29.9 | 34.2 | 38.5 | 42.8 |
| 1 3/4 in. | 5.3 | 10.6 | 15.8 | 21.1 | 26.4 | 31.7 | 37.0 | 42.2 | 47.5 | 52.8 |
| 2 in. | 6.4 | 12.8 | 19.2 | 25.6 | 32.0 | 38.3 | 44.7 | 51.1 | 57.5 | 63.9 |
| 2 1/4 in. | 7.6 | 15.2 | 22.8 | 30.4 | 38.0 | 45.6 | 53.2 | 60.8 | 68.4 | 76.0 |
| 2 1/2 in. | 8.9 | 17.9 | 26.8 | 35.7 | 44.6 | 53.6 | 62.5 | 71.4 | 80.3 | 89.3 |
| 2 3/4 in. | 10.4 | 20.7 | 31.1 | 41.4 | 51.8 | 62.1 | 72.5 | 82.8 | 93.2 | 103.5 |
| 3 in. | 11.9 | 23.8 | 35.6 | 47.5 | 59.4 | 71.3 | 83.2 | 95.1 | 106.9 | 118.8 |
| 3 1/4 in. | 13.5 | 27.0 | 40.6 | 54.1 | 67.6 | 81.1 | 94.6 | 108.2 | 121.7 | 135.2 |
| 3 1/2 in. | 15.3 | 30.5 | 45.8 | 61.1 | 76.3 | 91.6 | 106.8 | 122.1 | 137.4 | 152.6 |
| 3 3/4 in. | 17.1 | 34.2 | 51.3 | 68.4 | 85.6 | 102.7 | 119.8 | 136.9 | 154.0 | 171.1 |
| 4 in. | 19.1 | 38.1 | 57.2 | 76.3 | 95.3 | 114.4 | 133.5 | 152.5 | 171.6 | 190.7 |
| 4 1/4 in. | 21.1 | 42.2 | 63.4 | 84.5 | 105.6 | 126.7 | 147.8 | 169.0 | 190.1 | 211.2 |
| 4 1/2 in. | 23.3 | 46.6 | 69.9 | 93.2 | 116.5 | 139.8 | 163.0 | 186.3 | 209.6 | 232.9 |
| 4 3/4 in. | 25.6 | 51.1 | 76.7 | 102.2 | 127.8 | 153.4 | 178.9 | 204.5 | 230.0 | 255.6 |
| 5 in. | 27.9 | 55.9 | 83.8 | 111.8 | 139.7 | 167.6 | 195.7 | 223.5 | 251.5 | 279.4 |
| 5 1/4 in. | 30.4 | 60.8 | 91.2 | 121.7 | 152.1 | 182.5 | 212.9 | 243.3 | 273.7 | 304.2 |
| 5 1/2 in. | 33.0 | 66.0 | 99.0 | 132.0 | 165.1 | 198.1 | 231.1 | 264.1 | 297.1 | 330.1 |
| 5 3/4 in. | 35.7 | 71.4 | 107.1 | 142.8 | 178.5 | 214.2 | 249.9 | 285.6 | 321.3 | 357.0 |
| 6 in. | 38.5 | 77.0 | 115.5 | 154.0 | 192.5 | 231.0 | 269.5 | 308.0 | 346.5 | 385.0 |
| 6 1/4 in. | 41.4 | 82.8 | 124.2 | 165.6 | 207.0 | 248.4 | 289.8 | 331.3 | 372.7 | 414.1 |
| 6 1/2 in. | 44.4 | 88.8 | 133.3 | 177.7 | 222.1 | 266.5 | 310.9 | 355.3 | 399.8 | 444.2 |
| 6 3/4 in. | 47.5 | 95.1 | 142.6 | 190.1 | 237.7 | 285.2 | 332.7 | 380.3 | 427.8 | 475.3 |
| 7 in. | 50.8 | 101.5 | 152.3 | 203.0 | 253.8 | 304.5 | 355.3 | 406.0 | 456.8 | 507.6 |
| 7 1/4 in. | 54.1 | 108.2 | 162.3 | 216.3 | 270.4 | 324.5 | 378.6 | 432.7 | 486.8 | 540.8 |
| 7 1/2 in. | 57.5 | 115.0 | 172.6 | 230.1 | 287.6 | 345.1 | 402.6 | 460.1 | 517.7 | 575.2 |
| 7 3/4 in. | 61.1 | 122.1 | 183.2 | 244.2 | 305.3 | 366.3 | 427.4 | 488.4 | 549.5 | 610.6 |
| 8 in. | 64.7 | 129.4 | 194.1 | 258.8 | 323.5 | 388.2 | 452.9 | 517.6 | 582.3 | 647.0 |
| 8 1/4 in. | 68.4 | 136.9 | 205.3 | 273.8 | 342.2 | 410.7 | 479.1 | 547.6 | 616.0 | 684.5 |
| 8 1/2 in. | 72.3 | 144.6 | 216.9 | 289.2 | 361.5 | 433.8 | 506.1 | 578.4 | 650.7 | 723.1 |
| 8 3/4 in. | 76.3 | 152.5 | 228.8 | 305.1 | 381.3 | 457.6 | 533.8 | 610.1 | 686.4 | 762.6 |
| 9 in. | 80.3 | 160.7 | 241.0 | 321.3 | 401.7 | 482.0 | 562.3 | 642.7 | 723.0 | 803.3 |
| 9 1/4 in. | 84.5 | 169.0 | 253.4 | 337.9 | 422.4 | 506.9 | 591.4 | 675.8 | 760.3 | 844.8 |
| 9 1/2 in. | 93.2 | 186.3 | 279.5 | 372.7 | 465.8 | 559.0 | 652.2 | 745.3 | 838.5 | 931.7 |
| 9 3/4 in. | 102.2 | 204.5 | 306.7 | 409.0 | 511.2 | 613.4 | 715.7 | 817.9 | 920.2 | 1022.4 |
| 10 in. | 111.8 | 223.5 | 335.3 | 447.0 | 558.8 | 670.5 | 782.3 | 894.0 | 1005.8 | 1117.6 |
| 6 in. | 121.7 | 243.3 | 365.0 | 486.7 | 608.3 | 730.0 | 841.6 | 973.3 | 1099.5 | 1216.6 |

Table containing the weight of Round Bar Iron, from 1 to 10 feet in length, and from $\frac{1}{8}$ of an inch to 6 inches diameter.

| Inches diam. | LENGTH OF THE BARS IN FEET. | | | | | | | | | |
|----------------|-----------------------------|---------|---------|---------|---------|---------|---------|---------|---------|----------|
| | 1 foot. | 2 feet. | 3 feet. | 4 feet. | 5 feet. | 6 feet. | 7 feet. | 8 feet. | 9 feet. | 10 feet. |
| | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. |
| $\frac{1}{8}$ | 0.2 | 0.3 | 0.5 | 0.7 | 0.8 | 1.0 | 1.2 | 1.3 | 1.5 | 1.7 |
| $\frac{7}{16}$ | 0.4 | 0.7 | 1.1 | 1.5 | 1.9 | 2.2 | 2.6 | 3.0 | 3.4 | 3.7 |
| $\frac{1}{2}$ | 0.7 | 1.3 | 2.0 | 2.7 | 3.3 | 4.0 | 4.6 | 5.3 | 6.0 | 6.6 |
| $\frac{9}{16}$ | 1.0 | 2.1 | 3.1 | 4.2 | 5.2 | 6.3 | 7.3 | 8.3 | 9.4 | 10.4 |
| $\frac{5}{8}$ | 1.5 | 3.0 | 4.5 | 6.0 | 7.5 | 9.0 | 10.5 | 11.9 | 13.4 | 14.9 |
| $\frac{3}{4}$ | 2.0 | 4.1 | 6.1 | 8.1 | 10.2 | 12.2 | 14.2 | 16.3 | 18.3 | 20.3 |
| 1 in. | 2.7 | 5.3 | 8.0 | 10.6 | 13.3 | 15.9 | 18.6 | 21.2 | 23.9 | 26.5 |
| $1\frac{1}{8}$ | 3.4 | 6.7 | 10.1 | 13.4 | 16.8 | 20.2 | 23.5 | 26.9 | 30.2 | 33.6 |
| $1\frac{1}{4}$ | 4.2 | 8.3 | 12.5 | 16.7 | 20.9 | 25.0 | 29.2 | 33.4 | 37.5 | 41.7 |
| $1\frac{3}{8}$ | 5.0 | 10.0 | 15.1 | 20.1 | 25.1 | 30.1 | 35.1 | 40.2 | 45.2 | 50.2 |
| $1\frac{1}{2}$ | 6.0 | 11.9 | 17.9 | 23.9 | 29.9 | 35.8 | 41.8 | 47.8 | 53.7 | 59.7 |
| $1\frac{3}{4}$ | 7.0 | 14.0 | 21.0 | 28.0 | 35.1 | 42.1 | 49.1 | 56.1 | 63.1 | 70.1 |
| $1\frac{7}{8}$ | 8.1 | 16.3 | 24.4 | 32.5 | 40.6 | 48.8 | 56.9 | 65.0 | 73.2 | 81.3 |
| 2 in. | 9.3 | 18.7 | 28.0 | 37.3 | 46.7 | 56.0 | 65.3 | 74.7 | 84.0 | 93.3 |
| $2\frac{1}{8}$ | 10.6 | 21.2 | 31.8 | 42.5 | 53.1 | 63.7 | 74.3 | 84.9 | 95.5 | 106.2 |
| $2\frac{1}{4}$ | 12.0 | 24.0 | 36.0 | 48.0 | 59.9 | 71.9 | 83.9 | 95.9 | 107.9 | 119.9 |
| $2\frac{3}{8}$ | 13.4 | 26.9 | 40.3 | 53.8 | 67.2 | 80.6 | 94.1 | 107.5 | 121.0 | 134.4 |
| $2\frac{1}{2}$ | 15.0 | 30.0 | 44.9 | 60.0 | 74.9 | 89.9 | 104.8 | 119.8 | 134.8 | 149.8 |
| $2\frac{5}{8}$ | 16.7 | 33.4 | 50.1 | 66.8 | 83.4 | 100.1 | 116.8 | 133.5 | 150.2 | 166.9 |
| $2\frac{3}{4}$ | 18.3 | 36.6 | 54.9 | 73.2 | 91.5 | 109.8 | 128.1 | 146.3 | 164.6 | 182.9 |
| $2\frac{7}{8}$ | 20.1 | 40.2 | 60.2 | 80.3 | 100.4 | 120.5 | 140.5 | 160.6 | 180.7 | 200.8 |
| 3 in. | 21.9 | 43.9 | 65.8 | 87.8 | 109.7 | 131.7 | 153.6 | 175.6 | 197.5 | 219.4 |
| $3\frac{1}{8}$ | 23.9 | 47.8 | 71.7 | 95.6 | 119.4 | 143.3 | 167.2 | 191.1 | 215.0 | 238.9 |
| $3\frac{1}{4}$ | 25.9 | 51.9 | 77.8 | 103.7 | 129.6 | 155.6 | 181.5 | 207.4 | 233.3 | 259.3 |
| $3\frac{3}{8}$ | 28.0 | 56.1 | 84.1 | 112.2 | 140.2 | 168.2 | 196.3 | 224.3 | 253.4 | 280.4 |
| $3\frac{1}{2}$ | 30.2 | 60.5 | 90.7 | 121.0 | 151.2 | 181.4 | 211.7 | 241.9 | 272.2 | 302.4 |
| $3\frac{3}{4}$ | 32.5 | 65.0 | 97.5 | 130.0 | 162.6 | 195.1 | 227.6 | 260.1 | 292.6 | 325.1 |
| $3\frac{7}{8}$ | 34.9 | 69.8 | 104.7 | 139.5 | 174.4 | 209.3 | 244.2 | 279.1 | 314.0 | 348.9 |
| 4 in. | 37.3 | 74.7 | 112.0 | 149.3 | 186.7 | 224.0 | 261.3 | 298.7 | 336.0 | 373.3 |
| $4\frac{1}{8}$ | 39.9 | 79.7 | 119.6 | 159.5 | 199.3 | 239.2 | 279.0 | 318.9 | 358.8 | 398.6 |
| $4\frac{1}{4}$ | 42.5 | 84.9 | 127.4 | 169.9 | 212.3 | 254.8 | 297.2 | 339.7 | 382.2 | 424.6 |
| $4\frac{3}{8}$ | 45.2 | 90.3 | 135.5 | 180.7 | 225.9 | 271.0 | 316.2 | 361.4 | 406.6 | 451.7 |
| $4\frac{1}{2}$ | 48.0 | 95.9 | 143.9 | 191.8 | 239.8 | 287.7 | 333.7 | 383.6 | 431.6 | 479.5 |
| $4\frac{3}{4}$ | 50.8 | 101.6 | 152.4 | 203.3 | 254.1 | 304.9 | 355.7 | 406.5 | 457.3 | 508.2 |
| $4\frac{7}{8}$ | 53.8 | 107.5 | 161.3 | 215.0 | 268.8 | 322.6 | 376.3 | 430.1 | 483.8 | 537.6 |
| 5 in. | 56.8 | 113.6 | 170.4 | 227.2 | 283.9 | 340.7 | 397.5 | 454.3 | 511.1 | 567.9 |
| $5\frac{1}{8}$ | 60.0 | 119.8 | 179.7 | 239.6 | 299.5 | 359.4 | 419.3 | 479.2 | 539.1 | 599.0 |
| $5\frac{1}{4}$ | 63.1 | 126.2 | 189.3 | 252.4 | 315.5 | 378.6 | 441.7 | 504.8 | 567.8 | 630.9 |
| $5\frac{3}{8}$ | 66.8 | 133.5 | 200.3 | 267.0 | 333.8 | 400.5 | 467.3 | 534.0 | 600.8 | 667.5 |
| $5\frac{1}{2}$ | 73.2 | 146.3 | 219.5 | 292.7 | 365.9 | 439.0 | 512.2 | 585.4 | 658.5 | 731.7 |
| $5\frac{3}{4}$ | 80.3 | 160.6 | 240.9 | 321.2 | 401.5 | 481.8 | 562.1 | 642.4 | 722.7 | 803.0 |
| $5\frac{7}{8}$ | 87.8 | 175.6 | 263.3 | 351.1 | 438.9 | 526.7 | 614.4 | 702.2 | 790.0 | 877.8 |
| 6 in. | 95.6 | 191.1 | 286.7 | 382.2 | 477.8 | 573.3 | 668.9 | 764.4 | 860.0 | 955.5 |

Table containing the weight of Flat Bar Iron, 1 foot in length,
of various breadths and thicknesses.

| Breadth in inches. | THICKNESS IN PARTS OF AN INCH. | | | | | | | | | |
|-----------------------|--------------------------------|---------------|----------------|---------------|---------------|---------------|---------------|---------------|---------------|---------|
| | $\frac{1}{4}$ | $\frac{1}{5}$ | $\frac{3}{16}$ | $\frac{1}{2}$ | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 Inch. |
| | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. |
| 1 in. | 0.83 | 1.04 | 1.25 | 1.45 | 1.66 | 1.87 | 2.08 | 2.50 | 2.91 | 3.33 |
| 1 $\frac{1}{4}$ | 0.93 | 1.17 | 1.40 | 1.64 | 1.87 | 2.00 | 2.34 | 2.81 | 3.28 | 3.75 |
| 1 $\frac{1}{2}$ | 1.04 | 1.30 | 1.56 | 1.82 | 2.08 | 2.34 | 2.60 | 3.12 | 3.74 | 4.16 |
| 1 $\frac{3}{4}$ | 1.14 | 1.43 | 1.71 | 2.00 | 2.29 | 2.57 | 2.86 | 3.43 | 4.01 | 4.58 |
| 2 in. | 1.25 | 1.56 | 1.87 | 2.18 | 2.50 | 2.81 | 3.12 | 3.75 | 4.37 | 5.00 |
| 2 $\frac{1}{4}$ | 1.35 | 1.69 | 2.03 | 2.36 | 2.70 | 3.04 | 3.38 | 4.06 | 4.73 | 5.41 |
| 2 $\frac{1}{2}$ | 1.45 | 1.82 | 2.18 | 2.55 | 2.91 | 3.28 | 3.64 | 4.37 | 5.10 | 5.83 |
| 2 $\frac{3}{4}$ | 1.56 | 1.95 | 2.34 | 2.73 | 3.12 | 3.51 | 3.90 | 4.68 | 5.46 | 6.25 |
| 3 in. | 1.66 | 2.08 | 2.50 | 2.91 | 3.33 | 3.75 | 4.16 | 5.00 | 5.83 | 6.66 |
| 3 $\frac{1}{4}$ | 1.77 | 2.21 | 2.65 | 3.09 | 3.54 | 3.98 | 4.42 | 5.31 | 6.19 | 7.08 |
| 3 $\frac{1}{2}$ | 1.87 | 2.34 | 2.81 | 3.28 | 3.75 | 4.21 | 4.68 | 5.62 | 6.56 | 7.50 |
| 3 $\frac{3}{4}$ | 1.97 | 2.47 | 2.96 | 3.46 | 3.95 | 4.45 | 4.94 | 5.93 | 6.92 | 7.91 |
| 4 in. | 2.08 | 2.60 | 3.12 | 3.64 | 4.16 | 4.68 | 5.20 | 6.25 | 7.29 | 8.33 |
| 4 $\frac{1}{4}$ | 2.18 | 2.73 | 3.28 | 3.82 | 4.37 | 4.92 | 5.46 | 6.56 | 7.65 | 8.75 |
| 4 $\frac{1}{2}$ | 2.29 | 2.86 | 3.43 | 4.01 | 4.58 | 5.15 | 5.72 | 6.87 | 8.02 | 9.16 |
| 4 $\frac{3}{4}$ | 2.39 | 2.99 | 3.59 | 4.19 | 4.79 | 5.39 | 5.98 | 7.18 | 8.38 | 9.58 |
| 5 in. | 2.50 | 3.12 | 3.75 | 4.37 | 5.00 | 5.62 | 6.25 | 7.50 | 8.75 | 10.00 |
| 5 $\frac{1}{4}$ | 2.70 | 3.38 | 4.06 | 4.73 | 5.41 | 6.09 | 6.77 | 8.12 | 9.47 | 10.83 |
| 5 $\frac{1}{2}$ | 2.91 | 3.64 | 4.37 | 5.10 | 5.83 | 6.56 | 7.29 | 8.75 | 10.20 | 11.66 |
| 5 $\frac{3}{4}$ | 3.12 | 3.90 | 4.68 | 5.46 | 6.25 | 7.03 | 7.81 | 9.37 | 10.93 | 12.50 |
| 6 in. | 3.33 | 4.16 | 5.00 | 5.83 | 6.66 | 7.50 | 8.33 | 10.00 | 11.66 | 13.33 |
| 6 $\frac{1}{4}$ | 3.54 | 4.42 | 5.31 | 6.19 | 7.08 | 7.96 | 8.85 | 10.62 | 12.39 | 14.16 |
| 6 $\frac{1}{2}$ | 3.75 | 4.68 | 5.62 | 6.56 | 7.50 | 8.43 | 9.37 | 11.25 | 13.12 | 15.00 |
| 6 $\frac{3}{4}$ | 3.95 | 4.94 | 5.93 | 6.92 | 7.91 | 8.90 | 9.89 | 11.87 | 13.85 | 15.83 |
| 7 in. | 4.17 | 5.20 | 6.25 | 7.29 | 8.33 | 9.37 | 10.41 | 12.50 | 14.58 | 16.66 |
| 7 $\frac{1}{4}$ | 4.37 | 5.46 | 6.56 | 7.65 | 8.75 | 9.84 | 10.93 | 13.12 | 15.31 | 17.50 |
| 7 $\frac{1}{2}$ | 4.58 | 5.72 | 6.87 | 8.02 | 9.16 | 10.31 | 11.45 | 13.75 | 16.04 | 18.33 |
| 7 $\frac{3}{4}$ | 4.79 | 5.98 | 7.18 | 8.38 | 9.58 | 10.78 | 11.97 | 14.37 | 16.77 | 19.16 |
| 8 in. | 5.00 | 6.26 | 7.50 | 8.75 | 10.00 | 11.25 | 12.50 | 15.00 | 17.50 | 20.00 |

Comparative Gravity of Metals.

| | | |
|---------------------|----------------------|--------------------|
| Bar Iron being 1.00 | Cast Iron being 1.00 | Dry Deal being 1.0 |
| Cast Iron = .95 | Bar Iron = 1.07 | Cast Iron = 11.0 |
| Steel = 1.02 | Steel = 1.08 | Cast Tin = 11.2 |
| Copper = 1.16 | Brass = 1.16 | Brass = 12.7 |
| Brass = 1.09 | Copper = 1.21 | Copper = 13.3 |
| Lead = 1.48 | Lead = 1.56 | Lead = 17.1 |

Table containing the weight of Cast Iron Balls from 3 to 12 inches diameter.

| Diameter in inches. | Weight in Lbs. | Diameter in inches. | Weight in Lbs. | Diameter in inches. | Weight in Lbs. |
|---------------------------|----------------------|---------------------------|----------------------|---------------------------|----------------------|
| 3 | 3.7 | 6 | 29.7 | 9 | 100.3 |
| 3½ | 4.7 | 6½ | 33.6 | 9½ | 108.9 |
| 3¾ | 5.8 | 6¾ | 37.8 | 9¾ | 118.0 |
| 3⅞ | 7.2 | 6⅞ | 42.3 | 9⅞ | 127.6 |
| 4 | 8.8 | 7 | 47.2 | 10 | 137.7 |
| 4¼ | 10.5 | 7¼ | 52.4 | 10¼ | 148.2 |
| 4½ | 12.5 | 7½ | 58.0 | 10½ | 159.4 |
| 4¾ | 14.7 | 7¾ | 64.0 | 10¾ | 171.0 |
| 5 | 17.1 | 8 | 70.4 | 11 | 183.2 |
| 5¼ | 19.9 | 8¼ | 77.3 | 11¼ | 209.4 |
| 5½ | 22.9 | 8½ | 84.5 | 12 | 237.9 |
| 5¾ | 26.1 | 8¾ | 92.2 | | |

Properties of Metals.

| NAMES OF METALS. | Specific gravity water being 1000. | Melting point in degrees of Fahr. | Contraction in parts of an inch per lineal foot, from the fluid to the average tem- perature in solid state. | Cohesive strength of an inch square prism in lbs. | Scale of wire-draw- ing ductility. | Scale of laminae ductility. | Scale as conductors of electricity. | Ratio of power in the conduction of heat. |
|---------------------|---------------------------------------|--------------------------------------|---|---|---------------------------------------|--------------------------------|--|--|
| Platinum | 19500 | 3280 | | | 3 | 5 | ... | 3.8 |
| Pure Gold | 19258 | 2016 | | | 1 | 1 | 3 | 10.0 |
| Mercury | 13560 | | | | ... | ... | ... | ... |
| Lead | 11352 | 612 | .319 | 1824 | 8 | 7 | 6 | 1.8 |
| Pure Silver..... | 10474 | 1873 | | | 2 | 2 | 2 | 9.7 |
| Bismuth | 9823 | 476 | .156 | 3250 | ... | ... | ... | ... |
| Copper, cast..... | 8788 | 1996 | .193 | 19072 | ... | ... | ... | ... |
| " wrought..... | 8910 | | | 33892 | 5 | 3 | 1 | 8.9 |
| Brass, cast | 7824 | 1900 | .210 | 17968 | ... | ... | ... | ... |
| " sheet..... | 8396 | | | 27935 | 6 | 6 | ... | 8.6 |
| Iron, cast..... | 7264 | 2786 | .125 | 17628 | ... | ... | ... | ... |
| " bar | 7700 | | .137 | 56000 | 4 | 8 | 4 | 3.7 |
| Steel, soft..... | 7833 | | .133 | 127632 | ... | ... | ... | ... |
| " hard | 7816 | | | | ... | ... | ... | ... |
| Tin, cast | 7291 | 442 | .278 | 4763 | 8 | 4 | 5 | 3.0 |
| Zinc, cast..... | 7190 | 773 | .329 | 11334 | 7 | 8 | 7 | 3.6 |

NOTE.—The elastic power or direct tension of bar iron, medium quality, equal 22400 lbs. per square inch of sectional area.

Table containing the weight of Cast Iron Pipes, 1 foot in length.

| Diam. of bore in inches. | THICKNESS IN INCHES. | | | | | | | |
|-----------------------------------|----------------------|---------------|---------------|---------------|---------------|-------|----------------|----------------|
| | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 in | $1\frac{1}{8}$ | $1\frac{1}{4}$ |
| | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. |
| $1\frac{1}{8}$ | 6.9 | 9.9 | | | | | | |
| 2 | 3.8 | 12.3 | 16.1 | 20.3 | | | | |
| $2\frac{1}{8}$ | 10.6 | 14.7 | 19.2 | 23.9 | | | | |
| 3 | 12.4 | 17.2 | 22.2 | 27.6 | 33.8 | 39.3 | 45.6 | |
| $3\frac{1}{8}$ | 14.2 | 19.6 | 25.3 | 31.3 | 37.6 | 44.2 | 51.1 | |
| 4 | 16.8 | 22.1 | 28.4 | 35.0 | 41.9 | 49.1 | 56.6 | 64.4 |
| $4\frac{1}{8}$ | 18.0 | 24.5 | 31.4 | 38.7 | 46.2 | 54.0 | 62.1 | 70.6 |
| 5 | 19.8 | 27.0 | 34.5 | 42.3 | 50.5 | 58.9 | 67.6 | 76.7 |
| $5\frac{1}{8}$ | 21.6 | 29.5 | 37.6 | 46.0 | 54.8 | 63.8 | 73.2 | 82.8 |
| 6 | 23.5 | 31.9 | 40.7 | 49.7 | 59.1 | 68.7 | 78.7 | 88.8 |
| $6\frac{1}{8}$ | 25.3 | 34.4 | 43.7 | 53.4 | 63.4 | 73.4 | 84.2 | 95.1 |
| 7 | 27.2 | 36.8 | 46.8 | 56.8 | 67.7 | 78.5 | 89.7 | 101.2 |
| $7\frac{1}{8}$ | 29.0 | 39.1 | 49.9 | 60.7 | 72.0 | 83.5 | 95.3 | 107.4 |
| 8 | 30.8 | 41.7 | 52.9 | 64.4 | 76.2 | 88.4 | 100.8 | 113.5 |
| $8\frac{1}{8}$ | 32.9 | 44.4 | 56.2 | 68.3 | 80.8 | 93.5 | 106.5 | 119.9 |
| 9 | 34.5 | 46.6 | 59.1 | 71.8 | 84.8 | 98.2 | 111.8 | 125.8 |
| $9\frac{1}{8}$ | 36.3 | 49.1 | 62.1 | 75.5 | 89.1 | 103.1 | 117.4 | 131.9 |
| 10 | 38.2 | 51.5 | 65.2 | 79.2 | 93.4 | 108.0 | 122.8 | 138.1 |
| $10\frac{1}{8}$ | | 54.0 | 68.2 | 82.8 | 97.7 | 112.9 | 128.4 | 144.2 |
| 11 | | 56.4 | 71.3 | 86.5 | 102.0 | 117.8 | 133.9 | 150.3 |
| $11\frac{1}{8}$ | | 58.9 | 74.3 | 90.1 | 106.3 | 122.7 | 139.4 | 156.4 |
| 12 | | 61.3 | 77.4 | 93.6 | 110.6 | 127.6 | 145.0 | 162.6 |
| 13 | | | 82.7 | 101.2 | 118.2 | 137.4 | 154.1 | 173.5 |
| 14 | | | 89.3 | 108.2 | 126.5 | 146.2 | 165.3 | 185.2 |
| 15 | | | 95.2 | 115.7 | 135.3 | 156.2 | 176.2 | 198.1 |
| 16 | | | | 123.3 | 143.1 | 166.1 | 187.5 | 211.3 |
| 17 | | | | 130.2 | 152.5 | 178.5 | 198.2 | 223.4 |
| 18 | | | | 137.0 | 161.2 | 185.3 | 209.1 | 235.6 |
| 19 | | | | | 169.2 | 195.7 | 222.3 | 247.1 |
| 20 | | | | | 178.1 | 205.2 | 233.2 | 259.0 |
| 21 | | | | | | 214.1 | 243.5 | 273.2 |
| 22 | | | | | | 223.0 | 254.8 | 285.4 |
| 23 | | | | | | 233.4 | 265.5 | 298.3 |
| 24 | | | | | | 245.2 | 277.5 | 310.6 |

NOTE.—The area of a circle in inches, multiplied by the length in inches, and 263 = the weight in lbs. avoirdupois of cast iron.

Table containing the weight of Solid Cylinders of Cast Iron, one foot in length, and from $\frac{1}{8}$ of an inch to 14 inches diameter.

| Diameter in Inches. | Weight in Lbs. | Diameter in Inches. | Weight in Lbs. |
|---------------------------|----------------------|---------------------------|----------------------|
| $\frac{1}{8}$ | 1.39 | 5 in. | 61.96 |
| $\frac{1}{4}$ | 1.88 | $5\frac{1}{8}$ | 64.66 |
| $\frac{3}{8}$ in. | 2.47 | $5\frac{1}{4}$ | 68.31 |
| $\frac{1}{2}$ | 3.13 | $5\frac{1}{2}$ | 71.00 |
| $\frac{5}{8}$ | 3.87 | $5\frac{3}{4}$ | 74.98 |
| $\frac{3}{4}$ | 4.68 | $5\frac{7}{8}$ | 78.65 |
| $1\frac{1}{8}$ | 5.57 | $6\frac{1}{8}$ | 81.95 |
| $1\frac{1}{4}$ | 6.54 | $6\frac{1}{4}$ | 85.81 |
| $1\frac{3}{8}$ | 7.59 | | |
| $1\frac{1}{2}$ | 8.71 | 6 in. | 89.28 |
| | | $6\frac{1}{8}$ | 96.82 |
| 2 in. | 9.91 | $6\frac{1}{4}$ | 104.72 |
| $2\frac{1}{8}$ | 11.19 | $6\frac{3}{4}$ | 112.98 |
| $2\frac{1}{4}$ | 12.54 | | |
| $2\frac{3}{8}$ | 13.96 | 7 in. | 121.45 |
| $2\frac{1}{2}$ | 15.49 | $7\frac{1}{8}$ | 130.28 |
| $2\frac{5}{8}$ | 17.08 | $7\frac{1}{4}$ | 139.42 |
| $2\frac{3}{4}$ | 18.74 | $7\frac{3}{4}$ | 148.87 |
| $2\frac{7}{8}$ | 20.48 | $7\frac{7}{8}$ | 158.63 |
| | | 8 in. | 168.15 |
| 3 in. | 22.35 | $8\frac{1}{8}$ | 179.08 |
| $3\frac{1}{8}$ | 24.20 | $8\frac{1}{4}$ | 189.00 |
| $3\frac{1}{4}$ | 26.18 | $8\frac{3}{4}$ | |
| $3\frac{3}{8}$ | 28.28 | | |
| $3\frac{1}{2}$ | 30.36 | 9 in. | 200.77 |
| $3\frac{5}{8}$ | 32.57 | $9\frac{1}{8}$ | 211.12 |
| $3\frac{3}{4}$ | 34.85 | $9\frac{1}{4}$ | 223.70 |
| $3\frac{7}{8}$ | 37.21 | $9\frac{3}{4}$ | 235.31 |
| | | | |
| 4 in. | 39.66 | 10 in. | 247.87 |
| $4\frac{1}{8}$ | 41.80 | $10\frac{1}{8}$ | 273.27 |
| $4\frac{1}{4}$ | 44.77 | | |
| $4\frac{3}{8}$ | 47.00 | 11 in. | 299.92 |
| $4\frac{1}{2}$ | 50.19 | $11\frac{1}{8}$ | 327.81 |
| $4\frac{5}{8}$ | 52.71 | $11\frac{1}{4}$ | 356.93 |
| $4\frac{3}{4}$ | 55.92 | 12 in. | 418.90 |
| $4\frac{7}{8}$ | 58.72 | 13 | 485.83 |
| | | 14 | |

NOTE.—The area of a circle in inches, multiplied by the length in inches, and by .263 — the weight in lbs. avoirdupois of cast iron.

*Table of economical advantages in using Steam expansively, by
Professor Gordon, Glasgow.*

| | Proportion of stroke made before steam is cut off | Volume after expansion, that before expansion taken as unity. | Mechanical effect developed by a given volume of steam for different degrees of expansion, the temperature being supposed maintained constant. | Economy of fuel by obtaining the increase of mechanical effect thus available. | Initial pressure of steam required to allow of this degree of expansion in any given cylinder, doing the work by full pressure, in the manner of that pressure taken as unity. | Initial pressure of steam required to allow of this degree of expansion in any given cylinder doing the work by full pressure, with steam of 1.264 atmospheres, or 22 lbs., taken as unity. | Temperature corresponding to foregoing pressure or elastic force. | Weight of a cubic foot of steam of this density and pressure. | Economy of fuel indicated in this manner as resulting from the use of expansion. |
|-------|---|---|--|--|--|---|---|---|--|
| | | | Per Cent. | Atmospheres. | Lbs. | Atmospheres. | | Lbs. | Per Cent. |
| Total | 1.00 | 1.0000 | 0 | 1.000 | 28.000 | 1.564 | 236.3 | .0556 | 0 |
| 3-4 | 1.33 | 1.2851 | . | 1.087 | 28.851 | 1.622 | 238.0 | .0575 | 22½ |
| 3-5 | 1.66 | 1.5068 | 33 | 1.105 | 25.415 | 1.713 | 241.8 | .0604 | 35 |
| 4-7 | 1.75 | 1.5596 | . | 1.121 | 25.783 | 1.753 | 242.7 | .0617 | 36½ |
| 5-9 | 1.80 | 1.5876 | . | 1.139 | 26.197 | 1.781 | 243.6 | .0626 | 37 |
| 10-19 | 1.90 | 1.6419 | . | 1.157 | 26.611 | 1.810 | 244.8 | .0635 | 40 |
| 1-2 | 2.00 | 1.6931 | 30 | 1.195 | 27.485 | 1.869 | 246.0 | .0655 | 41 |
| 4-9 | 2.25 | 1.8109 | . | 1.231 | 28.813 | 1.925 | 248.0 | .0672 | 46 |
| 2-5 | 2.50 | 1.9163 | . | 1.304 | 29.992 | 2.040 | 251.0 | .0709 | 49 |
| 4-11 | 2.75 | 2.0116 | 50 | 1.367 | 31.441 | 2.188 | 254.5 | .0740 | 51½ |
| 1-3 | 3.00 | 2.0986 | 52½ | 1.429 | 32.867 | 2.235 | 257.0 | .0771 | 53½ |
| 4-13 | 3.25 | 2.1786 | . | 1.491 | 34.293 | 2.332 | 259.3 | .0802 | 55½ |
| 2-7 | 3.50 | 2.2528 | . | 1.553 | 35.719 | 2.429 | 261.5 | .0832 | 57 |
| 4-15 | 3.75 | 2.3217 | . | 1.589 | 36.547 | 2.485 | 263.5 | .0849 | 59½ |
| 1-4 | 4.00 | 2.3860 | 50 | 1.677 | 38.571 | 2.623 | 266.9 | .0892 | 60 |
| 2-9 | 4.50 | 2.5040 | . | 1.797 | 41.931 | 2.811 | 271.0 | .0951 | 62 |
| 1-5 | 5.00 | 2.609 | 62 | 1.873 | 43.079 | 2.929 | 273.8 | .0988 | 64½ |
| 2-11 | 5.50 | 2.705 | . | 2.033 | 46.759 | 3.180 | 279.0 | .1064 | 68 |
| 1-6 | 6.00 | 2.792 | 65 | 2.149 | 49.427 | 3.361 | 283.0 | .1118 | 66½ |
| 2-13 | 6.50 | 2.872 | . | 2.263 | 52.049 | 3.529 | 285.8 | .1173 | 67½ |
| 1-7 | 7.00 | 2.946 | . | 2.376 | 54.648 | 3.716 | 289.0 | .1227 | 68½ |
| 1-8 | 8.00 | 3.0794 | . | 2.597 | 59.731 | 4.062 | 294.7 | .1331 | 70 |

NOTE.—Mr. McNaught has ascertained, by the application of his indicators, that there is no economical advantage in cutting off the steam from an engine at more than three-fourths the stroke, and at two-thirds, he asserts, is the most advantageous point.

Table containing Degrees of Heat by the Fahrenheit, Reaumer, and Centigrade Thermometers, comparatively indicated.

| Faht. | Reau. | Cent. | Faht. | Reau. | Cent. | Faht. | Reau. | Cent. |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 350 | 141.3 | 176.7 | 186 | 68.4 | 85.5 | 108 | 33.7 | 42.2 |
| 320 | 128.0 | 160.0 | 184 | 67.5 | 84.4 | 106 | 32.8 | 41.1 |
| 300 | 119.1 | 148.9 | 182 | 66.6 | 83.3 | 104 | 32.0 | 40.0 |
| 290 | 114.7 | 143.3 | 180 | 65.7 | 82.2 | 102 | 31.1 | 38.8 |
| 280 | 110.2 | 137.8 | 178 | 64.8 | 81.1 | 100 | 30.2 | 37.7 |
| 270 | 105.8 | 132.2 | 176 | 64.0 | 80.0 | 98 | 29.3 | 36.6 |
| 260 | 101.3 | 126.6 | 174 | 63.1 | 78.8 | 96 | 28.4 | 35.5 |
| 250 | 96.9 | 121.1 | 172 | 62.2 | 77.7 | 94 | 27.5 | 34.4 |
| 248 | 96.0 | 120.0 | 170 | 61.3 | 76.6 | 92 | 26.6 | 33.3 |
| 246 | 95.1 | 118.8 | 168 | 60.4 | 75.5 | 90 | 25.7 | 32.2 |
| 244 | 94.2 | 117.7 | 166 | 59.5 | 74.4 | 88 | 24.8 | 31.1 |
| 242 | 93.3 | 116.6 | 164 | 58.6 | 73.3 | 86 | 24.0 | 30.0 |
| 240 | 92.4 | 115.5 | 162 | 57.7 | 72.2 | 84 | 23.1 | 28.8 |
| 238 | 91.6 | 114.4 | 160 | 56.8 | 71.1 | 82 | 22.2 | 27.7 |
| 236 | 90.7 | 113.3 | 158 | 56.0 | 70.0 | 80 | 21.3 | 26.6 |
| 234 | 89.8 | 112.2 | 156 | 55.1 | 68.8 | 78 | 20.4 | 25.5 |
| 232 | 88.9 | 111.1 | 154 | 54.2 | 67.7 | 76 | 19.5 | 24.4 |
| 230 | 88.0 | 110.0 | 152 | 53.3 | 66.6 | 74 | 18.6 | 23.3 |
| 228 | 87.1 | 108.9 | 150 | 52.4 | 65.5 | 72 | 17.7 | 22.2 |
| 226 | 86.2 | 107.8 | 148 | 51.5 | 64.4 | 70 | 16.8 | 21.1 |
| 224 | 85.3 | 106.7 | 146 | 50.6 | 63.3 | 68 | 16.0 | 20.0 |
| 222 | 84.4 | 105.6 | 144 | 49.7 | 62.2 | 66 | 15.1 | 18.8 |
| 220 | 83.6 | 104.4 | 142 | 48.8 | 61.1 | 64 | 14.2 | 17.7 |
| 218 | 82.7 | 103.3 | 140 | 48.0 | 60.0 | 62 | 13.3 | 16.6 |
| 216 | 81.8 | 102.2 | 138 | 47.1 | 58.8 | 60 | 12.4 | 15.5 |
| 214 | 80.9 | 101.1 | 136 | 46.2 | 57.7 | 58 | 11.5 | 14.4 |
| 212 | 80.0 | 100.0 | 134 | 45.3 | 56.6 | 56 | 10.6 | 13.3 |
| 210 | 79.1 | 98.8 | 132 | 44.4 | 55.5 | 54 | 9.7 | 12.2 |
| 208 | 78.2 | 97.7 | 130 | 43.5 | 54.4 | 52 | 8.8 | 11.1 |
| 206 | 77.3 | 96.6 | 128 | 42.6 | 53.3 | 50 | 8.0 | 10.0 |
| 204 | 76.4 | 95.5 | 126 | 41.7 | 52.2 | 48 | 7.1 | 8.8 |
| 202 | 75.5 | 94.4 | 124 | 40.8 | 51.1 | 46 | 6.2 | 7.7 |
| 200 | 74.6 | 93.3 | 122 | 40.0 | 50.0 | 44 | 5.3 | 6.6 |
| 198 | 73.7 | 92.2 | 120 | 39.1 | 48.8 | 42 | 4.4 | 5.5 |
| 196 | 72.8 | 91.1 | 118 | 38.2 | 47.7 | 40 | 3.5 | 4.4 |
| 194 | 72.0 | 90.0 | 116 | 37.3 | 46.6 | 38 | 2.6 | 3.3 |
| 192 | 71.1 | 88.8 | 114 | 36.4 | 45.5 | 36 | 1.7 | 2.2 |
| 190 | 70.2 | 87.7 | 112 | 35.5 | 44.4 | 34 | 0.8 | 1.1 |
| 188 | 69.3 | 86.6 | 110 | 34.6 | 43.3 | 32 | 0.0 | 0.0 |

Boiling points of Water at different heights of the Barometer.

| Barometer Inches. | Boiling Point Deg. of Fahr. | Barometer Inches. | Boiling Point. Deg. of Fahr. |
|----------------------|--------------------------------|---|---------------------------------|
| 31 | 213 57 | 28½ | 209.55 |
| 30½ | 212.79 | 28 | 208.69 |
| 30 | 212 00 | 27½ | 207.34 |
| 29½ | 211.20 | 27 | 206 96 |
| 29 | 210 38 | In a vacuum more or less perfect from 28 to 100. | |

Table containing the superficies and solid content of Spheres, from 1 to 12, and advancing by a tenth.

| Diam. | Superficies. | Solidity. | Diam. | Superficies. | Solidity. |
|-------|--------------|-----------|-------|--------------|-----------|
| 1.0 | 3.1416 | .5236 | 3.5 | 38.4846 | 22.4493 |
| .1 | 3.8013 | .6969 | .6 | 40.7151 | 24.4290 |
| .2 | 4.5239 | .9047 | .7 | 43.0085 | 26.5219 |
| .3 | 5.3093 | 1.1503 | .8 | 45.3647 | 28.7309 |
| .4 | 6.1575 | 1.4367 | .9 | 47.7837 | 31.0594 |
| .5 | 7.0686 | 1.7671 | 4.0 | 50.2656 | 33.5104 |
| .6 | 8.0424 | 2.1446 | .1 | 52.8102 | 36.0870 |
| .7 | 9.0792 | 2.5724 | .2 | 55.4178 | 38.7924 |
| .8 | 10.1787 | 3.0536 | .3 | 58.0881 | 41.6298 |
| .9 | 11.3411 | 3.5913 | .4 | 60.8213 | 44.6023 |
| 2.0 | 12.5664 | 4.1888 | .5 | 63.6174 | 47.7130 |
| .1 | 13.8544 | 4.8490 | .6 | 66.4782 | 50.9651 |
| .2 | 15.2053 | 5.5752 | .7 | 69.3979 | 54.3617 |
| .3 | 16.6190 | 6.3706 | .8 | 72.3824 | 57.9059 |
| .4 | 18.0956 | 7.2382 | .9 | 75.4298 | 61.6010 |
| .5 | 19.6350 | 8.1812 | 5.0 | 78.5400 | 65.4500 |
| .6 | 21.2372 | 9.2027 | .1 | 81.7130 | 69.4560 |
| .7 | 22.9022 | 10.3060 | .2 | 84.9488 | 73.6223 |
| .8 | 24.6300 | 11.4940 | .3 | 88.2475 | 77.9519 |
| .9 | 26.4208 | 12.7700 | .4 | 91.6090 | 82.4481 |
| 3.0 | 28.2744 | 14.1372 | .5 | 95.0334 | 87.1139 |
| .1 | 30.1907 | 15.5985 | .6 | 98.5205 | 91.9525 |
| .2 | 32.1699 | 17.1573 | .7 | 102.0705 | 96.9670 |
| .3 | 34.2120 | 18.8166 | .8 | 105.6834 | 102.1606 |
| .4 | 36.3168 | 20.5795 | .9 | 109.3590 | 107.5364 |

| Diam. | Superficies. | Solidity. | Diam. | Superficies. | Solidity. |
|-------|--------------|-----------|-------|--------------|-----------|
| 6.0 | 113.0976 | 113.0976 | 9.0 | 254.4696 | 381.7044 |
| .1 | 116.8989 | 118.8472 | .1 | 260.1558 | 394.5697 |
| .2 | 120.7631 | 124.7885 | .2 | 265.9130 | 407.7210 |
| .3 | 124.6901 | 130.9246 | .3 | 271.7169 | 421.1613 |
| .4 | 128.6799 | 137.2585 | .4 | 277.5917 | 434.8937 |
| .5 | 132.7326 | 143.7936 | .5 | 283.5294 | 448.9215 |
| .6 | 136.8480 | 150.5329 | .6 | 289.5298 | 463.2477 |
| .7 | 141.0264 | 157.4795 | .7 | 295.5931 | 477.7755 |
| .8 | 145.2675 | 164.6365 | .8 | 301.7192 | 492.8081 |
| .9 | 149.5715 | 172.0073 | .9 | 307.9082 | 508.0485 |
| 7.0 | 153.9384 | 179.5948 | 10.0 | 314.1600 | 523.6000 |
| .1 | 158.3680 | 187.4021 | .1 | 320.4746 | 539.4656 |
| .2 | 162.8605 | 195.4326 | .2 | 326.8520 | 555.6485 |
| .3 | 167.4158 | 203.6893 | .3 | 333.2923 | 572.1518 |
| .4 | 172.0340 | 212.1752 | .4 | 339.7954 | 588.9784 |
| .5 | 176.7150 | 220.8937 | .5 | 346.3614 | 606.1324 |
| .6 | 181.4588 | 229.8478 | .6 | 352.9901 | 623.6159 |
| .7 | 186.2654 | 239.0511 | .7 | 359.6817 | 641.4325 |
| .8 | 191.1349 | 248.4754 | .8 | 366.4362 | 659.5852 |
| .9 | 196.0672 | 258.1552 | .9 | 373.2534 | 678.0771 |
| 8.0 | 201.0624 | 268.0832 | 11.0 | 380.1336 | 696.9116 |
| .1 | 206.1203 | 278.2625 | .1 | 387.0765 | 716.0915 |
| .2 | 211.2411 | 288.6962 | .2 | 394.0823 | 735.6200 |
| .3 | 216.4248 | 299.3876 | .3 | 401.1509 | 755.5008 |
| .4 | 221.6712 | 310.3398 | .4 | 408.2823 | 775.7364 |
| .5 | 226.9806 | 321.5558 | .5 | 415.4766 | 796.3301 |
| .6 | 232.3527 | 333.0389 | .6 | 422.7336 | 817.2851 |
| .7 | 237.7877 | 344.7921 | .7 | 430.0536 | 838.6045 |
| .8 | 243.2855 | 356.8187 | .8 | 437.4363 | 860.2915 |
| .9 | 248.8461 | 369.1217 | .9 | 444.8819 | 882.3492 |
| | | | 12.0 | 452.3904 | 904.7808 |

A TABLE
CONTAINING THE
CIRCUMFERENCES, SQUARES, CUBES,
AND
AREAS OF CIRCLES,

*From $\frac{1}{8}$ th to 100 inches, advancing by a $\frac{1}{8}$ th, and also the side
of equal square, advancing at an equal ratio.*

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|---------|---------|---------|--------|-----------------|
| $\frac{1}{16}$ | .1963 | .0039 | .00024 | .0030 | .0554 |
| $\frac{1}{8}$ | .3927 | .0156 | .00195 | .0122 | .1107 |
| $\frac{3}{16}$ | .5890 | .0351 | .00659 | .0276 | .1661 |
| $\frac{1}{4}$ | .7854 | .0625 | .01562 | .0490 | .2115 |
| $\frac{5}{16}$ | .9817 | .0976 | .03051 | .0767 | .2669 |
| $\frac{3}{8}$ | 1.1781 | .1406 | .05273 | .1104 | .3223 |
| $\frac{7}{16}$ | 1.3744 | .1914 | .08374 | .1503 | .3771 |
| $\frac{1}{2}$ | 1.5708 | .25 | .125 | .1963 | .4331 |
| $\frac{9}{16}$ | 1.7671 | .3164 | .17797 | .2485 | .4995 |
| $\frac{5}{8}$ | 1.9635 | .3906 | .24414 | .3068 | .5438 |
| $\frac{11}{16}$ | 2.1598 | .4726 | .32495 | .3712 | .6093 |
| $\frac{3}{4}$ | 2.3562 | .5625 | .42187 | .4417 | .6646 |
| $\frac{13}{16}$ | 2.5525 | .6601 | .53637 | .5185 | .7200 |
| $\frac{7}{8}$ | 2.7489 | .7656 | .66992 | .6013 | .7754 |
| $\frac{15}{16}$ | 2.9452 | .8789 | .81397 | .6903 | .8308 |
| 1 in. | 3.1416 | 1 | 1 | .7854 | .8862 |
| $\frac{1}{16}$ | 3.3379 | 1.1289 | 1.19946 | .8861 | .9416 |
| $\frac{1}{8}$ | 3.5343 | 1.2656 | 1.42381 | .9940 | .9969 |
| $\frac{3}{16}$ | 3.7306 | 1.4101 | 1.67456 | 1.1075 | 1.0524 |
| $\frac{1}{4}$ | 3.9270 | 1.5625 | 1.95312 | 1.2271 | 1.0775 |
| $\frac{5}{16}$ | 4.1233 | 1.7226 | 2.26098 | 1.3529 | 1.1631 |
| $\frac{3}{8}$ | 4.3197 | 1.8906 | 2.59960 | 1.4848 | 1.2185 |
| $\frac{7}{16}$ | 4.5160 | 2.0664 | 2.97045 | 1.6229 | 1.2740 |
| $\frac{1}{2}$ | 4.7124 | 2.25 | 3.375 | 1.7671 | 1.3293 |
| $\frac{9}{16}$ | 4.9087 | 2.4414 | 3.81469 | 1.9175 | 1.3846 |
| $\frac{5}{8}$ | 5.1051 | 2.6406 | 4.29101 | 2.0739 | 1.4401 |
| $\frac{11}{16}$ | 5.3014 | 2.8476 | 4.80541 | 2.2365 | 1.4954 |
| $\frac{3}{4}$ | 5.4978 | 3.0625 | 5.35937 | 2.4052 | 1.5508 |
| $\frac{13}{16}$ | 5.6941 | 3.2851 | 5.95434 | 2.5801 | 1.6062 |
| $\frac{7}{8}$ | 5.8905 | 3.5156 | 6.59179 | 2.7611 | 1.6616 |
| $\frac{15}{16}$ | 6.0868 | 3.7539 | 7.27319 | 2.9483 | 1.7170 |
| 2 in. | 6.2832 | 4 | 8 | 3.1416 | 1.7724 |
| $\frac{1}{16}$ | 6.4795 | 4.2539 | 8.7736 | 3.3411 | 1.8278 |
| $\frac{1}{8}$ | 6.6759 | 4.5156 | 9.5957 | 3.5465 | 1.8831 |
| $\frac{3}{16}$ | 6.8722 | 4.7851 | 10.4675 | 3.7582 | 1.9385 |
| $\frac{1}{4}$ | 7.0686 | 5.0625 | 11.3906 | 3.9760 | 1.9939 |
| $\frac{5}{16}$ | 7.2649 | 5.3476 | 12.3663 | 4.2001 | 2.0493 |
| $\frac{3}{8}$ | 7.4613 | 5.6406 | 13.3964 | 4.4302 | 2.1047 |
| $\frac{7}{16}$ | 7.6576 | 5.9414 | 14.4822 | 4.6664 | 2.1601 |
| $\frac{1}{2}$ | 7.8540 | 6.25 | 15.625 | 4.9087 | 2.2155 |
| $\frac{9}{16}$ | 8.0503 | 6.5664 | 16.8265 | 5.1573 | 2.2709 |
| $\frac{5}{8}$ | 8.2467 | 6.8906 | 18.0878 | 5.4119 | 2.3262 |
| $\frac{11}{16}$ | 8.4430 | 7.2226 | 19.4108 | 5.6727 | 2.3816 |
| $\frac{3}{4}$ | 8.6394 | 7.5625 | 20.7968 | 5.9395 | 2.4370 |
| $\frac{13}{16}$ | 8.8357 | 7.9101 | 22.2472 | 6.2126 | 2.4924 |
| $\frac{7}{8}$ | 9.0321 | 8.2656 | 23.7636 | 6.4918 | 2.5478 |
| $\frac{15}{16}$ | 9.2284 | 8.6289 | 25.3474 | 6.7772 | 2.6032 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|--------------------|---------|---------|----------|---------|-------------------|
| 3 in. | 9.4248 | 9 | 27 | 7.0686 | 2.6586 |
| $\frac{1}{8}$ in. | 9.6211 | 9.3789 | 28.7228 | 7.3662 | 2.7140 |
| $\frac{1}{4}$ in. | 9.8175 | 9.7656 | 30.5175 | 7.6699 | 2.7694 |
| $\frac{3}{8}$ in. | 10.0138 | 10.1601 | 32.3853 | 7.9798 | 2.8247 |
| $\frac{1}{2}$ in. | 10.2102 | 10.5625 | 34.3281 | 8.2957 | 2.8801 |
| $\frac{5}{8}$ in. | 10.4065 | 10.9726 | 36.3467 | 8.6179 | 2.9355 |
| $\frac{3}{4}$ in. | 10.6029 | 11.3906 | 38.4433 | 8.9462 | 2.9909 |
| $\frac{7}{8}$ in. | 10.7992 | 11.8164 | 40.6178 | 9.2806 | 3.0463 |
| $\frac{1}{2}$ in. | 10.9956 | 12.25 | 42.875 | 9.6211 | 3.1017 |
| $\frac{9}{8}$ in. | 11.1919 | 12.6914 | 45.2031 | 9.9678 | 3.1570 |
| $\frac{5}{4}$ in. | 11.3883 | 13.1406 | 47.6347 | 10.3206 | 3.2124 |
| $\frac{11}{8}$ in. | 11.5846 | 13.5976 | 49.9461 | 10.6796 | 3.2678 |
| $\frac{3}{2}$ in. | 11.7810 | 14.0625 | 52.7343 | 11.0446 | 3.3232 |
| $\frac{13}{8}$ in. | 11.9773 | 14.5351 | 55.3930 | 11.4159 | 3.3786 |
| $\frac{7}{4}$ in. | 12.1737 | 15.1056 | 58.1855 | 11.7932 | 3.4340 |
| $\frac{15}{8}$ in. | 12.3700 | 15.5039 | 61.0256 | 12.1768 | 3.4894 |
| 4 in. | 12.5664 | 16 | 64. | 12.5664 | 3.5448 |
| $\frac{1}{8}$ in. | 12.7627 | 16.5039 | 67.0471 | 12.9622 | 3.6002 |
| $\frac{1}{4}$ in. | 12.9591 | 17.0156 | 70.1894 | 13.3640 | 3.6555 |
| $\frac{3}{8}$ in. | 13.1554 | 17.5351 | 73.4282 | 13.7721 | 3.7110 |
| $\frac{1}{2}$ in. | 13.3518 | 18.0625 | 76.7656 | 14.1862 | 3.7663 |
| $\frac{5}{8}$ in. | 13.5481 | 18.5976 | 80.2021 | 14.6066 | 3.8217 |
| $\frac{3}{4}$ in. | 13.7445 | 19.1406 | 83.7402 | 15.0331 | 3.8771 |
| $\frac{7}{8}$ in. | 13.9408 | 19.6914 | 87.3804 | 15.4657 | 3.9325 |
| $\frac{1}{2}$ in. | 14.1372 | 20.25 | 91.125 | 15.9043 | 3.9880 |
| $\frac{9}{8}$ in. | 14.3335 | 20.8164 | 94.9748 | 16.3492 | 4.0433 |
| $\frac{5}{4}$ in. | 14.5299 | 21.3906 | 98.9316 | 16.8001 | 4.0987 |
| $\frac{11}{8}$ in. | 14.7262 | 21.9726 | 101.8965 | 17.2573 | 4.1541 |
| $\frac{3}{2}$ in. | 14.9226 | 22.5625 | 107.1718 | 17.7205 | 4.2095 |
| $\frac{13}{8}$ in. | 15.1189 | 23.1601 | 111.4679 | 18.1900 | 4.2648 |
| $\frac{7}{4}$ in. | 15.3153 | 23.7656 | 115.8574 | 18.6655 | 4.3202 |
| $\frac{15}{8}$ in. | 15.5716 | 24.3789 | 120.2708 | 19.1472 | 4.3756 |
| 5 in. | 15.7080 | 25 | 125 | 19.6350 | 4.4310 |
| $\frac{1}{8}$ in. | 15.9043 | 25.6289 | 129.7463 | 20.1290 | 4.4864 |
| $\frac{1}{4}$ in. | 16.1007 | 26.2656 | 134.6113 | 20.6290 | 4.5417 |
| $\frac{3}{8}$ in. | 16.2970 | 26.9101 | 138.5961 | 21.1252 | 4.5971 |
| $\frac{1}{2}$ in. | 16.4934 | 27.5625 | 144.7031 | 21.6475 | 4.6525 |
| $\frac{5}{8}$ in. | 16.6897 | 28.2226 | 149.9306 | 22.1661 | 4.7079 |
| $\frac{3}{4}$ in. | 16.8861 | 28.8906 | 155.2871 | 22.6907 | 4.7633 |
| $\frac{7}{8}$ in. | 17.0824 | 29.5664 | 160.7673 | 23.2215 | 4.8187 |
| $\frac{1}{2}$ in. | 17.2788 | 30.25 | 166.375 | 23.7583 | 4.8741 |
| $\frac{9}{8}$ in. | 17.4751 | 30.9414 | 172.1115 | 24.3014 | 4.9294 |
| $\frac{5}{4}$ in. | 17.6715 | 31.6406 | 177.9785 | 24.8505 | 4.9848 |
| $\frac{11}{8}$ in. | 17.8678 | 32.3476 | 183.9669 | 25.4058 | 5.0402 |
| $\frac{3}{2}$ in. | 18.0642 | 33.0625 | 190.1093 | 25.9672 | 5.0956 |
| $\frac{13}{8}$ in. | 18.2605 | 33.7851 | 196.3759 | 26.5348 | 5.1510 |
| $\frac{7}{4}$ in. | 18.4569 | 34.5156 | 202.7792 | 27.1085 | 5.2064 |
| $\frac{15}{8}$ in. | 18.6532 | 35.2539 | 209.3130 | 27.6884 | 5.2618 |

| Dis. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|-----------------|---------|---------|----------|---------|-------------------|
| 6 in. | 18.8496 | 36 | 216 | 28.2744 | 5.3172 |
| $\frac{1}{16}$ | 19.0459 | 36.7539 | 222.8205 | 28.8665 | 5.3726 |
| $\frac{1}{8}$ | 19.2423 | 37.5156 | 229.7832 | 29.4647 | 5.4280 |
| $\frac{3}{16}$ | 19.4386 | 38.2851 | 236.8890 | 30.0798 | 5.4834 |
| $\frac{1}{4}$ | 19.6350 | 39.0625 | 244.1406 | 30.6796 | 5.5388 |
| $\frac{5}{16}$ | 19.8313 | 39.8476 | 249.2654 | 31.2964 | 5.5942 |
| $\frac{3}{8}$ | 20.0277 | 40.6406 | 259.0839 | 31.9192 | 5.6495 |
| $\frac{7}{16}$ | 20.2240 | 41.4414 | 256.7605 | 32.5481 | 5.7049 |
| $\frac{1}{2}$ | 20.4204 | 42.25 | 274.625 | 33.1831 | 5.7603 |
| $\frac{9}{16}$ | 20.6167 | 43.0664 | 282.6232 | 33.8244 | 5.8157 |
| $\frac{5}{8}$ | 20.8131 | 43.8906 | 290.7753 | 34.4717 | 5.8711 |
| $\frac{11}{16}$ | 21.0094 | 44.7226 | 299.0823 | 35.1252 | 5.9265 |
| $\frac{3}{4}$ | 21.2058 | 45.5625 | 307.5468 | 35.7847 | 5.9819 |
| $\frac{13}{16}$ | 21.4021 | 46.4101 | 316.1688 | 36.4505 | 6.0373 |
| $\frac{7}{8}$ | 21.5985 | 47.2656 | 324.9511 | 37.1224 | 6.0927 |
| $\frac{15}{16}$ | 21.7948 | 48.1289 | 333.8943 | 37.8005 | 6.1480 |
| 7 in. | 21.9912 | 49 | 343 | 38.4846 | 6.2034 |
| $\frac{1}{16}$ | 22.1875 | 49.8789 | 349.5702 | 39.1749 | 6.2588 |
| $\frac{1}{8}$ | 22.3839 | 50.7656 | 361.7040 | 39.8713 | 6.3142 |
| $\frac{3}{16}$ | 22.5802 | 51.6601 | 371.3070 | 40.5469 | 6.3 96 |
| $\frac{1}{4}$ | 22.7766 | 52.5625 | 381.0781 | 41.2825 | 6.4350 |
| $\frac{5}{16}$ | 22.9729 | 53.4726 | 391.0184 | 41.9974 | 6.4904 |
| $\frac{3}{8}$ | 23.1693 | 54.3906 | 401.1308 | 42.7184 | 6.5358 |
| $\frac{7}{16}$ | 23.3656 | 55.3164 | 411.4158 | 43.4455 | 6.5912 |
| $\frac{1}{2}$ | 23.5620 | 56.25 | 421.875 | 44.1787 | 6.6465 |
| $\frac{9}{16}$ | 23.7583 | 57.1914 | 432.5100 | 44.9181 | 6.7020 |
| $\frac{5}{8}$ | 23.9547 | 58.1406 | 443.3222 | 45.6636 | 6.7573 |
| $\frac{11}{16}$ | 24.1510 | 59.0976 | 454.3129 | 46.4153 | 6.8127 |
| $\frac{3}{4}$ | 24.3474 | 60.0625 | 465.4843 | 47.1730 | 6.8681 |
| $\frac{13}{16}$ | 24.5437 | 61.0351 | 476.8368 | 47.9370 | 6.9235 |
| $\frac{7}{8}$ | 24.7401 | 62.0156 | 488.3730 | 48.7070 | 6.9789 |
| $\frac{15}{16}$ | 24.9364 | 63.0039 | 500.0935 | 49.4833 | 7.0343 |
| 8 in. | 25.1328 | 64 | 512 | 50.2656 | 7.0897 |
| $\frac{1}{16}$ | 25.3291 | 65.0039 | 524.1939 | 51.0541 | 7.1451 |
| $\frac{1}{8}$ | 25.5255 | 66.0156 | 536.3769 | 51.8486 | 7.2005 |
| $\frac{3}{16}$ | 25.7218 | 67.0351 | 548.8499 | 52.8994 | 7.2559 |
| $\frac{1}{4}$ | 25.9182 | 68.0625 | 561.5156 | 53.4562 | 7.3112 |
| $\frac{5}{16}$ | 26.1145 | 69.0976 | 574.3739 | 54.2748 | 7.3666 |
| $\frac{3}{8}$ | 26.3109 | 70.1406 | 587.4277 | 55.0885 | 7.4220 |
| $\frac{7}{16}$ | 26.5072 | 71.1914 | 600.6775 | 55.9138 | 7.4774 |
| $\frac{1}{2}$ | 26.7036 | 72.25 | 614.125 | 56.7451 | 7.5328 |
| $\frac{9}{16}$ | 26.8999 | 73.3164 | 627.7717 | 57.5887 | 7.5882 |
| $\frac{5}{8}$ | 27.0963 | 74.3906 | 641.6191 | 58.4264 | 7.6436 |
| $\frac{11}{16}$ | 27.2926 | 75.4726 | 655.6683 | 59.7762 | 7.6990 |
| $\frac{3}{4}$ | 27.4890 | 76.5625 | 669.9218 | 60.1321 | 7.7544 |
| $\frac{13}{16}$ | 27.6853 | 77.6601 | 684.3797 | 60.9943 | 7.8098 |
| $\frac{7}{8}$ | 27.8817 | 78.7656 | 699.0449 | 61.8625 | 7.8651 |
| $\frac{15}{16}$ | 28.0780 | 79.8789 | 713.9177 | 62.7369 | 7.9205 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|------------------|---------|----------|----------|----------|----------------------|
| 9 in. | 28.2744 | 81 | 729 | 63.6174 | 7.9760 |
| $\frac{1}{8}$ | 28.4707 | 82.1289 | 744.2932 | 64.5041 | 8.0312 |
| $\frac{1}{4}$ | 28.6671 | 83.2656 | 759.7988 | 65.3968 | 8.0866 |
| $\frac{3}{8}$ | 28.8634 | 84.4101 | 775.5378 | 66.2957 | 8.1420 |
| $\frac{1}{2}$ | 29.0598 | 85.5625 | 791.4531 | 67.2007 | 8.1974 |
| $\frac{5}{8}$ | 29.2561 | 86.7226 | 807.8043 | 68.1120 | 8.2527 |
| $\frac{3}{4}$ | 29.4525 | 87.8906 | 823.9746 | 69.0293 | 8.3081 |
| $\frac{7}{8}$ | 29.6483 | 89.0664 | 840.5642 | 69.9528 | 8.3635 |
| $\frac{1}{2}$ | 29.8452 | 90.25 | 857.375 | 70.8823 | 8.4190 |
| $\frac{9}{8}$ | 30.0415 | 91.4414 | 874.3084 | 71.8181 | 8.4743 |
| $\frac{5}{4}$ | 30.2379 | 92.6406 | 891.6660 | 72.7599 | 8.5297 |
| $\frac{11}{8}$ | 30.4342 | 93.8476 | 909.1487 | 73.7079 | 8.5851 |
| $\frac{3}{2}$ | 30.6306 | 95.0625 | 926.8593 | 74.6620 | 8.6405 |
| $\frac{13}{8}$ | 30.8269 | 96.2851 | 944.7976 | 75.6223 | 8.6959 |
| $\frac{7}{4}$ | 31.0233 | 97.5156 | 962.9667 | 76.5887 | 8.7513 |
| $\frac{15}{8}$ | 31.2196 | 98.7539 | 981.3669 | 77.5613 | 8.8066 |
| 10 in. | 31.4160 | 100 | 1000 | 78.5400 | 8.8620 |
| $\frac{1}{8}$ | 31.6123 | 101.2539 | 1018.860 | 79.5248 | 8.9174 |
| $\frac{1}{4}$ | 31.8087 | 102.5156 | 1037.970 | 80.5157 | 8.9728 |
| $\frac{3}{8}$ | 32.0050 | 103.7851 | 1057.310 | 81.5128 | 9.0282 |
| $\frac{1}{2}$ | 32.2014 | 105.0625 | 1076.890 | 82.5160 | 9.0836 |
| $\frac{5}{8}$ | 32.3977 | 106.3476 | 1096.709 | 83.5254 | 9.1390 |
| $\frac{3}{4}$ | 32.5941 | 107.6406 | 1116.771 | 84.5409 | 9.1943 |
| $\frac{7}{8}$ | 32.7904 | 108.9414 | 1137.075 | 85.5626 | 9.2497 |
| $\frac{1}{2}$ | 32.9868 | 110.25 | 1157.625 | 86.5903 | 9.3051 |
| $\frac{9}{8}$ | 33.1831 | 111.5664 | 1178.420 | 87.6243 | 9.3605 |
| $\frac{5}{4}$ | 33.3795 | 112.8906 | 1199.462 | 88.6643 | 9.4159 |
| $\frac{11}{8}$ | 33.5758 | 114.2226 | 1220.755 | 89.7105 | 9.4713 |
| $\frac{3}{2}$ | 33.7722 | 115.5625 | 1242.296 | 90.7627 | 9.5267 |
| $\frac{13}{8}$ | 33.9685 | 116.9101 | 1264.090 | 91.8212 | 9.5821 |
| $\frac{7}{4}$ | 34.1649 | 118.2656 | 1286.138 | 92.8858 | 9.6375 |
| $\frac{15}{8}$ | 34.3612 | 119.6289 | 1308.430 | 93.9566 | 9.6929 |
| 11 in. | 34.5576 | 121 | 1331 | 95.0334 | 9.7482 |
| $\frac{1}{8}$ | 34.7539 | 122.3789 | 1353.816 | 96.1164 | 9.8036 |
| $\frac{1}{4}$ | 34.9503 | 123.7656 | 1376.892 | 97.2053 | 9.8590 |
| $\frac{3}{8}$ | 35.1466 | 125.1601 | 1400.228 | 98.3008 | 9.9144 |
| $\frac{1}{2}$ | 35.3430 | 126.5625 | 1423.828 | 99.4021 | 9.9698 |
| $\frac{5}{8}$ | 35.5393 | 127.9726 | 1447.690 | 100.5097 | 10.0252 |
| $\frac{3}{4}$ | 35.7357 | 129.3906 | 1471.818 | 101.6234 | 10.0806 |
| $\frac{7}{8}$ | 35.9320 | 130.8164 | 1496.412 | 102.7432 | 10.1360 |
| $\frac{1}{2}$ | 36.1284 | 132.25 | 1520.875 | 103.8691 | 10.1914 |
| $\frac{9}{8}$ | 36.3247 | 133.6914 | 1535.796 | 105.0012 | 10.2467 |
| $\frac{5}{4}$ | 36.5211 | 135.1406 | 1571.009 | 106.1394 | 10.3021 |
| $\frac{11}{8}$ | 36.7174 | 136.5976 | 1596.534 | 107.2838 | 10.3575 |
| $\frac{3}{2}$ | 36.9138 | 138.0625 | 1622.234 | 108.4342 | 10.4130 |
| $\frac{13}{8}$ | 37.1101 | 139.5351 | 1648.358 | 109.5909 | 10.4683 |
| $\frac{7}{4}$ | 37.3065 | 141.0156 | 1674.560 | 110.7536 | 10.5237 |
| $\frac{15}{8}$ | 37.5028 | 142.5039 | 1701.140 | 111.9226 | 10.5791 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|---------|----------|----------|----------|-----------------|
| 12 in. | 37.6992 | 144 | 1728 | 113.0976 | 10.6345 |
| $\frac{1}{16}$ | 37.8955 | 145.5039 | 1755.160 | 114.2788 | 10.6899 |
| $\frac{1}{8}$ | 38.0919 | 147.0156 | 1782.564 | 115.4660 | 10.7453 |
| $\frac{3}{16}$ | 38.2882 | 148.5351 | 1810.271 | 116.6645 | 10.8007 |
| $\frac{1}{4}$ | 38.4846 | 150.0625 | 1838.265 | 117.8590 | 10.8560 |
| $\frac{5}{16}$ | 38.6809 | 151.5976 | 1866.539 | 119.0648 | 10.9114 |
| $\frac{3}{8}$ | 38.8773 | 153.1406 | 1895.115 | 120.2766 | 10.9668 |
| $\frac{7}{16}$ | 39.0736 | 154.6914 | 1923.974 | 121.4946 | 11.0222 |
| $\frac{1}{2}$ | 39.2700 | 156.25 | 1953.125 | 122.7187 | 11.0776 |
| $\frac{9}{16}$ | 39.4663 | 157.8164 | 1982.568 | 123.9490 | 11.1339 |
| $\frac{5}{8}$ | 39.6627 | 159.3906 | 2012.306 | 125.1854 | 11.1884 |
| $\frac{11}{16}$ | 39.8590 | 160.9726 | 2042.339 | 126.4479 | 11.2437 |
| $\frac{3}{4}$ | 40.0554 | 162.5625 | 2072.671 | 127.6765 | 11.2991 |
| $\frac{13}{16}$ | 40.2517 | 164.1601 | 2103.301 | 128.8999 | 11.3544 |
| $\frac{7}{8}$ | 40.4481 | 165.7656 | 2134.232 | 130.1923 | 11.4099 |
| $\frac{15}{16}$ | 40.6444 | 167.3789 | 2165.514 | 131.4279 | 11.4652 |
| 13 in. | 40.8408 | 169 | 2197 | 132.7326 | 11.5206 |
| $\frac{1}{16}$ | 41.0371 | 170.6289 | 2228.840 | 134.0120 | 11.5760 |
| $\frac{1}{8}$ | 41.2338 | 172.2656 | 2260.986 | 135.2974 | 11.6314 |
| $\frac{3}{16}$ | 41.4298 | 173.9101 | 2293.439 | 136.5890 | 11.6868 |
| $\frac{1}{4}$ | 41.6262 | 175.5625 | 2326.203 | 137.8867 | 11.7422 |
| $\frac{5}{16}$ | 41.8225 | 177.2226 | 2359.275 | 139.1907 | 11.7976 |
| $\frac{3}{8}$ | 42.0189 | 178.8906 | 2392.661 | 140.5007 | 11.8530 |
| $\frac{7}{16}$ | 42.2152 | 180.5664 | 2426.361 | 141.8169 | 11.9083 |
| $\frac{1}{2}$ | 42.4116 | 182.25 | 2460.375 | 143.1391 | 11.9637 |
| $\frac{9}{16}$ | 42.6079 | 183.9414 | 2494.705 | 144.4726 | 12.0191 |
| $\frac{5}{8}$ | 42.8043 | 185.6406 | 2529.353 | 145.8021 | 12.0745 |
| $\frac{11}{16}$ | 43.0006 | 187.3476 | 2564.321 | 147.1428 | 12.1299 |
| $\frac{3}{4}$ | 43.1970 | 189.0625 | 2599.609 | 148.4896 | 12.1853 |
| $\frac{13}{16}$ | 43.3933 | 190.7851 | 2634.819 | 149.8426 | 12.2407 |
| $\frac{7}{8}$ | 43.5897 | 192.5156 | 2671.154 | 151.2017 | 12.2961 |
| $\frac{15}{16}$ | 43.7860 | 194.2539 | 2707.413 | 152.5670 | 12.3515 |
| 14 in. | 43.9824 | 196 | 2744 | 153.9384 | 12.4068 |
| $\frac{1}{16}$ | 44.1787 | 197.7539 | 2780.914 | 155.3159 | 12.4622 |
| $\frac{1}{8}$ | 44.3751 | 199.5156 | 2818.157 | 156.6995 | 12.5176 |
| $\frac{3}{16}$ | 44.5714 | 201.2851 | 2855.732 | 158.0893 | 12.5730 |
| $\frac{1}{4}$ | 44.7676 | 203.0625 | 2893.640 | 159.4852 | 12.6284 |
| $\frac{5}{16}$ | 44.9641 | 204.8476 | 2931.781 | 160.8374 | 12.6838 |
| $\frac{3}{8}$ | 45.1605 | 206.6406 | 2970.458 | 162.2956 | 12.7392 |
| $\frac{7}{16}$ | 45.3568 | 208.4414 | 3009.372 | 163.7099 | 12.7946 |
| $\frac{1}{2}$ | 45.5532 | 210.25 | 3048.625 | 165.1303 | 12.8500 |
| $\frac{9}{16}$ | 45.7495 | 212.0664 | 3088.217 | 166.5569 | 12.9053 |
| $\frac{5}{8}$ | 45.9459 | 213.8906 | 3128.150 | 167.9896 | 12.9607 |
| $\frac{11}{16}$ | 46.1422 | 215.7226 | 3168.425 | 169.4285 | 13.0161 |
| $\frac{3}{4}$ | 46.3386 | 217.5625 | 3209.046 | 170.8735 | 13.0715 |
| $\frac{13}{16}$ | 46.5349 | 219.4101 | 3250.012 | 172.3247 | 13.1270 |
| $\frac{7}{8}$ | 46.7313 | 221.2656 | 3291.325 | 173.7820 | 13.1823 |
| $\frac{15}{16}$ | 46.9276 | 223.1289 | 3332.988 | 175.2455 | 13.2377 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|---------|----------|----------|----------|-----------------|
| 15 in. | 47.1240 | 225 | 3375 | 176.7150 | 13.2930 |
| $\frac{1}{16}$ | 47.3203 | 226.8789 | 3414.781 | 178.1907 | 13.3484 |
| $\frac{1}{8}$ | 47.5167 | 228.7656 | 3460.079 | 179.6725 | 13.4038 |
| $\frac{3}{16}$ | 47.7130 | 230.6601 | 3503.150 | 181.1105 | 13.4592 |
| $\frac{1}{4}$ | 47.9094 | 232.5625 | 3546.578 | 182.6545 | 13.5146 |
| $\frac{5}{16}$ | 48.1057 | 234.4726 | 3590.361 | 184.1548 | 13.5700 |
| $\frac{3}{8}$ | 48.3021 | 236.3906 | 3633.505 | 185.6612 | 13.6254 |
| $\frac{7}{16}$ | 48.4984 | 238.3164 | 3679.009 | 187.1737 | 13.6808 |
| $\frac{1}{2}$ | 48.6948 | 240.25 | 3723.875 | 188.6923 | 13.7361 |
| $\frac{9}{16}$ | 48.8911 | 242.1914 | 3769.103 | 190.2171 | 13.7915 |
| $\frac{5}{8}$ | 49.0875 | 244.1406 | 3814.696 | 191.7480 | 13.8470 |
| $\frac{11}{16}$ | 49.2838 | 246.0976 | 3860.856 | 193.3351 | 13.9023 |
| $\frac{3}{4}$ | 49.4802 | 248.0625 | 3906.984 | 194.8282 | 13.9577 |
| $\frac{13}{16}$ | 49.6765 | 250.0351 | 3953.680 | 196.3776 | 14.0131 |
| $\frac{7}{8}$ | 49.8729 | 252.0156 | 4000.747 | 197.9330 | 14.0685 |
| $\frac{15}{16}$ | 50.0692 | 254.0039 | 4048.187 | 199.4947 | 14.1240 |
| 16 in. | 50.2656 | 256 | 4096 | 201.0624 | 14.1792 |
| $\frac{1}{16}$ | 50.4619 | 258.0039 | 4144.187 | 202.6363 | 14.2346 |
| $\frac{1}{8}$ | 50.6583 | 260.0156 | 4192.751 | 204.2162 | 14.2900 |
| $\frac{3}{16}$ | 50.8546 | 262.0351 | 4241.693 | 205.8024 | 14.3454 |
| $\frac{1}{4}$ | 51.0510 | 264.0625 | 4291.015 | 207.3946 | 14.4008 |
| $\frac{5}{16}$ | 51.2473 | 266.0976 | 4340.717 | 208.9931 | 14.4561 |
| $\frac{3}{8}$ | 51.4437 | 268.1406 | 4390.802 | 210.5976 | 14.5115 |
| $\frac{7}{16}$ | 51.6400 | 270.1914 | 4441.271 | 212.2083 | 14.5670 |
| $\frac{1}{2}$ | 51.8364 | 272.25 | 4492.125 | 213.8251 | 14.6223 |
| $\frac{9}{16}$ | 52.0327 | 274.3164 | 4544.366 | 215.4481 | 14.6777 |
| $\frac{5}{8}$ | 52.2291 | 276.3906 | 4594.993 | 217.0772 | 14.7331 |
| $\frac{11}{16}$ | 52.4254 | 278.4726 | 4657.011 | 218.7124 | 14.7885 |
| $\frac{3}{4}$ | 52.6218 | 280.5625 | 4699.421 | 220.3537 | 14.8439 |
| $\frac{13}{16}$ | 52.8181 | 282.6601 | 4752.223 | 222.0013 | 14.8993 |
| $\frac{7}{8}$ | 53.0145 | 284.7656 | 4805.419 | 223.6549 | 14.9547 |
| $\frac{15}{16}$ | 53.2108 | 286.8789 | 4859.011 | 225.3147 | 15.0101 |
| 17 in. | 53.4072 | 289 | 4913 | 226.9806 | 15.0654 |
| $\frac{1}{16}$ | 53.6035 | 291.1289 | 4967.286 | 228.6527 | 15.1208 |
| $\frac{1}{8}$ | 53.7999 | 293.2656 | 5022.173 | 230.3308 | 15.1762 |
| $\frac{3}{16}$ | 53.9962 | 295.4101 | 5077.361 | 232.0151 | 15.2316 |
| $\frac{1}{4}$ | 54.1926 | 297.5625 | 5132.953 | 233.7055 | 15.2869 |
| $\frac{5}{16}$ | 54.3889 | 299.7226 | 5188.947 | 235.4022 | 15.3424 |
| $\frac{3}{8}$ | 54.5853 | 301.8906 | 5245.349 | 237.1049 | 15.3977 |
| $\frac{7}{16}$ | 54.7816 | 304.0664 | 5302.157 | 238.8138 | 15.4531 |
| $\frac{1}{2}$ | 54.9780 | 306.25 | 5359.375 | 240.5287 | 15.5085 |
| $\frac{9}{16}$ | 55.1743 | 308.4414 | 5419.002 | 242.2499 | 15.5639 |
| $\frac{5}{8}$ | 55.3707 | 310.6406 | 5475.040 | 243.9771 | 15.6193 |
| $\frac{11}{16}$ | 55.5670 | 312.8476 | 5533.493 | 245.7105 | 15.6747 |
| $\frac{3}{4}$ | 55.7634 | 315.0625 | 5592.359 | 247.4500 | 15.7301 |
| $\frac{13}{16}$ | 55.9597 | 317.2851 | 5651.640 | 249.1952 | 15.7855 |
| $\frac{7}{8}$ | 56.1561 | 319.5156 | 5711.341 | 250.9475 | 15.8408 |
| $\frac{15}{16}$ | 56.3524 | 321.7539 | 5771.460 | 252.7050 | 15.8962 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|---------|----------|----------|----------|-----------------|
| 18 in. | 56.5488 | 324 | 5832 | 254.4696 | 15.9516 |
| $\frac{1}{16}$ | 56.7451 | 326.2539 | 5892.961 | 256.2398 | 16.0070 |
| $\frac{1}{8}$ | 56.9415 | 328.5156 | 5954.345 | 258.0161 | 16.0624 |
| $\frac{3}{16}$ | 57.1378 | 330.7851 | 6016.154 | 259.7986 | 16.1178 |
| $\frac{1}{4}$ | 57.3342 | 333.0625 | 6078.390 | 261.5872 | 16.1732 |
| $\frac{5}{16}$ | 57.5305 | 335.3476 | 6141.053 | 263.3820 | 16.2285 |
| $\frac{3}{8}$ | 57.7269 | 337.6406 | 6204.146 | 265.1829 | 16.2839 |
| $\frac{7}{16}$ | 57.9282 | 339.9414 | 6267.669 | 266.9900 | 16.3393 |
| $\frac{1}{2}$ | 58.1196 | 342.25 | 6331.625 | 268.8031 | 16.3947 |
| $\frac{9}{16}$ | 58.2159 | 344.5664 | 6396.010 | 270.6225 | 16.4501 |
| $\frac{5}{8}$ | 58.5123 | 346.8906 | 6460.837 | 272.4479 | 16.5055 |
| $\frac{11}{16}$ | 58.7806 | 349.2226 | 6566.497 | 274.2895 | 16.5609 |
| $\frac{3}{4}$ | 58.9056 | 351.5625 | 6591.796 | 276.1171 | 16.6163 |
| $\frac{13}{16}$ | 59.1013 | 353.9101 | 6658.933 | 277.9610 | 16.6717 |
| $\frac{7}{8}$ | 59.2977 | 356.2656 | 6724.513 | 279.8110 | 16.7270 |
| $\frac{15}{16}$ | 59.4940 | 358.6289 | 6791.534 | 281.672 | 16.7824 |
| 19 in. | 59.6904 | 361 | 6859 | 283.5294 | 16.8378 |
| $\frac{1}{16}$ | 59.8867 | 363.3789 | 6926.910 | 285.3978 | 16.8932 |
| $\frac{1}{8}$ | 60.0831 | 365.7656 | 6995.267 | 287.2723 | 16.9486 |
| $\frac{3}{16}$ | 60.2794 | 368.1601 | 7065.672 | 289.4030 | 17.0040 |
| $\frac{1}{4}$ | 60.4758 | 370.5625 | 7132.328 | 291.0397 | 17.0600 |
| $\frac{5}{16}$ | 60.6721 | 372.9726 | 7203.033 | 292.9324 | 17.1147 |
| $\frac{3}{8}$ | 60.8685 | 375.3906 | 7273.192 | 294.8312 | 17.1701 |
| $\frac{7}{16}$ | 61.0648 | 377.8164 | 7343.785 | 296.7367 | 17.2255 |
| $\frac{1}{2}$ | 61.2612 | 380.25 | 7414.875 | 298.6483 | 17.2809 |
| $\frac{9}{16}$ | 61.4575 | 382.6914 | 7486.410 | 300.5658 | 17.3363 |
| $\frac{5}{8}$ | 61.6539 | 385.1406 | 7558.384 | 302.4894 | 17.3917 |
| $\frac{11}{16}$ | 61.8502 | 387.5976 | 7630.827 | 304.4192 | 17.4471 |
| $\frac{3}{4}$ | 62.0466 | 390.0625 | 7703.734 | 306.3550 | 17.5025 |
| $\frac{13}{16}$ | 62.2429 | 392.5351 | 7777.111 | 308.2971 | 17.5579 |
| $\frac{7}{8}$ | 62.4393 | 395.0156 | 7850.935 | 310.2452 | 17.6132 |
| $\frac{15}{16}$ | 62.6356 | 397.5039 | 7925.234 | 312.1996 | 17.6686 |
| 20 in. | 62.8320 | 400 | 8000 | 314.1600 | 17.7240 |
| $\frac{1}{16}$ | 63.0283 | 402.5039 | 8075.234 | 316.1266 | 17.7794 |
| $\frac{1}{8}$ | 63.2247 | 405.0156 | 8150.939 | 318.0992 | 17.8348 |
| $\frac{3}{16}$ | 63.4210 | 407.5351 | 8227.114 | 320.0781 | 17.8902 |
| $\frac{1}{4}$ | 63.6174 | 410.0625 | 8303.765 | 322.0630 | 17.9456 |
| $\frac{5}{16}$ | 63.8137 | 412.5976 | 8380.888 | 324.0542 | 18.0010 |
| $\frac{3}{8}$ | 64.0101 | 415.1406 | 8458.489 | 326.0514 | 18.0563 |
| $\frac{7}{16}$ | 64.2064 | 417.6914 | 8536.567 | 328.0548 | 18.1117 |
| $\frac{1}{2}$ | 64.4028 | 420.25 | 8615.125 | 330.0643 | 18.1671 |
| $\frac{9}{16}$ | 64.5991 | 422.8164 | 8694.162 | 332.0800 | 18.2225 |
| $\frac{5}{8}$ | 64.7955 | 425.3906 | 8773.681 | 334.1018 | 18.2779 |
| $\frac{11}{16}$ | 64.9918 | 427.9726 | 8853.683 | 336.1297 | 18.3333 |
| $\frac{3}{4}$ | 65.1882 | 430.5625 | 8934.171 | 338.1637 | 18.3887 |
| $\frac{13}{16}$ | 65.3845 | 433.1601 | 9015.144 | 340.2040 | 18.4441 |
| $\frac{7}{8}$ | 65.5809 | 435.7656 | 9096.607 | 342.2503 | 18.4995 |
| $\frac{15}{16}$ | 65.7772 | 438.3789 | 9178.558 | 344.3028 | 18.5549 |

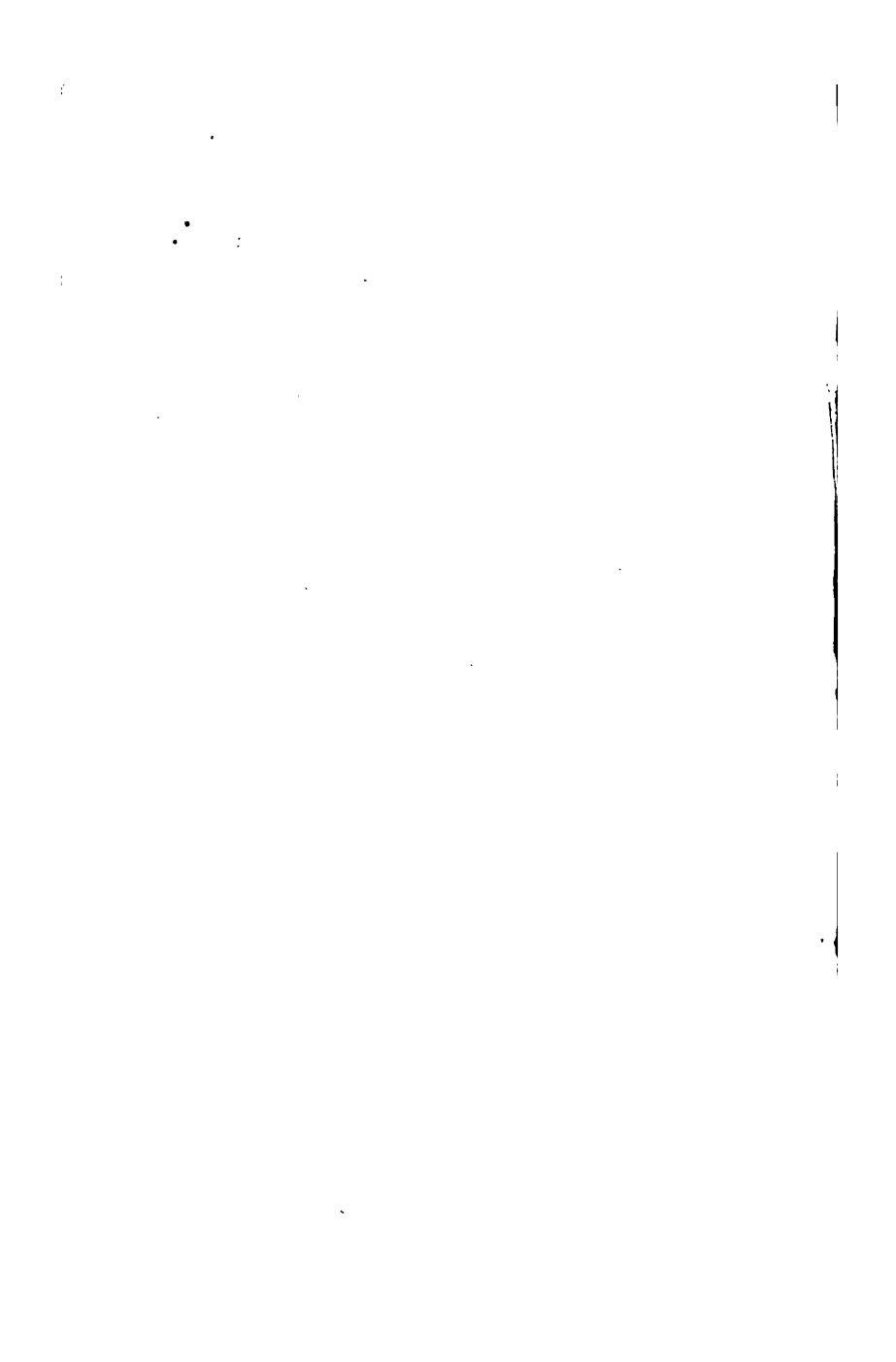
| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of — square. |
|-----------------|---------|----------|----------|----------|-------------------|
| 21 in. | 65.7936 | 441 | 9261 | 346.3614 | 18.6102 |
| $\frac{1}{16}$ | 66.1699 | 443.6289 | 9343.933 | 348.4267 | 18.6656 |
| $\frac{1}{8}$ | 66.3663 | 446.2656 | 9427.360 | 350.4970 | 18.7210 |
| $\frac{3}{16}$ | 66.5626 | 448.9101 | 9511.282 | 352.5740 | 18.7764 |
| $\frac{1}{4}$ | 66.7590 | 451.5625 | 9595.703 | 354.6571 | 18.8318 |
| $\frac{5}{16}$ | 66.9553 | 454.2226 | 9680.617 | 356.7465 | 18.8872 |
| $\frac{3}{8}$ | 67.1517 | 456.8906 | 9766.036 | 358.8419 | 18.9425 |
| $\frac{7}{16}$ | 67.3480 | 459.5664 | 9853.954 | 360.9435 | 18.9979 |
| $\frac{1}{2}$ | 67.5444 | 462.25 | 9938.375 | 363.0511 | 19.0533 |
| $\frac{9}{16}$ | 67.7407 | 464.9414 | 10025.29 | 365.1650 | 19.1087 |
| $\frac{5}{8}$ | 67.9371 | 467.6406 | 10112.72 | 367.2849 | 19.1641 |
| $\frac{11}{16}$ | 68.1334 | 470.3476 | 10200.66 | 369.4110 | 19.2195 |
| $\frac{3}{4}$ | 68.3298 | 473.0625 | 10289.11 | 371.5432 | 19.2749 |
| $\frac{13}{16}$ | 68.5261 | 475.7851 | 10378.06 | 373.6816 | 19.3303 |
| $\frac{7}{8}$ | 68.7225 | 478.5156 | 10467.52 | 375.8261 | 19.3857 |
| $\frac{15}{16}$ | 68.9188 | 481.2509 | 10557.54 | 377.9768 | 19.4410 |
| 22 in. | 69.1152 | 484 | 10648 | 380.1336 | 19.4964 |
| $\frac{1}{16}$ | 69.3115 | 486.7539 | 10739.00 | 382.2965 | 19.5518 |
| $\frac{1}{8}$ | 69.5079 | 489.5156 | 10830.53 | 384.4655 | 19.6072 |
| $\frac{3}{16}$ | 69.7042 | 492.2851 | 10922.57 | 386.6907 | 19.6626 |
| $\frac{1}{4}$ | 69.9006 | 495.0625 | 11015.14 | 388.8220 | 19.7180 |
| $\frac{5}{16}$ | 70.0969 | 497.8476 | 11108.22 | 391.0095 | 19.7734 |
| $\frac{3}{8}$ | 70.2933 | 500.6406 | 11201.83 | 393.2031 | 19.8287 |
| $\frac{7}{16}$ | 70.4806 | 503.4414 | 11295.96 | 395.4029 | 19.8841 |
| $\frac{1}{2}$ | 70.6860 | 506.25 | 11390.62 | 397.6087 | 19.9395 |
| $\frac{9}{16}$ | 70.8823 | 509.0664 | 11485.81 | 399.8207 | 19.9949 |
| $\frac{5}{8}$ | 71.0787 | 511.8906 | 11581.52 | 402.0388 | 20.0503 |
| $\frac{11}{16}$ | 71.2750 | 514.7226 | 11677.76 | 404.2631 | 20.1057 |
| $\frac{3}{4}$ | 71.4714 | 517.5625 | 11774.54 | 406.4935 | 20.1611 |
| $\frac{13}{16}$ | 71.6677 | 520.4101 | 11871.85 | 408.7301 | 20.2165 |
| $\frac{7}{8}$ | 71.8641 | 523.2656 | 11969.70 | 410.9728 | 20.2719 |
| $\frac{15}{16}$ | 72.0604 | 526.1289 | 12068.08 | 413.2317 | 20.3272 |
| 23 in. | 72.2568 | 529 | 12167 | 415.4766 | 20.3826 |
| $\frac{1}{16}$ | 72.4531 | 531.8789 | 12266.45 | 417.7377 | 20.4380 |
| $\frac{1}{8}$ | 72.6495 | 534.7656 | 12366.45 | 420.0049 | 20.4934 |
| $\frac{3}{16}$ | 72.8458 | 537.6601 | 12466.99 | 422.2783 | 20.5490 |
| $\frac{1}{4}$ | 73.0422 | 540.5625 | 12568.07 | 424.5577 | 20.6042 |
| $\frac{5}{16}$ | 73.2385 | 543.4726 | 12669.70 | 426.8434 | 20.6596 |
| $\frac{3}{8}$ | 73.4349 | 546.3906 | 12771.88 | 429.1352 | 20.7150 |
| $\frac{7}{16}$ | 73.6312 | 549.3164 | 12874.60 | 431.4331 | 20.7703 |
| $\frac{1}{2}$ | 73.8276 | 552.25 | 12977.87 | 433.7371 | 20.8257 |
| $\frac{9}{16}$ | 74.0239 | 555.1914 | 13081.69 | 436.0473 | 20.8811 |
| $\frac{5}{8}$ | 74.2203 | 558.1406 | 13185.98 | 438.3636 | 20.9365 |
| $\frac{11}{16}$ | 74.4166 | 561.0976 | 13290.99 | 440.6811 | 20.9919 |
| $\frac{3}{4}$ | 74.6130 | 564.0625 | 13396.48 | 443.0146 | 21.0473 |
| $\frac{13}{16}$ | 74.8093 | 567.0351 | 13502.52 | 445.3539 | 21.1027 |
| $\frac{7}{8}$ | 75.0057 | 570.0156 | 13609.12 | 447.6992 | 21.1581 |
| $\frac{15}{16}$ | 75.2020 | 573.0039 | 13716.28 | 450.0418 | 21.2134 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|-----------------|---------|----------|-----------|----------|-------------------|
| 24 in. | 75.3984 | 576 | 13824 | 452.3904 | 21.2688 |
| $\frac{1}{16}$ | 75.5947 | 579.0039 | 13932.281 | 454.7497 | 21.3242 |
| $\frac{1}{8}$ | 75.7911 | 582.0156 | 14041.126 | 457.1150 | 21.3796 |
| $\frac{3}{16}$ | 75.9874 | 585.0351 | 14150.536 | 459.4866 | 21.4350 |
| $\frac{1}{4}$ | 76.1838 | 588.0625 | 14260.515 | 461.8642 | 21.4904 |
| $\frac{5}{16}$ | 76.3801 | 591.0976 | 14371.060 | 464.2481 | 21.5558 |
| $\frac{3}{8}$ | 76.5765 | 594.1406 | 14482.177 | 466.6380 | 21.6012 |
| $\frac{7}{16}$ | 76.7728 | 597.1914 | 14593.864 | 469.0341 | 21.6566 |
| $\frac{1}{2}$ | 76.9692 | 600.25 | 14706.125 | 471.4363 | 21.7119 |
| $\frac{9}{16}$ | 77.1655 | 603.3164 | 14818.959 | 473.8447 | 21.7673 |
| $\frac{5}{8}$ | 77.3619 | 606.3906 | 14932.368 | 476.2592 | 21.8227 |
| $\frac{11}{16}$ | 77.5582 | 609.4726 | 15046.354 | 478.6798 | 21.8781 |
| $\frac{3}{4}$ | 77.7546 | 612.5625 | 15160.921 | 481.1065 | 21.9335 |
| $\frac{13}{16}$ | 77.9509 | 615.6601 | 15285.065 | 483.5395 | 21.9889 |
| $\frac{7}{8}$ | 78.1473 | 618.7656 | 15391.794 | 485.9785 | 22.0443 |
| $\frac{15}{16}$ | 78.3436 | 621.8789 | 15508.105 | 488.4237 | 22.0997 |
| 25 in. | 78.5400 | 625 | 15625 | 490.8750 | 22.1550 |
| $\frac{1}{16}$ | 78.7363 | 628.1289 | 15742.480 | 493.3325 | 22.2104 |
| $\frac{1}{8}$ | 78.9327 | 631.2656 | 15860.548 | 495.7960 | 22.2658 |
| $\frac{3}{16}$ | 79.1290 | 634.4101 | 15979.204 | 498.2657 | 22.3212 |
| $\frac{1}{4}$ | 79.3254 | 637.5625 | 16098.453 | 500.7415 | 22.3766 |
| $\frac{5}{16}$ | 79.5217 | 640.7226 | 16218.290 | 503.2236 | 22.4320 |
| $\frac{3}{8}$ | 79.7181 | 643.8906 | 16338.323 | 505.7117 | 22.4873 |
| $\frac{7}{16}$ | 79.9144 | 647.0664 | 16459.751 | 508.2060 | 22.5427 |
| $\frac{1}{2}$ | 80.1108 | 650.25 | 16581.375 | 510.7063 | 22.5981 |
| $\frac{9}{16}$ | 80.3071 | 653.4414 | 16703.595 | 513.2129 | 22.6535 |
| $\frac{5}{8}$ | 80.5035 | 656.6406 | 16826.415 | 515.7255 | 22.7089 |
| $\frac{11}{16}$ | 80.6998 | 659.8476 | 16949.824 | 518.2443 | 22.7643 |
| $\frac{3}{4}$ | 80.8962 | 663.0625 | 17073.859 | 520.7692 | 22.8197 |
| $\frac{13}{16}$ | 81.0925 | 666.2851 | 17195.482 | 523.3003 | 22.8751 |
| $\frac{7}{8}$ | 81.2889 | 669.5156 | 17323.716 | 525.8375 | 22.9305 |
| $\frac{15}{16}$ | 81.4852 | 672.7539 | 17449.552 | 528.3809 | 22.9858 |
| 26 in. | 81.6816 | 676 | 17576 | 530.9304 | 23.0412 |
| $\frac{1}{16}$ | 81.8779 | 679.2539 | 17703.054 | 533.4860 | 23.0966 |
| $\frac{1}{8}$ | 82.0743 | 682.5156 | 17830.720 | 536.0477 | 23.1520 |
| $\frac{3}{16}$ | 82.2706 | 685.7851 | 17952.708 | 538.6156 | 23.2074 |
| $\frac{1}{4}$ | 82.4670 | 689.0625 | 18087.890 | 541.1896 | 23.2628 |
| $\frac{5}{16}$ | 82.6633 | 692.3476 | 18217.396 | 543.7698 | 23.3182 |
| $\frac{3}{8}$ | 82.8597 | 695.6406 | 18347.520 | 546.3561 | 23.3735 |
| $\frac{7}{16}$ | 83.0560 | 698.9414 | 18468.254 | 548.9486 | 23.4289 |
| $\frac{1}{2}$ | 83.2524 | 702.25 | 18609.625 | 551.5471 | 23.4843 |
| $\frac{9}{16}$ | 83.4487 | 705.5664 | 18751.607 | 554.1519 | 23.5397 |
| $\frac{5}{8}$ | 83.6451 | 708.8906 | 18874.212 | 556.7627 | 23.5951 |
| $\frac{11}{16}$ | 83.8414 | 712.2226 | 19007.440 | 559.3797 | 23.6505 |
| $\frac{3}{4}$ | 84.0378 | 715.5625 | 19141.296 | 562.0027 | 23.7088 |
| $\frac{13}{16}$ | 84.2341 | 718.9101 | 19275.767 | 564.6320 | 23.7613 |
| $\frac{7}{8}$ | 84.4305 | 722.2656 | 19410.888 | 567.2674 | 23.8166 |
| $\frac{15}{16}$ | 84.6268 | 725.6289 | 19546.628 | 569.4090 | 23.8721 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of — square. |
|------------------|---------|----------|-----------|----------|----------------------|
| 27 in. | 84.8232 | 729 | 19683 | 572.5566 | 23.9274 |
| $\frac{1}{16}$ | 85.0195 | 732.3789 | 19820.003 | 575.2104 | 23.9628 |
| $\frac{1}{8}$ | 85.2159 | 735.7656 | 19957.642 | 577.8703 | 24.0332 |
| $\frac{3}{16}$ | 85.4122 | 739.1601 | 20058.957 | 580.5364 | 24.0936 |
| $\frac{1}{4}$ | 85.6086 | 742.5625 | 20234.828 | 583.2085 | 24.1490 |
| $\frac{5}{16}$ | 85.8049 | 745.9726 | 20374.376 | 585.8869 | 24.2044 |
| $\frac{3}{8}$ | 86.0013 | 749.3906 | 20514.567 | 588.5714 | 24.2598 |
| $\frac{7}{16}$ | 86.1976 | 752.8164 | 20655.399 | 591.2620 | 24.3192 |
| $\frac{1}{2}$ | 86.3940 | 756.25 | 20796.875 | 593.9587 | 24.3705 |
| $\frac{9}{16}$ | 86.5903 | 759.6914 | 20942.994 | 596.6616 | 24.4269 |
| $\frac{5}{8}$ | 86.7867 | 763.1406 | 21081.759 | 599.3706 | 24.4813 |
| $\frac{11}{16}$ | 86.9830 | 766.5976 | 21225.171 | 602.0858 | 24.5067 |
| $\frac{3}{4}$ | 87.1794 | 770.0625 | 21369.234 | 604.8070 | 24.5921 |
| $\frac{13}{16}$ | 87.3757 | 773.5351 | 21514.044 | 607.5345 | 24.6475 |
| $\frac{7}{8}$ | 87.5721 | 777.0156 | 21659.309 | 610.2680 | 24.7029 |
| $\frac{15}{16}$ | 87.7684 | 780.5039 | 21805.327 | 613.0078 | 24.7583 |
| 28 in. | 87.9648 | 784 | 21952 | 615.7536 | 24.8136 |
| $\frac{1}{16}$ | 88.1611 | 787.5039 | 22099.328 | 618.5051 | 24.8690 |
| $\frac{1}{8}$ | 88.3575 | 791.0156 | 22247.313 | 621.2636 | 24.9244 |
| $\frac{3}{16}$ | 88.5538 | 794.5351 | 22395.958 | 624.0279 | 24.9797 |
| $\frac{1}{4}$ | 88.7502 | 798.0625 | 22545.265 | 626.7982 | 25.0351 |
| $\frac{5}{16}$ | 88.9465 | 801.5976 | 22695.231 | 629.5748 | 25.0905 |
| $\frac{3}{8}$ | 89.1429 | 805.1406 | 22845.864 | 632.3574 | 25.1459 |
| $\frac{7}{16}$ | 89.3392 | 808.6914 | 22997.161 | 635.1462 | 25.2013 |
| $\frac{1}{2}$ | 89.5356 | 812.25 | 23149.125 | 637.9411 | 25.2567 |
| $\frac{9}{16}$ | 89.7319 | 815.8164 | 23301.755 | 640.7422 | 25.3121 |
| $\frac{5}{8}$ | 89.9283 | 819.3906 | 23455.056 | 643.5494 | 25.3675 |
| $\frac{11}{16}$ | 90.1246 | 822.9726 | 23609.026 | 646.3627 | 25.4229 |
| $\frac{3}{4}$ | 90.3210 | 826.5625 | 23763.671 | 649.1821 | 25.4783 |
| $\frac{13}{16}$ | 90.5173 | 830.1601 | 23919.007 | 652.0078 | 25.5337 |
| $\frac{7}{8}$ | 90.7137 | 833.7656 | 24074.981 | 654.8395 | 25.5891 |
| $\frac{15}{16}$ | 90.9100 | 837.3789 | 24231.651 | 657.6774 | 25.6446 |
| 29 in. | 91.1064 | 841 | 24389 | 660.5214 | 25.6998 |
| $\frac{1}{16}$ | 91.3027 | 844.6289 | 24547.027 | 663.3716 | 25.7524 |
| $\frac{1}{8}$ | 91.4991 | 848.2656 | 24705.735 | 666.2278 | 25.8106 |
| $\frac{3}{16}$ | 91.6954 | 851.9101 | 24865.126 | 669.0902 | 25.8660 |
| $\frac{1}{4}$ | 91.8918 | 855.5625 | 25025.203 | 671.9587 | 25.9214 |
| $\frac{5}{16}$ | 92.0081 | 859.2226 | 25195.962 | 674.8335 | 26.9768 |
| $\frac{3}{8}$ | 92.2845 | 862.8906 | 25347.411 | 677.7143 | 26.0325 |
| $\frac{7}{16}$ | 92.4808 | 866.5664 | 25519.548 | 680.6013 | 26.0876 |
| $\frac{1}{2}$ | 92.6772 | 870.25 | 25672.375 | 683.4943 | 26.1429 |
| $\frac{9}{16}$ | 92.8735 | 873.9414 | 25835.892 | 686.3936 | 26.1983 |
| $\frac{5}{8}$ | 93.0699 | 877.6406 | 26000.102 | 689.2989 | 26.2537 |
| $\frac{11}{16}$ | 93.2662 | 881.3476 | 26165.006 | 692.2104 | 26.3091 |
| $\frac{3}{4}$ | 93.4626 | 885.0625 | 26330.609 | 695.1280 | 26.3645 |
| $\frac{13}{16}$ | 93.6589 | 888.7851 | 26496.905 | 698.0518 | 26.4799 |
| $\frac{7}{8}$ | 93.8553 | 892.5156 | 26663.903 | 700.9817 | 26.4783 |
| $\frac{15}{16}$ | 94.0516 | 896.2539 | 26831.521 | 703.9178 | 26.5307 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|----------|----------|-----------|----------|-----------------|
| 30 ins. | 94.2480 | 900 | 27000 | 706.8600 | 26.5860 |
| $\frac{1}{16}$ | 94.4443 | 903.7539 | 27249.101 | 709.8083 | 26.6413 |
| $\frac{1}{8}$ | 94.6407 | 907.5156 | 27338.907 | 712.7627 | 26.6967 |
| $\frac{3}{16}$ | 94.8370 | 911.2851 | 27463.846 | 715.7233 | 26.7521 |
| $\frac{1}{4}$ | 95.0334 | 915.0625 | 27680.640 | 718.6900 | 26.8075 |
| $\frac{5}{16}$ | 95.2297 | 918.8476 | 27852.567 | 721.6629 | 26.8629 |
| $\frac{3}{8}$ | 95.4261 | 922.6406 | 28025.208 | 724.6419 | 26.9183 |
| $\frac{7}{16}$ | 95.6224 | 926.4414 | 28198.561 | 727.6271 | 26.9737 |
| $\frac{1}{2}$ | 95.8188 | 930.25 | 28372.625 | 730.6183 | 27.0291 |
| $\frac{9}{16}$ | 96.0151 | 934.0664 | 28547.504 | 733.6158 | 27.0844 |
| $\frac{5}{8}$ | 96.2115 | 937.8906 | 28722.899 | 736.6193 | 27.1398 |
| $\frac{11}{16}$ | 96.4078 | 941.7226 | 28899.122 | 739.6290 | 27.1952 |
| $\frac{3}{4}$ | 96.6042 | 945.5625 | 29076.046 | 742.6447 | 27.2506 |
| $\frac{13}{16}$ | 96.8005 | 949.4101 | 29253.698 | 745.6667 | 27.3060 |
| $\frac{7}{8}$ | 96.9969 | 953.2656 | 29432.075 | 748.6948 | 27.3614 |
| $\frac{15}{16}$ | 97.1932 | 957.1289 | 29606.975 | 751.7291 | 27.4168 |
| 31 ins. | 97.3896 | 961 | 29791 | 754.7694 | 27.4722 |
| $\frac{1}{16}$ | 97.5859 | 964.8789 | 29979.550 | 757.8159 | 27.5275 |
| $\frac{1}{8}$ | 97.7823 | 968.7656 | 30152.829 | 760.8685 | 27.5829 |
| $\frac{3}{16}$ | 97.9786 | 972.6601 | 30296.203 | 763.9273 | 27.6383 |
| $\frac{1}{4}$ | 98.1750 | 976.5625 | 30517.578 | 766.9921 | 27.6937 |
| $\frac{5}{16}$ | 98.3713 | 980.4726 | 30701.048 | 770.0632 | 27.7491 |
| $\frac{3}{8}$ | 98.5677 | 984.3906 | 30885.255 | 773.1404 | 27.8045 |
| $\frac{7}{16}$ | 98.7648 | 988.3164 | 30946.712 | 776.2237 | 27.8599 |
| $\frac{1}{2}$ | 98.9684 | 992.25 | 31255.875 | 779.3131 | 27.9153 |
| $\frac{9}{16}$ | 99.1567 | 996.1914 | 31442.191 | 782.4087 | 27.9706 |
| $\frac{5}{8}$ | 99.3531 | 1000.140 | 31629.446 | 785.5104 | 28.0260 |
| $\frac{11}{16}$ | 99.5494 | 1004.097 | 31817.542 | 788.6183 | 28.0814 |
| $\frac{3}{4}$ | 99.7458 | 1008.062 | 32005.984 | 791.7322 | 28.1368 |
| $\frac{13}{16}$ | 99.9421 | 1012.035 | 32195.366 | 794.8524 | 28.1922 |
| $\frac{7}{8}$ | 100.1385 | 1016.015 | 32385.497 | 797.9786 | 28.2476 |
| $\frac{15}{16}$ | 100.3348 | 1020.003 | 32576.375 | 801.1111 | 28.3030 |
| ins. | 100.5312 | 1024 | 32768 | 804.2496 | 28.3584 |
| $\frac{1}{16}$ | 100.7275 | 1028.003 | 32960.375 | 807.3943 | 28.4137 |
| $\frac{1}{8}$ | 100.9240 | 1032.015 | 33153.501 | 810.5450 | 28.4691 |
| $\frac{3}{16}$ | 101.1202 | 1036.035 | 33295.578 | 813.7020 | 28.5245 |
| $\frac{1}{4}$ | 101.3166 | 1040.062 | 33542.015 | 816.8650 | 28.5799 |
| $\frac{5}{16}$ | 101.5130 | 1044.097 | 33737.403 | 820.0343 | 28.6352 |
| $\frac{3}{8}$ | 101.7093 | 1048.840 | 33956.314 | 823.2096 | 28.6912 |
| $\frac{7}{16}$ | 101.9056 | 1052.191 | 34180.258 | 826.3911 | 28.7466 |
| $\frac{1}{2}$ | 102.1020 | 1056.25 | 34328.125 | 829.5787 | 28.8015 |
| $\frac{9}{16}$ | 102.2983 | 1060.316 | 34526.552 | 832.7725 | 28.8568 |
| $\frac{5}{8}$ | 102.4947 | 1064.390 | 34725.743 | 835.9724 | 28.9122 |
| $\frac{11}{16}$ | 102.6910 | 1068.472 | 34925.698 | 839.1784 | 28.9676 |
| $\frac{3}{4}$ | 102.8874 | 1072.562 | 35026.421 | 842.3905 | 29.0230 |
| $\frac{13}{16}$ | 103.0837 | 1076.660 | 35327.909 | 845.6089 | 29.0784 |
| $\frac{7}{8}$ | 103.2801 | 1080.765 | 35530.169 | 848.8333 | 29.1338 |
| $\frac{15}{16}$ | 103.4764 | 1084.878 | 35733.198 | 852.0639 | 29.1892 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|-----------------|----------|----------|-----------|-----------|-------------------|
| 33 in. | 103.6728 | 1089 | 35937 | 855.3006 | 29.2446 |
| $\frac{1}{16}$ | 103.8691 | 1093.129 | 36141.577 | 858.5436 | 29.2999 |
| $\frac{1}{8}$ | 104.0655 | 1097.265 | 36354.928 | 861.7924 | 29.3553 |
| $\frac{3}{16}$ | 104.2618 | 1101.410 | 36553.144 | 865.0475 | 29.4107 |
| $\frac{1}{4}$ | 104.4582 | 1105.562 | 36759.944 | 868.3087 | 29.4661 |
| $\frac{5}{16}$ | 104.6545 | 1109.722 | 36967.614 | 871.5760 | 29.5215 |
| $\frac{3}{8}$ | 104.8509 | 1113.890 | 37256.088 | 874.8497 | 29.5769 |
| $\frac{7}{16}$ | 105.0472 | 1118.066 | 37385.332 | 878.1290 | 29.6323 |
| $\frac{1}{2}$ | 105.2436 | 1122.25 | 37595.375 | 881.4151 | 29.6877 |
| $\frac{9}{16}$ | 105.4399 | 1126.441 | 37806.176 | 884.7070 | 29.7431 |
| $\frac{5}{8}$ | 105.6363 | 1130.640 | 38017.784 | 888.0051 | 29.7985 |
| $\frac{11}{16}$ | 105.8326 | 1134.847 | 38230.158 | 891.3090 | 29.8539 |
| $\frac{3}{4}$ | 106.0290 | 1139.062 | 38443.352 | 894.6196 | 29.9092 |
| $\frac{13}{16}$ | 106.2253 | 1143.285 | 38657.324 | 897.9360 | 29.9646 |
| $\frac{7}{8}$ | 106.4217 | 1147.515 | 38872.088 | 901.2587 | 30.0200 |
| $\frac{15}{16}$ | 106.6180 | 1151.754 | 39087.651 | 904.5875 | 30.0754 |
| 34 in. | 106.8144 | 1156 | 39304 | 907.9224 | 30.1308 |
| $\frac{1}{16}$ | 107.0107 | 1160.254 | 39521.152 | 911.2645 | 30.1862 |
| $\frac{1}{8}$ | 107.2071 | 1164.515 | 39738.288 | 914.6105 | 30.2416 |
| $\frac{3}{16}$ | 107.4034 | 1168.785 | 39957.837 | 917.9640 | 30.2970 |
| $\frac{1}{4}$ | 107.5998 | 1173.062 | 40177.384 | 921.3232 | 30.3523 |
| $\frac{5}{16}$ | 107.7961 | 1177.347 | 40397.719 | 924.6883 | 30.4077 |
| $\frac{3}{8}$ | 107.9925 | 1181.640 | 40618.888 | 928.0605 | 30.4631 |
| $\frac{7}{16}$ | 108.1888 | 1185.941 | 40840.843 | 931.4380 | 30.5185 |
| $\frac{1}{2}$ | 108.3852 | 1190.25 | 41063.625 | 934.8223 | 30.5739 |
| $\frac{9}{16}$ | 108.5815 | 1194.566 | 41287.187 | 938.2121 | 30.6293 |
| $\frac{5}{8}$ | 108.7779 | 1198.890 | 41511.576 | 941.6087 | 30.6847 |
| $\frac{11}{16}$ | 108.9742 | 1203.222 | 41736.763 | 945.0110 | 30.7400 |
| $\frac{3}{4}$ | 109.1706 | 1207.562 | 41962.792 | 948.4195 | 30.7954 |
| $\frac{13}{16}$ | 109.3669 | 1211.910 | 42189.617 | 951.8341 | 30.8508 |
| $\frac{7}{8}$ | 109.5633 | 1216.265 | 42417.256 | 955.2550 | 30.9062 |
| $\frac{15}{16}$ | 109.7596 | 1220.629 | 42695.725 | 958.6820 | 30.9616 |
| 35 in. | 109.9560 | 1225 | 42875 | 962.1150 | 31.0170 |
| $\frac{1}{16}$ | 110.1523 | 1229.379 | 43105.081 | 965.5542 | 31.0724 |
| $\frac{1}{8}$ | 110.3487 | 1233.765 | 43352.016 | 968.9995 | 31.1278 |
| $\frac{3}{16}$ | 110.5450 | 1238.160 | 43567.755 | 972.4510 | 31.1831 |
| $\frac{1}{4}$ | 110.7414 | 1242.562 | 43800.320 | 975.9085 | 31.2386 |
| $\frac{5}{16}$ | 110.9377 | 1246.968 | 44033.557 | 979.3686 | 31.2939 |
| $\frac{3}{8}$ | 111.1341 | 1251.390 | 44267.944 | 982.8422 | 31.3493 |
| $\frac{7}{16}$ | 111.3304 | 1255.816 | 44502.979 | 986.3180 | 31.4047 |
| $\frac{1}{2}$ | 111.5263 | 1260.25 | 44738.875 | 989.8003 | 31.4601 |
| $\frac{9}{16}$ | 111.7231 | 1264.591 | 44972.017 | 993.2097 | 31.5155 |
| $\frac{5}{8}$ | 111.9195 | 1269.140 | 45213.120 | 996.7890 | 31.5709 |
| $\frac{11}{16}$ | 112.1158 | 1273.597 | 45451.493 | 1000.3472 | 31.6263 |
| $\frac{3}{4}$ | 112.3122 | 1278.062 | 45690.728 | 1003.7992 | 31.6817 |
| $\frac{13}{16}$ | 112.5086 | 1282.535 | 45930.784 | 1007.3030 | 31.7370 |
| $\frac{7}{8}$ | 112.7049 | 1287.015 | 46171.680 | 1010.8220 | 31.7924 |
| $\frac{15}{16}$ | 112.9012 | 1291.504 | 46413.425 | 1014.3472 | 31.8478 |



| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------------|----------|----------|-----------|-----------|-----------------|
| 36 $\frac{1}{16}$ in. | 113.0976 | 1296 | 46656 | 1017.8784 | 31.9032 |
| $\frac{1}{8}$ | 113.2939 | 1306.503 | 47115.796 | 1021.4158 | 31.9585 |
| $\frac{3}{16}$ | 113.4903 | 1308.015 | 47252.063 | 1024.9592 | 32.0139 |
| $\frac{1}{4}$ | 113.6866 | 1309.535 | 47388.801 | 1028.5089 | 32.0693 |
| $\frac{5}{16}$ | 113.8830 | 1314.062 | 47634.765 | 1032.0646 | 32.1247 |
| $\frac{3}{8}$ | 114.0793 | 1318.597 | 47881.565 | 1035.6266 | 32.1801 |
| $\frac{7}{16}$ | 114.2757 | 1323.140 | 48129.239 | 1039.1946 | 32.2355 |
| $\frac{1}{2}$ | 114.4720 | 1327.691 | 48377.795 | 1042.7913 | 32.2909 |
| $\frac{9}{16}$ | 114.6684 | 1332.25 | 48627.125 | 1046.3941 | 32.3463 |
| $\frac{5}{8}$ | 114.8647 | 1336.816 | 48877.349 | 1049.9581 | 32.4016 |
| $\frac{11}{16}$ | 115.0611 | 1341.390 | 49128.430 | 1053.5281 | 32.4570 |
| $\frac{3}{4}$ | 115.2572 | 1345.972 | 49380.360 | 1057.1269 | 32.5124 |
| $\frac{13}{16}$ | 115.4538 | 1350.562 | 49633.171 | 1060.7317 | 32.5678 |
| $\frac{7}{8}$ | 115.6501 | 1355.160 | 49886.831 | 1064.3428 | 32.6232 |
| $\frac{15}{16}$ | 115.8465 | 1359.765 | 50141.356 | 1067.9599 | 32.6786 |
| | 116.0428 | 1364.378 | 50396.745 | 1071.5832 | 32.7340 |
| 37 $\frac{1}{16}$ in. | 116.2392 | 1369 | 50653 | 1075.2126 | 32.7894 |
| $\frac{1}{8}$ | 116.4355 | 1373.628 | 51010.121 | 1078.8482 | 32.8447 |
| $\frac{3}{16}$ | 116.6319 | 1378.265 | 51168.110 | 1082.4898 | 32.9001 |
| $\frac{1}{4}$ | 116.8282 | 1382.910 | 51426.969 | 1086.1376 | 32.9555 |
| $\frac{5}{16}$ | 117.0246 | 1387.562 | 51686.703 | 1089.7915 | 33.0109 |
| $\frac{3}{8}$ | 117.2209 | 1392.222 | 52447.305 | 1093.4517 | 33.0663 |
| $\frac{7}{16}$ | 117.4173 | 1396.890 | 52208.786 | 1097.1179 | 33.0217 |
| $\frac{1}{2}$ | 117.6136 | 1401.566 | 52471.142 | 1100.7903 | 33.1771 |
| $\frac{9}{16}$ | 117.8100 | 1406.25 | 52734.375 | 1104.4687 | 33.2325 |
| $\frac{5}{8}$ | 118.0063 | 1410.941 | 52998.497 | 1108.1534 | 33.2878 |
| $\frac{11}{16}$ | 118.2027 | 1415.640 | 53263.477 | 1111.8441 | 33.3432 |
| $\frac{3}{4}$ | 118.3990 | 1420.347 | 53517.892 | 1115.5410 | 33.3986 |
| $\frac{13}{16}$ | 118.5954 | 1425.062 | 53796.109 | 1119.2440 | 33.4540 |
| $\frac{7}{8}$ | 118.7917 | 1429.785 | 54063.629 | 1122.9532 | 33.5094 |
| $\frac{15}{16}$ | 118.9881 | 1434.515 | 54332.278 | 1126.6685 | 33.5648 |
| | 119.1844 | 1439.253 | 54601.694 | 1130.3900 | 33.6202 |
| 38 $\frac{1}{16}$ in. | 119.3808 | 1444 | 54872 | 1134.1176 | 33.6756 |
| $\frac{1}{8}$ | 119.5771 | 1448.753 | 55143.195 | 1137.8513 | 33.7309 |
| $\frac{3}{16}$ | 119.7735 | 1453.515 | 55415.282 | 1141.5911 | 33.7863 |
| $\frac{1}{4}$ | 119.9698 | 1458.285 | 55687.252 | 1145.3371 | 33.8417 |
| $\frac{5}{16}$ | 120.1662 | 1463.062 | 55962.140 | 1149.0892 | 33.8971 |
| $\frac{3}{8}$ | 120.3625 | 1467.847 | 56236.915 | 1152.8475 | 33.9525 |
| $\frac{7}{16}$ | 120.5589 | 1472.640 | 56512.583 | 1156.6119 | 34.0079 |
| $\frac{1}{2}$ | 120.7552 | 1477.441 | 56789.213 | 1160.3825 | 34.0633 |
| $\frac{9}{16}$ | 120.9516 | 1482.25 | 57066.625 | 1164.1591 | 34.1187 |
| $\frac{5}{8}$ | 121.1479 | 1487.066 | 57244.998 | 1167.9420 | 34.1740 |
| $\frac{11}{16}$ | 121.3443 | 1491.890 | 57624.274 | 1171.7309 | 34.2294 |
| $\frac{3}{4}$ | 121.5406 | 1496.722 | 57904.455 | 1175.5260 | 34.2848 |
| $\frac{13}{16}$ | 121.7370 | 1501.562 | 58185.546 | 1179.3271 | 34.3402 |
| $\frac{7}{8}$ | 121.9333 | 1506.410 | 58467.542 | 1183.1345 | 34.3956 |
| $\frac{15}{16}$ | 122.1297 | 1511.265 | 58750.450 | 1186.9480 | 34.4510 |
| | 122.3260 | 1516.128 | 59034.251 | 1190.7677 | 34.5064 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|------------------|----------|----------|-----------|-----------|----------------------|
| 39 in. | 122.5224 | 1521 | 59319 | 1194.5934 | 34.5618 |
| $\frac{1}{16}$ | 122.7187 | 1525.878 | 59604.445 | 1198.4253 | 34.6171 |
| $\frac{1}{8}$ | 122.9151 | 1530.765 | 59891.204 | 1202.2633 | 34.6725 |
| $\frac{3}{16}$ | 123.1114 | 1535.660 | 60178.680 | 1206.1075 | 34.7279 |
| $\frac{1}{4}$ | 123.3078 | 1540.562 | 60466.078 | 1209.9577 | 34.7833 |
| $\frac{5}{16}$ | 123.5041 | 1545.472 | 60756.391 | 1213.8142 | 34.8387 |
| $\frac{3}{8}$ | 123.7005 | 1550.390 | 61046.629 | 1217.6768 | 34.8941 |
| $\frac{7}{16}$ | 123.8968 | 1555.316 | 61337.798 | 1221.5455 | 34.9495 |
| $\frac{1}{2}$ | 124.0932 | 1560.25 | 61629.875 | 1225.4203 | 35.0049 |
| $\frac{9}{16}$ | 124.2895 | 1565.191 | 61922.884 | 1229.3013 | 35.0602 |
| $\frac{5}{8}$ | 124.4859 | 1570.140 | 62216.822 | 1233.1884 | 35.1156 |
| $\frac{11}{16}$ | 124.6822 | 1575.097 | 62511.686 | 1237.0817 | 35.1710 |
| $\frac{3}{4}$ | 124.8786 | 1580.062 | 62807.484 | 1240.9810 | 35.2264 |
| $\frac{13}{16}$ | 125.0749 | 1585.035 | 63304.209 | 1244.8866 | 35.2818 |
| $\frac{7}{8}$ | 125.2713 | 1590.015 | 63401.872 | 1248.7982 | 35.3372 |
| $\frac{15}{16}$ | 125.4676 | 1595.003 | 63700.468 | 1252.7161 | 35.3926 |
| 40 in. | 125.6640 | 1600 | 64000 | 1256.6400 | 35.4480 |
| $\frac{1}{16}$ | 125.8603 | 1605.003 | 64300.468 | 1260.5701 | 35.5033 |
| $\frac{1}{8}$ | 126.0567 | 1610.015 | 64601.875 | 1264.5062 | 35.5587 |
| $\frac{3}{16}$ | 126.2530 | 1615.035 | 64894.223 | 1268.4486 | 35.6141 |
| $\frac{1}{4}$ | 126.4494 | 1620.062 | 65207.515 | 1272.3970 | 35.6695 |
| $\frac{5}{16}$ | 126.6457 | 1625.097 | 65511.747 | 1276.3517 | 35.7249 |
| $\frac{3}{8}$ | 126.8421 | 1630.140 | 65816.926 | 1280.3124 | 35.7803 |
| $\frac{7}{16}$ | 127.0384 | 1635.191 | 66123.052 | 1284.2793 | 35.8357 |
| $\frac{1}{2}$ | 127.2348 | 1640.25 | 66430.125 | 1288.2523 | 35.8911 |
| $\frac{9}{16}$ | 127.4311 | 1645.316 | 66738.146 | 1292.2315 | 35.9464 |
| $\frac{5}{8}$ | 127.6275 | 1650.390 | 67047.110 | 1296.2168 | 36.0018 |
| $\frac{11}{16}$ | 127.8238 | 1655.472 | 67357.041 | 1300.2082 | 36.0572 |
| $\frac{3}{4}$ | 128.0202 | 1660.562 | 67667.925 | 1304.2057 | 36.1126 |
| $\frac{13}{16}$ | 128.2165 | 1665.660 | 67971.590 | 1308.2095 | 36.1680 |
| $\frac{7}{8}$ | 128.4129 | 1670.765 | 68292.539 | 1312.2193 | 36.2234 |
| $\frac{15}{16}$ | 128.6092 | 1675.878 | 68706.292 | 1316.2353 | 36.2788 |
| 41 in. | 128.8056 | 1681 | 68921 | 1320.2574 | 36.3342 |
| $\frac{1}{16}$ | 129.0019 | 1686.128 | 69236.667 | 1324.2857 | 36.3895 |
| $\frac{1}{8}$ | 129.1983 | 1691.265 | 69553.297 | 1328.3200 | 36.4449 |
| $\frac{3}{16}$ | 129.3946 | 1696.410 | 69870.890 | 1332.3605 | 36.5003 |
| $\frac{1}{4}$ | 129.5910 | 1701.562 | 70189.453 | 1336.4071 | 36.5557 |
| $\frac{5}{16}$ | 129.7873 | 1706.722 | 70508.977 | 1340.4600 | 36.6111 |
| $\frac{3}{8}$ | 129.9837 | 1711.890 | 70829.473 | 1344.5189 | 36.6665 |
| $\frac{7}{16}$ | 130.1800 | 1717.066 | 71150.938 | 1348.5840 | 36.7219 |
| $\frac{1}{2}$ | 130.3764 | 1722.25 | 71473.375 | 1352.6551 | 36.7773 |
| $\frac{9}{16}$ | 130.5727 | 1727.441 | 71703.482 | 1356.7325 | 36.8326 |
| $\frac{5}{8}$ | 130.7691 | 1732.640 | 72121.164 | 1360.8159 | 36.8880 |
| $\frac{11}{16}$ | 130.9654 | 1737.847 | 72444.541 | 1364.9055 | 36.9434 |
| $\frac{3}{4}$ | 131.1618 | 1743.062 | 72772.859 | 1369.0012 | 36.9988 |
| $\frac{13}{16}$ | 131.3581 | 1748.285 | 73100.170 | 1373.1031 | 37.0542 |
| $\frac{7}{8}$ | 131.5545 | 1753.515 | 73428.465 | 1377.2111 | 37.1096 |
| $\frac{15}{16}$ | 131.7508 | 1758.753 | 73757.791 | 1381.3253 | 37.1650 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|-----------------|----------|----------|-----------|-----------|-------------------|
| 42 in. | 131.9472 | 1764 | 74088 | 1385.4456 | 37.2204 |
| $\frac{1}{16}$ | 132.1435 | 1769.253 | 74419.242 | 1389.5720 | 37.2757 |
| $\frac{1}{8}$ | 132.3399 | 1774.515 | 74751.469 | 1393.7045 | 37.3311 |
| $\frac{3}{16}$ | 132.5362 | 1779.785 | 75084.683 | 1397.8432 | 37.3865 |
| $\frac{1}{4}$ | 132.7326 | 1785.062 | 75418.890 | 1401.9880 | 37.4419 |
| $\frac{5}{16}$ | 132.9289 | 1790.347 | 75711.770 | 1406.1390 | 37.4973 |
| $\frac{3}{8}$ | 133.1253 | 1795.640 | 76090.270 | 1410.2961 | 37.5527 |
| $\frac{7}{16}$ | 133.3216 | 1800.941 | 76426.450 | 1414.4594 | 37.6081 |
| $\frac{1}{2}$ | 133.5180 | 1806.25 | 76765.625 | 1418.6287 | 37.6635 |
| $\frac{9}{16}$ | 133.7143 | 1811.566 | 77304.794 | 1422.8043 | 37.7188 |
| $\frac{5}{8}$ | 133.9107 | 1816.890 | 77444.961 | 1426.9859 | 37.7742 |
| $\frac{11}{16}$ | 134.1070 | 1822.222 | 77786.127 | 1431.1737 | 37.8296 |
| $\frac{3}{4}$ | 134.3034 | 1827.562 | 78128.296 | 1435.3675 | 37.8850 |
| $\frac{13}{16}$ | 134.4997 | 1832.910 | 78471.463 | 1439.5676 | 37.9404 |
| $\frac{7}{8}$ | 134.6961 | 1838.265 | 78815.637 | 1443.7738 | 37.9958 |
| $\frac{15}{16}$ | 134.8924 | 1843.628 | 79160.815 | 1447.9862 | 38.0512 |
| 43 in. | 135.0888 | 1849 | 79507 | 1452.2046 | 38.1066 |
| $\frac{1}{16}$ | 135.2851 | 1854.378 | 79854.191 | 1456.4292 | 38.1619 |
| $\frac{1}{8}$ | 135.4815 | 1859.765 | 80202.391 | 1460.6599 | 38.2173 |
| $\frac{3}{16}$ | 135.6778 | 1865.160 | 80551.601 | 1464.8968 | 38.2727 |
| $\frac{1}{4}$ | 135.8742 | 1870.562 | 80901.828 | 1469.1397 | 38.3281 |
| $\frac{5}{16}$ | 136.0705 | 1875.972 | 81253.063 | 1473.3839 | 38.3835 |
| $\frac{3}{8}$ | 136.2669 | 1881.390 | 81605.317 | 1477.6342 | 38.4389 |
| $\frac{7}{16}$ | 136.4632 | 1886.816 | 81958.587 | 1481.9006 | 38.4943 |
| $\frac{1}{2}$ | 136.6596 | 1892.25 | 82312.875 | 1486.1731 | 38.5497 |
| $\frac{9}{16}$ | 136.8559 | 1897.691 | 82668.181 | 1490.4468 | 38.6050 |
| $\frac{5}{8}$ | 137.0523 | 1903.140 | 83024.508 | 1494.7266 | 38.6604 |
| $\frac{11}{16}$ | 137.2436 | 1908.597 | 83382.857 | 1499.0126 | 38.7158 |
| $\frac{3}{4}$ | 137.4450 | 1914.062 | 83740.234 | 1503.3046 | 38.7712 |
| $\frac{13}{16}$ | 137.6413 | 1919.535 | 84099.631 | 1507.6029 | 38.8266 |
| $\frac{7}{8}$ | 137.8377 | 1925.015 | 84460.059 | 1511.9072 | 38.8820 |
| $\frac{15}{16}$ | 138.0340 | 1930.503 | 84831.515 | 1516.2178 | 38.9374 |
| 44 in. | 138.2304 | 1936 | 85184 | 1520.5344 | 38.9928 |
| $\frac{1}{16}$ | 138.4267 | 1941.503 | 85547.515 | 1524.8572 | 39.0481 |
| $\frac{1}{8}$ | 138.6231 | 1947.015 | 85912.063 | 1529.1860 | 39.1035 |
| $\frac{3}{16}$ | 138.8194 | 1952.535 | 86278.844 | 1533.5211 | 39.1589 |
| $\frac{1}{4}$ | 139.0158 | 1958.062 | 86644.265 | 1537.8622 | 39.2143 |
| $\frac{5}{16}$ | 139.2121 | 1963.597 | 87011.918 | 1542.2046 | 39.2697 |
| $\frac{3}{8}$ | 139.4085 | 1969.140 | 87380.614 | 1546.5530 | 39.3251 |
| $\frac{7}{16}$ | 139.6048 | 1974.691 | 87740.259 | 1550.9176 | 39.3805 |
| $\frac{1}{2}$ | 139.8012 | 1980.25 | 88121.125 | 1555.2883 | 39.4359 |
| $\frac{9}{16}$ | 139.9975 | 1985.816 | 88492.943 | 1559.6602 | 39.4912 |
| $\frac{5}{8}$ | 140.1939 | 1991.390 | 88865.805 | 1564.0382 | 39.5466 |
| $\frac{11}{16}$ | 140.3902 | 1996.972 | 89239.713 | 1568.4223 | 39.6020 |
| $\frac{3}{4}$ | 140.5866 | 2002.562 | 89614.652 | 1572.8125 | 39.6574 |
| $\frac{13}{16}$ | 140.7829 | 2008.160 | 89990.674 | 1577.2090 | 39.7128 |
| $\frac{7}{8}$ | 140.9793 | 2013.765 | 90367.731 | 1581.6115 | 39.7682 |
| $\frac{15}{16}$ | 141.1756 | 2019.378 | 90745.839 | 1586.0203 | 39.8236 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|----------|----------|------------|-----------|-----------------|
| 45 in. | 141.3720 | 2025 | 91125 | 1590.4350 | 39.8790 |
| $\frac{1}{16}$ | 141.5683 | 2030.628 | 91515.214 | 1594.4560 | 39.9343 |
| $\frac{1}{8}$ | 141.7647 | 2036.265 | 91886.485 | 1599.2830 | 39.9897 |
| $\frac{3}{16}$ | 141.9610 | 2041.910 | 92268.812 | 1603.7162 | 40.0451 |
| $\frac{1}{4}$ | 142.1574 | 2047.562 | 92652.203 | 1608.1555 | 40.1005 |
| $\frac{5}{16}$ | 142.3537 | 2053.222 | 93036.640 | 1612.5961 | 40.1559 |
| $\frac{3}{8}$ | 142.5501 | 2058.890 | 93422.161 | 1617.0427 | 40.2113 |
| $\frac{7}{16}$ | 142.7464 | 2064.566 | 93808.735 | 1621.5055 | 40.2667 |
| $\frac{1}{2}$ | 142.9428 | 2070.25 | 94196.375 | 1625.9743 | 40.3221 |
| $\frac{9}{16}$ | 143.1391 | 2075.941 | 94585.080 | 1630.4444 | 40.3774 |
| $\frac{5}{8}$ | 143.3355 | 2081.640 | 94974.852 | 1634.9205 | 40.4328 |
| $\frac{11}{16}$ | 143.5318 | 2087.347 | 95363.694 | 1639.4028 | 40.4882 |
| $\frac{3}{4}$ | 143.7282 | 2093.062 | 95757.609 | 1643.8912 | 40.5436 |
| $\frac{13}{16}$ | 143.9245 | 2098.735 | 96149.592 | 1648.3858 | 40.5990 |
| $\frac{7}{8}$ | 144.1209 | 2104.515 | 96544.653 | 1652.8865 | 40.6544 |
| $\frac{15}{16}$ | 144.3172 | 2110.253 | 97239.788 | 1657.3934 | 40.7098 |
| 46 in. | 144.5136 | 2116 | 97336 | 1661.9064 | 40.7652 |
| $\frac{1}{16}$ | 144.7099 | 2121.753 | 97733.289 | 1666.4255 | 40.8025 |
| $\frac{1}{8}$ | 144.9063 | 2127.515 | 98131.657 | 1670.9507 | 40.8759 |
| $\frac{3}{16}$ | 145.1026 | 2133.285 | 98531.103 | 1675.4821 | 40.9313 |
| $\frac{1}{4}$ | 145.2990 | 2139.062 | 98931.640 | 1680.0196 | 40.9867 |
| $\frac{5}{16}$ | 145.4953 | 2144.847 | 99333.254 | 1684.5583 | 41.0421 |
| $\frac{3}{8}$ | 145.6917 | 2150.640 | 99735.957 | 1689.1031 | 41.0975 |
| $\frac{7}{16}$ | 145.8880 | 2156.441 | 100139.447 | 1693.6641 | 41.1529 |
| $\frac{1}{2}$ | 146.0844 | 2162.25 | 100544.625 | 1698.2311 | 41.2083 |
| $\frac{9}{16}$ | 146.2807 | 2168.066 | 100950.601 | 1702.7994 | 41.2636 |
| $\frac{5}{8}$ | 146.4771 | 2173.890 | 101357.649 | 1707.3737 | 41.3190 |
| $\frac{11}{16}$ | 146.6734 | 2179.722 | 101765.778 | 1711.9542 | 41.3744 |
| $\frac{3}{4}$ | 146.8698 | 2185.562 | 102175.046 | 1716.5407 | 41.4298 |
| $\frac{13}{16}$ | 147.0661 | 2191.410 | 102185.385 | 1721.1335 | 41.4852 |
| $\frac{7}{8}$ | 147.2625 | 2197.265 | 102996.825 | 1725.7324 | 41.5406 |
| $\frac{15}{16}$ | 147.4588 | 2203.128 | 103413.900 | 1730.3375 | 41.5960 |
| 47 in. | 147.6552 | 2209 | 103823 | 1734.9486 | 41.6514 |
| $\frac{1}{16}$ | 147.8515 | 2214.878 | 104237.738 | 1739.5659 | 41.7067 |
| $\frac{1}{8}$ | 148.0479 | 2220.765 | 104653.579 | 1744.1893 | 41.7621 |
| $\frac{3}{16}$ | 148.2442 | 2226.660 | 105070.523 | 1748.8189 | 41.8175 |
| $\frac{1}{4}$ | 148.4406 | 2232.562 | 105488.578 | 1753.4545 | 41.8729 |
| $\frac{5}{16}$ | 148.6369 | 2238.472 | 105907.734 | 1758.0914 | 41.9283 |
| $\frac{3}{8}$ | 148.8333 | 2244.390 | 106328.004 | 1762.7344 | 41.9837 |
| $\frac{7}{16}$ | 149.0296 | 2250.316 | 106749.384 | 1767.3935 | 42.0391 |
| $\frac{1}{2}$ | 149.2260 | 2256.25 | 107171.875 | 1772.0587 | 42.0945 |
| $\frac{9}{16}$ | 149.4223 | 2262.191 | 107593.478 | 1776.7251 | 42.1498 |
| $\frac{5}{8}$ | 149.6187 | 2268.140 | 108020.196 | 1781.3976 | 42.2052 |
| $\frac{11}{16}$ | 149.8150 | 2274.097 | 108446.029 | 1786.0763 | 42.2606 |
| $\frac{3}{4}$ | 150.0114 | 2280.062 | 108872.984 | 1790.7610 | 42.3160 |
| $\frac{13}{16}$ | 150.2077 | 2286.035 | 109310.753 | 1795.4520 | 42.3714 |
| $\frac{7}{8}$ | 150.4041 | 2292.015 | 109730.246 | 1800.1490 | 42.4268 |
| $\frac{15}{16}$ | 150.6004 | 2298.003 | 110160.561 | 1804.8523 | 42.4822 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|-----------------|----------|----------|------------|-----------|-------------------|
| 48 in. | 150.7968 | 2304 | 110592 | 1809.5616 | 42.5376 |
| $\frac{1}{16}$ | 150.9931 | 2310.004 | 111024.610 | 1814.2551 | 42.5929 |
| $\frac{1}{8}$ | 151.1895 | 2316.015 | 111458.250 | 1818.9986 | 42.6483 |
| $\frac{3}{16}$ | 151.3858 | 2322.035 | 111993.066 | 1823.7264 | 42.7037 |
| $\frac{1}{4}$ | 151.5822 | 2328.062 | 112329.015 | 1828.4602 | 42.7591 |
| $\frac{5}{16}$ | 151.7785 | 2334.097 | 112855.090 | 1833.1953 | 42.8145 |
| $\frac{3}{8}$ | 151.9749 | 2340.140 | 113204.301 | 1837.9364 | 42.8699 |
| $\frac{7}{16}$ | 152.1712 | 2346.191 | 113643.645 | 1842.6937 | 42.9253 |
| $\frac{1}{2}$ | 152.3676 | 2352.25 | 114084.125 | 1847.4571 | 42.9807 |
| $\frac{9}{16}$ | 152.5639 | 2358.316 | 114725.740 | 1852.2167 | 43.0361 |
| $\frac{5}{8}$ | 152.7603 | 2364.390 | 114968.493 | 1856.9924 | 43.0915 |
| $\frac{11}{16}$ | 152.9566 | 2370.472 | 115412.384 | 1861.7892 | 43.1468 |
| $\frac{3}{4}$ | 153.1530 | 2376.562 | 115857.421 | 1866.5521 | 43.2022 |
| $\frac{13}{16}$ | 153.3493 | 2382.660 | 116303.596 | 1871.3413 | 43.2576 |
| $\frac{7}{8}$ | 153.5457 | 2388.765 | 116750.918 | 1876.1365 | 43.3130 |
| $\frac{15}{16}$ | 153.7420 | 2394.878 | 117199.386 | 1880.9379 | 43.3684 |
| 49 in. | 153.9384 | 2401 | 117649 | 1885.7454 | 43.4238 |
| $\frac{1}{16}$ | 154.1347 | 2407.129 | 118099.810 | 1890.5591 | 43.4791 |
| $\frac{1}{8}$ | 154.3311 | 2413.265 | 118551.672 | 1895.3788 | 43.5345 |
| $\frac{3}{16}$ | 154.5274 | 2419.410 | 119004.734 | 1900.2047 | 43.5899 |
| $\frac{1}{4}$ | 154.7238 | 2425.562 | 119458.953 | 1905.0367 | 43.6453 |
| $\frac{5}{16}$ | 154.9201 | 2431.722 | 119914.320 | 1909.8700 | 43.7007 |
| $\frac{3}{8}$ | 155.1165 | 2437.890 | 120370.848 | 1914.7093 | 43.7561 |
| $\frac{7}{16}$ | 155.3128 | 2444.066 | 120828.532 | 1919.5648 | 43.8115 |
| $\frac{1}{2}$ | 155.5092 | 2450.25 | 121287.375 | 1924.4263 | 43.8669 |
| $\frac{9}{16}$ | 155.7055 | 2456.441 | 121747.376 | 1929.2891 | 43.9223 |
| $\frac{5}{8}$ | 155.9019 | 2462.640 | 122208.539 | 1934.1579 | 43.9777 |
| $\frac{11}{16}$ | 156.0982 | 2468.847 | 122671.264 | 1939.0329 | 44.0330 |
| $\frac{3}{4}$ | 156.2946 | 2475.062 | 123134.359 | 1943.9140 | 44.0884 |
| $\frac{13}{16}$ | 156.4909 | 2481.285 | 123599.014 | 1948.8013 | 44.1438 |
| $\frac{7}{8}$ | 156.6873 | 2487.515 | 124064.336 | 1953.6947 | 44.1992 |
| $\frac{15}{16}$ | 156.8836 | 2493.753 | 124531.835 | 1958.0943 | 44.2546 |
| 50 in. | 157.0800 | 2500 | 125000 | 1963.5000 | 44.3100 |
| $\frac{1}{16}$ | 157.2763 | 2506.254 | 125469.386 | 1968.4118 | 44.3653 |
| $\frac{1}{8}$ | 157.4727 | 2512.515 | 125939.844 | 1973.3297 | 44.4207 |
| $\frac{3}{16}$ | 157.6690 | 2518.785 | 126411.527 | 1978.2525 | 44.4761 |
| $\frac{1}{4}$ | 157.8654 | 2525.062 | 126884.390 | 1983.1840 | 44.5315 |
| $\frac{5}{16}$ | 158.0617 | 2531.347 | 127358.426 | 1988.6154 | 44.5869 |
| $\frac{3}{8}$ | 158.2581 | 2537.640 | 127833.645 | 1993.0529 | 44.6423 |
| $\frac{7}{16}$ | 158.4544 | 2543.941 | 128310.004 | 1998.0066 | 44.6977 |
| $\frac{1}{2}$ | 158.6508 | 2550.25 | 128787.625 | 2002.9663 | 44.7531 |
| $\frac{9}{16}$ | 158.8471 | 2556.566 | 129266.388 | 2007.9273 | 44.8085 |
| $\frac{5}{8}$ | 159.0435 | 2562.890 | 129746.336 | 2012.8943 | 44.8639 |
| $\frac{11}{16}$ | 159.2398 | 2569.222 | 130327.469 | 2017.8675 | 44.9192 |
| $\frac{3}{4}$ | 159.4362 | 2575.562 | 130709.797 | 2022.8467 | 44.9746 |
| $\frac{13}{16}$ | 159.6325 | 2581.910 | 131193.306 | 2027.8172 | 45.0300 |
| $\frac{7}{8}$ | 159.8289 | 2588.265 | 131678.012 | 2032.8238 | 45.0854 |
| $\frac{15}{16}$ | 160.0252 | 2594.628 | 132163.909 | 2037.8216 | 45.1408 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|-----------------|----------|----------|------------|-----------|-------------------|
| 51 in. | 160.2216 | 2601 | 132651 | 2042.8254 | 45.1962 |
| $\frac{1}{16}$ | 160.4179 | 2607.379 | 133139.336 | 2047.8354 | 45.2515 |
| $\frac{1}{8}$ | 160.6143 | 2613.765 | 133628.766 | 2052.8515 | 45.3069 |
| $\frac{3}{16}$ | 160.8106 | 2620.160 | 134119.445 | 2057.8798 | 45.3623 |
| $\frac{1}{4}$ | 161.0070 | 2626.562 | 134611.328 | 2062.9021 | 45.4177 |
| $\frac{5}{16}$ | 161.2033 | 2632.972 | 135104.406 | 2067.9317 | 45.4731 |
| $\frac{3}{8}$ | 161.3997 | 2639.390 | 135598.692 | 2072.9674 | 45.5285 |
| $\frac{7}{16}$ | 161.5960 | 2645.816 | 136094.181 | 2078.0293 | 45.5839 |
| $\frac{1}{2}$ | 161.7924 | 2652.25 | 136590.875 | 2083.0771 | 45.6393 |
| $\frac{9}{16}$ | 161.9887 | 2658.691 | 137088.775 | 2088.1362 | 45.6947 |
| $\frac{5}{8}$ | 162.1851 | 2665.140 | 137587.883 | 2093.2014 | 45.7501 |
| $\frac{11}{16}$ | 162.3814 | 2671.597 | 138088.220 | 2098.2678 | 45.8054 |
| $\frac{3}{4}$ | 162.5778 | 2678.062 | 138589.734 | 2103.3502 | 45.8608 |
| $\frac{13}{16}$ | 162.7741 | 2684.535 | 139092.474 | 2108.4339 | 45.9162 |
| $\frac{7}{8}$ | 162.9705 | 2691.015 | 139596.434 | 2113.5236 | 45.9716 |
| $\frac{15}{16}$ | 163.1668 | 2697.503 | 140101.557 | 2118.1196 | 46.0270 |
| 52 in. | 163.3632 | 2704 | 140608 | 2123.7216 | 46.0824 |
| $\frac{1}{16}$ | 163.5595 | 2710.504 | 141115.661 | 2128.8298 | 46.1377 |
| $\frac{1}{8}$ | 163.7559 | 2717.015 | 141624.438 | 2133.9440 | 46.1931 |
| $\frac{3}{16}$ | 163.9522 | 2723.535 | 142134.389 | 2139.0645 | 46.2485 |
| $\frac{1}{4}$ | 164.1486 | 2730.062 | 142645.765 | 2144.1910 | 46.3039 |
| $\frac{5}{16}$ | 164.3449 | 2736.597 | 143158.251 | 2149.3238 | 46.3593 |
| $\frac{3}{8}$ | 164.5413 | 2743.140 | 143671.989 | 2154.4626 | 46.4147 |
| $\frac{7}{16}$ | 164.7376 | 2749.691 | 144186.942 | 2159.6076 | 46.4701 |
| $\frac{1}{2}$ | 164.9340 | 2756.25 | 144703.125 | 2164.7587 | 46.5255 |
| $\frac{9}{16}$ | 165.1303 | 2762.816 | 145219.537 | 2169.9160 | 46.5809 |
| $\frac{5}{8}$ | 165.3267 | 2769.390 | 145739.180 | 2175.0794 | 46.6363 |
| $\frac{11}{16}$ | 165.5230 | 2775.972 | 146260.052 | 2180.2489 | 46.6916 |
| $\frac{3}{4}$ | 165.7194 | 2782.562 | 146780.172 | 2185.4245 | 46.7470 |
| $\frac{13}{16}$ | 165.9157 | 2789.160 | 146953.872 | 2190.6064 | 46.8024 |
| $\frac{7}{8}$ | 166.1121 | 2795.765 | 147826.106 | 2195.7943 | 46.8578 |
| $\frac{15}{16}$ | 166.3084 | 2802.378 | 148350.893 | 2200.9884 | 46.9132 |
| 53 in. | 166.5048 | 2809 | 148877 | 2206.1886 | 46.9686 |
| $\frac{1}{16}$ | 166.7011 | 2815.629 | 149404.361 | 2211.3950 | 47.0239 |
| $\frac{1}{8}$ | 166.8975 | 2822.265 | 149932.860 | 2216.6074 | 47.0793 |
| $\frac{3}{16}$ | 167.0938 | 2828.910 | 150462.655 | 2221.8260 | 47.1347 |
| $\frac{1}{4}$ | 167.2902 | 2835.562 | 150993.703 | 2227.0507 | 47.1901 |
| $\frac{5}{16}$ | 167.4865 | 2842.222 | 151525.992 | 2232.2817 | 47.2455 |
| $\frac{3}{8}$ | 167.6829 | 2848.890 | 152059.535 | 2237.5187 | 47.3009 |
| $\frac{7}{16}$ | 167.8792 | 2855.566 | 152594.329 | 2242.7619 | 47.3563 |
| $\frac{1}{2}$ | 168.0756 | 2862.25 | 153130.375 | 2248.0111 | 47.4117 |
| $\frac{9}{16}$ | 168.2719 | 2868.941 | 153667.673 | 2253.2666 | 47.4671 |
| $\frac{5}{8}$ | 168.4683 | 2875.640 | 154206.227 | 2258.5281 | 47.5225 |
| $\frac{11}{16}$ | 168.6646 | 2882.347 | 154746.036 | 2263.7908 | 47.5778 |
| $\frac{3}{4}$ | 168.8610 | 2889.062 | 155287.109 | 2269.0696 | 47.6332 |
| $\frac{13}{16}$ | 169.0573 | 2895.785 | 155829.336 | 2274.3496 | 47.6886 |
| $\frac{7}{8}$ | 169.2537 | 2902.515 | 156373.028 | 2279.6357 | 47.7440 |
| $\frac{15}{16}$ | 169.4500 | 2909.253 | 156917.882 | 2284.9280 | 47.7994 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|----------|----------|------------|-----------|-----------------|
| 54 in. | 169.6464 | 2916 | 157464 | 2290.2264 | 47.8548 |
| $\frac{1}{16}$ | 169.8427 | 2922.754 | 158011.436 | 2295.5309 | 47.9101 |
| $\frac{1}{8}$ | 170.0391 | 2929.515 | 158560.032 | 2300.8415 | 47.9655 |
| $\frac{3}{16}$ | 170.2354 | 2936.285 | 159109.948 | 2306.1583 | 48.0209 |
| $\frac{1}{4}$ | 170.4318 | 2943.062 | 159661.140 | 2311.4812 | 48.0763 |
| $\frac{5}{16}$ | 170.6281 | 2949.847 | 160213.597 | 2316.8163 | 48.1317 |
| $\frac{3}{8}$ | 170.8245 | 2956.640 | 160767.332 | 2322.1455 | 48.1871 |
| $\frac{7}{16}$ | 171.0208 | 2963.441 | 161322.541 | 2327.4819 | 48.2425 |
| $\frac{1}{2}$ | 171.2172 | 2970.25 | 161878.625 | 2332.8343 | 48.2979 |
| $\frac{9}{16}$ | 171.4135 | 2977.066 | 162436.185 | 2338.1880 | 48.3533 |
| $\frac{5}{8}$ | 171.6099 | 2983.890 | 162995.024 | 2343.5477 | 48.4087 |
| $\frac{11}{16}$ | 171.8062 | 2990.722 | 163554.242 | 2348.9636 | 48.4640 |
| $\frac{3}{4}$ | 172.0026 | 2997.562 | 164116.547 | 2354.2855 | 48.5194 |
| $\frac{13}{16}$ | 172.1989 | 3004.410 | 164679.328 | 2359.6637 | 48.5748 |
| $\frac{7}{8}$ | 172.3953 | 3011.265 | 165243.199 | 2365.0480 | 48.6302 |
| $\frac{15}{16}$ | 172.5916 | 3018.128 | 165808.456 | 2370.4385 | 48.6856 |
| 55 in. | 172.7880 | 3025 | 166375 | 2375.8350 | 48.7410 |
| $\frac{1}{16}$ | 172.9843 | 3031.879 | 166942.886 | 2381.2382 | 48.7963 |
| $\frac{1}{8}$ | 173.1807 | 3038.765 | 167511.953 | 2386.6465 | 48.8517 |
| $\frac{3}{16}$ | 173.3770 | 3045.660 | 168085.866 | 2392.0515 | 48.9071 |
| $\frac{1}{4}$ | 173.5734 | 3052.562 | 168654.078 | 2397.4825 | 48.9625 |
| $\frac{5}{16}$ | 173.7697 | 3059.472 | 169225.578 | 2402.9098 | 49.0179 |
| $\frac{3}{8}$ | 173.9661 | 3066.390 | 169801.379 | 2408.3432 | 49.0733 |
| $\frac{7}{16}$ | 174.1624 | 3073.316 | 170379.779 | 2413.7777 | 49.1287 |
| $\frac{1}{2}$ | 174.3588 | 3080.25 | 170953.875 | 2419.2283 | 49.1841 |
| $\frac{9}{16}$ | 174.5551 | 3087.191 | 171532.072 | 2424.7026 | 49.2395 |
| $\frac{5}{8}$ | 174.7515 | 3094.140 | 172111.570 | 2430.1830 | 49.2949 |
| $\frac{11}{16}$ | 174.9478 | 3101.097 | 172692.372 | 2435.6246 | 49.3502 |
| $\frac{3}{4}$ | 175.1442 | 3108.062 | 173274.484 | 2441.0722 | 49.4056 |
| $\frac{13}{16}$ | 175.3405 | 3115.035 | 173856.496 | 2446.5486 | 49.4610 |
| $\frac{7}{8}$ | 175.5369 | 3122.015 | 174442.621 | 2452.0310 | 49.5164 |
| $\frac{15}{16}$ | 175.7332 | 3129.003 | 175028.655 | 2457.0197 | 49.5718 |
| 56 in. | 175.9296 | 3136. | 175616 | 2463.0144 | 49.6272 |
| $\frac{1}{16}$ | 176.1259 | 3143.004 | 176204.712 | 2468.5153 | 49.6825 |
| $\frac{1}{8}$ | 176.3223 | 3150.015 | 176794.625 | 2474.0222 | 49.7379 |
| $\frac{3}{16}$ | 176.5186 | 3157.035 | 177385.909 | 2479.5354 | 49.7933 |
| $\frac{1}{4}$ | 176.7150 | 3164.062 | 177978.515 | 2485.0546 | 49.8487 |
| $\frac{5}{16}$ | 176.9113 | 3171.097 | 178572.433 | 2490.5361 | 49.9041 |
| $\frac{3}{8}$ | 177.1077 | 3178.140 | 179167.676 | 2496.1116 | 49.9595 |
| $\frac{7}{16}$ | 177.3040 | 3185.191 | 179764.239 | 2501.6493 | 50.0149 |
| $\frac{1}{2}$ | 177.5004 | 3192.25 | 180362.125 | 2507.1931 | 50.0703 |
| $\frac{9}{16}$ | 177.6967 | 3199.316 | 180961.343 | 2512.7431 | 50.1257 |
| $\frac{5}{8}$ | 177.8931 | 3206.390 | 181561.867 | 2518.2992 | 50.1811 |
| $\frac{11}{16}$ | 178.0894 | 3213.472 | 182163.728 | 2523.8614 | 50.2364 |
| $\frac{3}{4}$ | 178.2858 | 3220.562 | 182766.921 | 2529.4297 | 50.2918 |
| $\frac{13}{16}$ | 178.4821 | 3227.660 | 183371.441 | 2535.0043 | 50.3472 |
| $\frac{7}{8}$ | 178.6785 | 3234.765 | 183977.293 | 2540.5849 | 50.4026 |
| $\frac{15}{16}$ | 178.8748 | 3241.878 | 184584.489 | 2546.1717 | 50.4580 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Slide of = square. |
|-----------------|----------|----------|------------|-----------|--------------------|
| 57 in. | 179.0712 | 3249 | 185193 | 2551.7646 | 50.5134 |
| $\frac{1}{16}$ | 179.2675 | 3256.129 | 185802.912 | 2557.3637 | 50.5687 |
| $\frac{1}{8}$ | 179.4639 | 3263.265 | 186414.047 | 2562.9688 | 50.6241 |
| $\frac{3}{16}$ | 179.6602 | 3270.410 | 187026.577 | 2568.5801 | 50.6795 |
| $\frac{1}{4}$ | 179.8566 | 3277.562 | 187640.453 | 2574.1975 | 50.7349 |
| $\frac{5}{16}$ | 180.0529 | 3284.722 | 188255.664 | 2579.8212 | 50.7903 |
| $\frac{3}{8}$ | 180.2493 | 3291.890 | 188872.223 | 2585.4509 | 50.8457 |
| $\frac{7}{16}$ | 180.4456 | 3299.066 | 189490.126 | 2591.0869 | 50.9011 |
| $\frac{1}{2}$ | 180.6420 | 3306.25 | 190109.375 | 2596.7287 | 50.9565 |
| $\frac{9}{16}$ | 180.8383 | 3313.441 | 190729.970 | 2602.3769 | 51.0119 |
| $\frac{5}{8}$ | 181.0347 | 3320.640 | 191351.914 | 2608.0311 | 51.0673 |
| $\frac{11}{16}$ | 181.2310 | 3327.847 | 191985.008 | 2613.6942 | 51.1226 |
| $\frac{3}{4}$ | 181.4274 | 3335.062 | 192599.859 | 2619.3580 | 51.1780 |
| $\frac{13}{16}$ | 181.6237 | 3342.285 | 193225.857 | 2625.0307 | 51.2334 |
| $\frac{7}{8}$ | 181.8201 | 3349.515 | 193853.215 | 2630.7095 | 51.2888 |
| $\frac{15}{16}$ | 182.0164 | 3356.753 | 194471.829 | 2636.3945 | 51.3442 |
| 58 in. | 182.2128 | 3364 | 195112 | 2642.0856 | 51.3996 |
| $\frac{1}{16}$ | 182.4091 | 3371.254 | 195743.487 | 2647.7328 | 51.4549 |
| $\frac{1}{8}$ | 182.6055 | 3378.515 | 196376.219 | 2653.4861 | 51.5103 |
| $\frac{3}{16}$ | 182.8018 | 3385.785 | 197010.370 | 2659.2565 | 51.5657 |
| $\frac{1}{4}$ | 182.9982 | 3393.062 | 197645.890 | 2664.9112 | 51.6211 |
| $\frac{5}{16}$ | 183.1945 | 3400.347 | 198282.869 | 2670.6330 | 51.6765 |
| $\frac{3}{8}$ | 183.3909 | 3407.640 | 198921.020 | 2676.3609 | 51.7319 |
| $\frac{7}{16}$ | 183.5872 | 3414.941 | 199561.638 | 2682.0950 | 51.7873 |
| $\frac{1}{2}$ | 183.7836 | 3422.25 | 200201.625 | 2687.8351 | 51.8427 |
| $\frac{9}{16}$ | 183.9799 | 3429.566 | 200743.982 | 2693.5814 | 51.8981 |
| $\frac{5}{8}$ | 184.1763 | 3436.890 | 201487.711 | 2699.3338 | 51.9535 |
| $\frac{11}{16}$ | 184.3726 | 3444.222 | 202132.813 | 2705.0924 | 52.0088 |
| $\frac{3}{4}$ | 184.5690 | 3451.562 | 202779.296 | 2710.8571 | 52.0642 |
| $\frac{13}{16}$ | 184.7653 | 3458.910 | 203027.158 | 2716.6280 | 52.1196 |
| $\frac{7}{8}$ | 184.9617 | 3466.265 | 204076.387 | 2722.4050 | 52.1750 |
| $\frac{15}{16}$ | 185.1580 | 3473.628 | 204729.005 | 2728.1882 | 52.2304 |
| 59 in. | 185.3544 | 3481 | 205379 | 2733.9774 | 52.2858 |
| $\frac{1}{16}$ | 185.5507 | 3488.379 | 206032.437 | 2739.7728 | 52.3411 |
| $\frac{1}{8}$ | 185.7471 | 3495.765 | 206687.141 | 2745.5743 | 52.3965 |
| $\frac{3}{16}$ | 185.9434 | 3503.160 | 207343.288 | 2751.3820 | 52.4519 |
| $\frac{1}{4}$ | 186.1398 | 3510.562 | 208000.828 | 2757.1957 | 52.5073 |
| $\frac{5}{16}$ | 186.3361 | 3517.972 | 208659.649 | 2763.0157 | 52.5627 |
| $\frac{3}{8}$ | 186.5325 | 3525.390 | 209320.066 | 2768.8418 | 52.6181 |
| $\frac{7}{16}$ | 186.7288 | 3532.816 | 209981.374 | 2774.6745 | 52.6735 |
| $\frac{1}{2}$ | 186.9252 | 3540.25 | 210644.875 | 2780.5123 | 52.7289 |
| $\frac{9}{16}$ | 187.1215 | 3547.691 | 211309.369 | 2786.3568 | 52.7843 |
| $\frac{5}{8}$ | 187.3179 | 3555.140 | 211975.258 | 2792.2074 | 52.8397 |
| $\frac{11}{16}$ | 187.5142 | 3562.597 | 212642.544 | 2798.0642 | 52.8950 |
| $\frac{3}{4}$ | 187.7106 | 3570.062 | 213311.234 | 2803.9270 | 52.9504 |
| $\frac{13}{16}$ | 187.9069 | 3577.535 | 213981.318 | 2809.7461 | 53.0058 |
| $\frac{7}{8}$ | 188.1033 | 3585.015 | 214642.809 | 2815.6712 | 53.0612 |
| $\frac{15}{16}$ | 188.2996 | 3592.503 | 215325.702 | 2821.5526 | 53.1166 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|------------------|----------|----------|------------|-----------|----------------------|
| 60 in. | 188.4960 | 3600 | 216000 | 2827.4400 | 53.1720 |
| $\frac{1}{16}$ | 188.6923 | 3607.503 | 216676.003 | 2833.3336 | 53.2274 |
| $\frac{1}{8}$ | 188.8887 | 3615.015 | 217352.813 | 2839.2332 | 53.2828 |
| $\frac{3}{16}$ | 189.0850 | 3622.535 | 218041.381 | 2845.1391 | 53.3381 |
| $\frac{1}{4}$ | 189.2814 | 3630.062 | 218711.265 | 2851.0510 | 53.3935 |
| $\frac{5}{16}$ | 189.4777 | 3637.597 | 219392.605 | 2856.9692 | 53.4489 |
| $\frac{3}{8}$ | 189.6741 | 3645.140 | 220075.363 | 2862.8934 | 53.5043 |
| $\frac{7}{16}$ | 189.8704 | 3652.691 | 221759.536 | 2868.8223 | 53.5597 |
| $\frac{1}{2}$ | 189.0668 | 3660.25 | 221445.125 | 2874.7603 | 53.6151 |
| $\frac{9}{16}$ | 190.2631 | 3667.816 | 222132.140 | 2880.7030 | 53.6705 |
| $\frac{5}{8}$ | 190.4595 | 3675.390 | 222820.555 | 2886.6517 | 53.7259 |
| $\frac{11}{16}$ | 190.6558 | 3682.972 | 223510.400 | 2892.6067 | 53.7813 |
| $\frac{3}{4}$ | 190.8522 | 3690.562 | 224201.672 | 2898.5677 | 53.8367 |
| $\frac{13}{16}$ | 191.0485 | 3698.160 | 224894.361 | 2904.5350 | 53.8920 |
| $\frac{7}{8}$ | 191.2449 | 3705.765 | 225588.481 | 2910.5083 | 53.9474 |
| $\frac{15}{16}$ | 191.4412 | 3713.378 | 226284.016 | 2916.4878 | 54.0028 |
| 61 in. | 191.6376 | 3721 | 226981 | 2922.4734 | 54.0582 |
| $\frac{1}{16}$ | 191.8339 | 3728.628 | 227679.402 | 2928.4652 | 54.1136 |
| $\frac{1}{8}$ | 192.0303 | 3736.265 | 228379.235 | 2934.4630 | 54.1680 |
| $\frac{3}{16}$ | 192.2266 | 3743.910 | 229079.699 | 2940.4670 | 54.2243 |
| $\frac{1}{4}$ | 192.4230 | 3751.562 | 229783.203 | 2946.4771 | 54.2797 |
| $\frac{5}{16}$ | 192.6193 | 3759.222 | 230487.336 | 2952.4938 | 54.3351 |
| $\frac{3}{8}$ | 192.8157 | 3766.890 | 231192.911 | 2958.5159 | 54.3905 |
| $\frac{7}{16}$ | 193.0120 | 3774.566 | 231949.923 | 2964.5445 | 54.4459 |
| $\frac{1}{2}$ | 193.2084 | 3782.25 | 232608.375 | 2970.5791 | 54.5013 |
| $\frac{9}{16}$ | 193.4047 | 3789.941 | 233311.067 | 2976.6200 | 54.5567 |
| $\frac{5}{8}$ | 193.6011 | 3797.640 | 234029.602 | 2982.6669 | 54.6121 |
| $\frac{11}{16}$ | 193.7974 | 3805.347 | 234744.380 | 2988.7200 | 54.6675 |
| $\frac{3}{4}$ | 193.9938 | 3813.062 | 235456.609 | 2994.7792 | 54.7229 |
| $\frac{13}{16}$ | 194.1901 | 3820.785 | 236172.279 | 3000.8423 | 54.7782 |
| $\frac{7}{8}$ | 194.3865 | 3828.515 | 236889.403 | 3006.9161 | 54.8336 |
| $\frac{15}{16}$ | 194.5828 | 3836.253 | 237607.976 | 3012.9938 | 54.8890 |
| 62 in. | 194.7792 | 3844 | 238328 | 3019.0776 | 54.9444 |
| $\frac{1}{16}$ | 194.9755 | 3851.753 | 239050.476 | 3025.1675 | 54.9998 |
| $\frac{1}{8}$ | 195.1719 | 3859.515 | 239772.406 | 3031.2635 | 55.0552 |
| $\frac{3}{16}$ | 195.3682 | 3867.285 | 240496.792 | 3037.3607 | 55.1105 |
| $\frac{1}{4}$ | 195.5646 | 3875.062 | 241222.640 | 3043.4740 | 55.1659 |
| $\frac{5}{16}$ | 195.7609 | 3882.847 | 241948.941 | 3049.6885 | 55.2213 |
| $\frac{3}{8}$ | 195.9573 | 3890.640 | 242678.707 | 3055.7091 | 55.2767 |
| $\frac{7}{16}$ | 196.1536 | 3898.441 | 243408.935 | 3061.8359 | 55.3321 |
| $\frac{1}{2}$ | 196.3500 | 3906.25 | 244140.625 | 3067.9687 | 55.3875 |
| $\frac{9}{16}$ | 196.5463 | 3914.066 | 244873.779 | 3074.1578 | 55.4429 |
| $\frac{5}{8}$ | 196.7427 | 3921.890 | 245608.399 | 3080.2529 | 55.4983 |
| $\frac{11}{16}$ | 196.9390 | 3929.722 | 246344.485 | 3086.4042 | 55.5536 |
| $\frac{3}{4}$ | 197.1354 | 3937.562 | 247082.047 | 3092.5615 | 55.6090 |
| $\frac{13}{16}$ | 197.3317 | 3945.410 | 247821.072 | 3098.7251 | 55.6644 |
| $\frac{7}{8}$ | 197.5281 | 3953.265 | 248561.574 | 3104.8948 | 55.7198 |
| $\frac{15}{16}$ | 197.7244 | 3961.128 | 249309.650 | 3111.0707 | 55.7752 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|----------|----------|------------|-----------|-----------------|
| 63 in. | 197.9208 | 3969 | 250047 | 3117.2526 | 55.8306 |
| $\frac{1}{16}$ | 198.1171 | 3976.878 | 250791.925 | 3124.4407 | 55.8850 |
| $\frac{1}{8}$ | 198.3135 | 3984.765 | 251538.328 | 3129.6349 | 55.9414 |
| $\frac{3}{16}$ | 198.5098 | 3992.660 | 252286.210 | 3135.8353 | 55.9967 |
| $\frac{1}{4}$ | 198.7062 | 4000.562 | 253035.578 | 3142.0417 | 56.0521 |
| $\frac{5}{16}$ | 198.9025 | 4008.472 | 253786.921 | 3148.7544 | 56.1075 |
| $\frac{3}{8}$ | 199.0989 | 4016.390 | 254538.754 | 3154.4732 | 56.1629 |
| $\frac{7}{16}$ | 199.2952 | 4024.316 | 255292.571 | 3160.7981 | 56.2183 |
| $\frac{1}{2}$ | 199.4916 | 4032.25 | 256047.875 | 3166.9291 | 56.2737 |
| $\frac{9}{16}$ | 199.6879 | 4040.191 | 256804.665 | 3173.1663 | 56.3291 |
| $\frac{5}{8}$ | 199.8843 | 4048.140 | 257562.945 | 3179.4096 | 56.3845 |
| $\frac{11}{16}$ | 200.0806 | 4056.097 | 258322.715 | 3185.6591 | 56.4398 |
| $\frac{3}{4}$ | 200.2770 | 4064.062 | 259083.984 | 3191.9146 | 56.4952 |
| $\frac{13}{16}$ | 200.4733 | 4072.035 | 259856.739 | 3193.1764 | 56.5506 |
| $\frac{7}{8}$ | 200.6697 | 4080.015 | 260610.996 | 3204.4442 | 56.6060 |
| $\frac{15}{16}$ | 200.8660 | 4088.003 | 261376.749 | 3210.7183 | 56.6614 |
| 64 in. | 201.0624 | 4096 | 262144 | 3216.9984 | 56.7168 |
| $\frac{1}{16}$ | 201.2587 | 4104.003 | 262912.749 | 3223.2847 | 56.7721 |
| $\frac{1}{8}$ | 201.4551 | 4112.015 | 263683.000 | 3229.5770 | 56.8276 |
| $\frac{3}{16}$ | 201.6514 | 4120.035 | 264454.153 | 3235.8746 | 56.8829 |
| $\frac{1}{4}$ | 201.8478 | 4128.062 | 265228.015 | 3242.1782 | 56.9383 |
| $\frac{5}{16}$ | 202.0441 | 4136.097 | 266102.777 | 3248.4936 | 56.9937 |
| $\frac{3}{8}$ | 202.2405 | 4144.140 | 266779.051 | 3254.8080 | 57.0491 |
| $\frac{7}{16}$ | 202.4368 | 4152.191 | 267557.633 | 3261.1311 | 57.1045 |
| $\frac{1}{2}$ | 202.6332 | 4160.25 | 268336.125 | 3267.4603 | 57.1599 |
| $\frac{9}{16}$ | 202.8295 | 4168.316 | 269054.927 | 3273.7957 | 57.2153 |
| $\frac{5}{8}$ | 203.0259 | 4176.390 | 269899.242 | 3280.1372 | 57.2707 |
| $\frac{11}{16}$ | 203.2222 | 4184.472 | 270683.071 | 3286.4875 | 57.3261 |
| $\frac{3}{4}$ | 203.4186 | 4192.562 | 271468.422 | 3292.8385 | 57.3815 |
| $\frac{13}{16}$ | 203.6149 | 4200.650 | 272248.153 | 3299.1985 | 57.4368 |
| $\frac{7}{8}$ | 203.8113 | 4208.765 | 273043.668 | 3305.5645 | 57.4922 |
| $\frac{15}{16}$ | 204.0076 | 4216.878 | 273814.092 | 3311.9367 | 57.5476 |
| 65 in. | 204.2040 | 4225 | 274625 | 3318.3151 | 57.6030 |
| $\frac{1}{16}$ | 204.4003 | 4233.128 | 275417.949 | 3324.7495 | 57.6584 |
| $\frac{1}{8}$ | 204.5917 | 4241.265 | 276212.422 | 3331.0900 | 57.7138 |
| $\frac{3}{16}$ | 204.7930 | 4249.410 | 277198.283 | 3337.9857 | 57.7691 |
| $\frac{1}{4}$ | 204.9894 | 4257.562 | 277805.953 | 3343.8875 | 57.8245 |
| $\frac{5}{16}$ | 205.1857 | 4265.722 | 278606.007 | 3350.2976 | 57.8799 |
| $\frac{3}{8}$ | 205.3821 | 4273.890 | 279405.608 | 3356.7137 | 57.9353 |
| $\frac{7}{16}$ | 205.5784 | 4282.066 | 280207.720 | 3363.1350 | 57.9907 |
| $\frac{1}{2}$ | 205.7748 | 4290.25 | 281011.375 | 3369.5623 | 58.0461 |
| $\frac{9}{16}$ | 205.9711 | 4298.441 | 281816.564 | 3375.9959 | 58.1015 |
| $\frac{5}{8}$ | 206.1675 | 4306.640 | 282623.289 | 3382.4355 | 58.1569 |
| $\frac{11}{16}$ | 206.3638 | 4314.847 | 283431.551 | 3388.8813 | 58.2122 |
| $\frac{3}{4}$ | 206.5602 | 4323.062 | 284241.359 | 3395.3332 | 58.2676 |
| $\frac{13}{16}$ | 206.7565 | 4331.275 | 285037.242 | 3401.7913 | 58.3230 |
| $\frac{7}{8}$ | 206.9529 | 4339.515 | 285865.590 | 3408.2555 | 58.3784 |
| $\frac{15}{16}$ | 207.1492 | 4347.753 | 286879.943 | 3414.7259 | 58.4338 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|----------|----------|------------|-----------|-----------------|
| 66 in. | 207.3456 | 4356 | 287496 | 3421.2024 | 58.4892 |
| $\frac{1}{16}$ | 207.5419 | 4364.253 | 288313.523 | 3427.6850 | 58.5446 |
| $\frac{1}{8}$ | 207.7383 | 4372.515 | 289132.594 | 3434.1737 | 58.5990 |
| $\frac{3}{16}$ | 207.9346 | 4380.785 | 289953.213 | 3440.6676 | 58.6553 |
| $\frac{1}{4}$ | 208.1310 | 4389.062 | 290775.390 | 3447.1676 | 58.7108 |
| $\frac{5}{16}$ | 208.3273 | 4397.347 | 291592.211 | 3453.6758 | 58.7661 |
| $\frac{3}{8}$ | 208.5237 | 4405.640 | 292424.395 | 3460.1901 | 58.8215 |
| $\frac{7}{16}$ | 208.7200 | 4413.941 | 293251.231 | 3470.7096 | 58.8769 |
| $\frac{1}{2}$ | 208.9164 | 4422.25 | 294079.625 | 3473.2351 | 58.9323 |
| $\frac{9}{16}$ | 209.1127 | 4430.566 | 294899.576 | 3479.7669 | 58.9877 |
| $\frac{5}{8}$ | 209.3091 | 4438.890 | 295741.086 | 3486.3047 | 59.0431 |
| $\frac{11}{16}$ | 209.5054 | 4447.222 | 296574.157 | 3492.8487 | 59.0984 |
| $\frac{3}{4}$ | 209.7018 | 4455.562 | 297408.797 | 3499.3987 | 59.1539 |
| $\frac{13}{16}$ | 209.8981 | 4463.900 | 298244.325 | 3506.4550 | 59.2092 |
| $\frac{7}{8}$ | 210.0945 | 4472.265 | 299082.762 | 3512.5174 | 59.2646 |
| $\frac{15}{16}$ | 210.2908 | 4480.628 | 299922.097 | 3519.0860 | 59.3200 |
| 67 in. | 210.4872 | 4489 | 300763 | 3525.6606 | 59.3754 |
| $\frac{1}{16}$ | 210.6835 | 4497.378 | 301605.472 | 3532.2414 | 59.4308 |
| $\frac{1}{8}$ | 210.8799 | 4505.765 | 302449.516 | 3538.8283 | 59.4862 |
| $\frac{3}{16}$ | 211.0762 | 4514.160 | 303295.131 | 3545.4200 | 59.5415 |
| $\frac{1}{4}$ | 211.2726 | 4522.562 | 304142.328 | 3552.0185 | 59.5969 |
| $\frac{5}{16}$ | 211.4689 | 4530.972 | 304986.093 | 3558.6249 | 59.6523 |
| $\frac{3}{8}$ | 211.6653 | 4539.390 | 305841.442 | 3565.2374 | 59.7077 |
| $\frac{7}{16}$ | 211.8616 | 4547.816 | 306693.366 | 3571.8550 | 59.7631 |
| $\frac{1}{2}$ | 212.0580 | 4556.25 | 307546.875 | 3578.4787 | 59.8185 |
| $\frac{9}{16}$ | 212.2543 | 4564.691 | 308402.462 | 3585.1086 | 59.8739 |
| $\frac{5}{8}$ | 212.4507 | 4573.140 | 309258.633 | 3591.7446 | 59.9293 |
| $\frac{11}{16}$ | 212.6470 | 4581.597 | 310045.532 | 3598.8868 | 59.9847 |
| $\frac{3}{4}$ | 212.8434 | 4590.062 | 310976.734 | 3605.0350 | 60.0401 |
| $\frac{13}{16}$ | 213.0397 | 4598.535 | 311839.161 | 3611.6895 | 60.0954 |
| $\frac{7}{8}$ | 213.2361 | 4607.015 | 312701.184 | 3618.3500 | 60.1508 |
| $\frac{15}{16}$ | 213.4324 | 4615.503 | 313565.796 | 3625.0168 | 60.2062 |
| 68 in. | 213.6288 | 4624 | 314432 | 3631.6896 | 60.2616 |
| $\frac{1}{16}$ | 213.8251 | 4632.503 | 315299.796 | 3638.3686 | 60.3169 |
| $\frac{1}{8}$ | 214.0215 | 4641.015 | 316169.187 | 3645.0536 | 60.3723 |
| $\frac{3}{16}$ | 214.2178 | 4649.535 | 317040.174 | 3651.7439 | 60.4277 |
| $\frac{1}{4}$ | 214.4142 | 4658.062 | 317912.766 | 3658.4402 | 60.4831 |
| $\frac{5}{16}$ | 214.6105 | 4666.597 | 318786.948 | 3665.1448 | 60.5385 |
| $\frac{3}{8}$ | 214.8069 | 4675.140 | 319662.738 | 3671.8554 | 60.5939 |
| $\frac{7}{16}$ | 215.0032 | 4683.691 | 320780.130 | 3678.5762 | 60.6493 |
| $\frac{1}{2}$ | 215.1996 | 4692.25 | 321419.125 | 3685.2931 | 60.7047 |
| $\frac{9}{16}$ | 215.3959 | 4700.816 | 322459.724 | 3692.0212 | 60.7601 |
| $\frac{5}{8}$ | 215.5923 | 4709.390 | 323181.930 | 3698.7554 | 60.8155 |
| $\frac{11}{16}$ | 215.7886 | 4717.972 | 324065.743 | 3703.9957 | 60.8708 |
| $\frac{3}{4}$ | 215.9850 | 4726.562 | 324951.172 | 3712.2421 | 60.9262 |
| $\frac{13}{16}$ | 216.1813 | 4735.160 | 325837.204 | 3718.9948 | 60.9816 |
| $\frac{7}{8}$ | 216.3777 | 4743.765 | 326726.977 | 3725.7535 | 61.0371 |
| $\frac{15}{16}$ | 216.5748 | 4752.378 | 327617.120 | 3732.5184 | 61.0924 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|-----------------|----------|----------|------------|-----------|-------------------|
| 69 in. | 216.7704 | 4761 | 328509 | 3739.2894 | 61.1478 |
| $\frac{1}{16}$ | 216.9667 | 4769.628 | 329402.495 | 3745.8166 | 61.2032 |
| $\frac{1}{8}$ | 217.1631 | 4778.265 | 330297.609 | 3752.8498 | 61.2586 |
| $\frac{3}{16}$ | 217.3594 | 4786.910 | 331194.243 | 3759.6382 | 61.3139 |
| $\frac{1}{4}$ | 217.5558 | 4795.562 | 332092.703 | 3766.4327 | 61.3693 |
| $\frac{5}{16}$ | 217.7521 | 4804.222 | 332715.428 | 3773.2355 | 61.4247 |
| $\frac{3}{8}$ | 217.9485 | 4812.890 | 333894.285 | 3780.0443 | 61.4801 |
| $\frac{7}{16}$ | 218.1448 | 4821.566 | 334797.517 | 3786.8628 | 61.5355 |
| $\frac{1}{2}$ | 218.3412 | 4830.25 | 335702.375 | 3793.6703 | 61.5909 |
| $\frac{9}{16}$ | 218.5375 | 4838.941 | 336508.861 | 3800.5191 | 61.6463 |
| $\frac{5}{8}$ | 218.7339 | 4847.640 | 337516.977 | 3807.3369 | 61.7017 |
| $\frac{11}{16}$ | 218.9302 | 4856.347 | 338426.718 | 3814.2781 | 61.7571 |
| $\frac{3}{4}$ | 219.1266 | 4865.062 | 339338.109 | 3821.0200 | 61.8125 |
| $\frac{13}{16}$ | 219.3229 | 4873.785 | 340241.122 | 3827.8708 | 61.8678 |
| $\frac{7}{8}$ | 219.5193 | 4882.515 | 341165.773 | 3834.7277 | 61.9233 |
| $\frac{15}{16}$ | 219.7156 | 4891.253 | 341902.069 | 3841.5908 | 61.9786 |
| 70 in. | 219.9120 | 4900 | 343000 | 3848.4600 | 62.0341 |
| $\frac{1}{16}$ | 220.1083 | 4908.753 | 343919.570 | 3855.8353 | 62.0893 |
| $\frac{1}{8}$ | 220.3047 | 4917.515 | 344840.781 | 3862.2167 | 62.1448 |
| $\frac{3}{16}$ | 220.5010 | 4926.285 | 345759.635 | 3869.1033 | 62.2001 |
| $\frac{1}{4}$ | 220.6974 | 4935.062 | 346688.141 | 3875.9960 | 62.2555 |
| $\frac{5}{16}$ | 220.8937 | 4943.847 | 347514.284 | 3882.8969 | 62.3109 |
| $\frac{3}{8}$ | 221.0901 | 4952.640 | 348542.082 | 3889.8039 | 62.3663 |
| $\frac{7}{16}$ | 221.2864 | 4961.441 | 349471.528 | 3896.7211 | 62.4217 |
| $\frac{1}{2}$ | 221.4828 | 4970.25 | 350402.625 | 3903.6343 | 62.4771 |
| $\frac{9}{16}$ | 221.6791 | 4979.066 | 351335.372 | 3910.5538 | 62.5325 |
| $\frac{5}{8}$ | 221.8755 | 4987.890 | 352259.774 | 3917.4693 | 62.5879 |
| $\frac{11}{16}$ | 222.0718 | 4996.723 | 353205.828 | 3924.4260 | 62.6432 |
| $\frac{3}{4}$ | 222.2682 | 5005.562 | 354143.547 | 3931.3687 | 62.6986 |
| $\frac{13}{16}$ | 222.4645 | 5014.410 | 355182.915 | 3938.3177 | 62.7541 |
| $\frac{7}{8}$ | 222.6609 | 5023.265 | 356023.949 | 3945.2728 | 62.8094 |
| $\frac{15}{16}$ | 222.8572 | 5032.128 | 356966.643 | 3952.2341 | 62.8648 |
| 71 in. | 223.0536 | 5041 | 357911 | 3959.2014 | 62.9202 |
| $\frac{1}{16}$ | 223.2499 | 5049.878 | 358857.019 | 3966.1749 | 62.9756 |
| $\frac{1}{8}$ | 223.4463 | 5058.765 | 359804.703 | 3973.1545 | 63.0301 |
| $\frac{3}{16}$ | 223.6426 | 5067.660 | 360754.053 | 3980.1393 | 63.0863 |
| $\frac{1}{4}$ | 223.8390 | 5076.562 | 361705.078 | 3987.1301 | 63.1417 |
| $\frac{5}{16}$ | 224.0353 | 5085.472 | 362657.764 | 3994.1292 | 63.1971 |
| $\frac{3}{8}$ | 224.2317 | 5094.390 | 363612.129 | 4001.1344 | 63.2525 |
| $\frac{7}{16}$ | 224.4380 | 5103.316 | 364568.165 | 4008.1447 | 63.3079 |
| $\frac{1}{2}$ | 224.6244 | 5112.25 | 365525.875 | 4015.1611 | 63.3623 |
| $\frac{9}{16}$ | 224.8207 | 5121.191 | 366485.259 | 4022.1837 | 63.4187 |
| $\frac{5}{8}$ | 225.0171 | 5130.140 | 367446.320 | 4029.2124 | 63.4741 |
| $\frac{11}{16}$ | 225.2134 | 5139.097 | 368409.059 | 4036.2473 | 63.5295 |
| $\frac{3}{4}$ | 225.4098 | 5148.062 | 369373.484 | 4043.2882 | 63.5849 |
| $\frac{13}{16}$ | 225.6061 | 5157.035 | 370339.583 | 4050.3334 | 63.6402 |
| $\frac{7}{8}$ | 225.8025 | 5166.015 | 371307.371 | 4057.3886 | 63.6956 |
| $\frac{15}{16}$ | 225.9988 | 5175.003 | 372276.843 | 4064.4481 | 63.7511 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|----------|----------|------------|-----------|-----------------|
| 73 in. | 226.1952 | 5184 | 373248 | 4071.5136 | 63.8064 |
| $\frac{1}{16}$ | 226.3915 | 5193.008 | 374220.843 | 4078.5853 | 63.8617 |
| $\frac{1}{8}$ | 226.5879 | 5202.015 | 375195.375 | 4085.6631 | 63.9171 |
| $\frac{3}{16}$ | 226.7842 | 5211.035 | 376161.596 | 4092.7460 | 63.9725 |
| $\frac{1}{4}$ | 226.9806 | 5220.062 | 377149.515 | 4099.8350 | 64.0279 |
| $\frac{5}{16}$ | 227.1769 | 5229.097 | 378129.140 | 4106.9323 | 64.0833 |
| $\frac{3}{8}$ | 227.3733 | 5238.140 | 379110.425 | 4114.0356 | 64.1367 |
| $\frac{7}{16}$ | 227.5696 | 5247.191 | 380093.427 | 4121.1442 | 64.1941 |
| $\frac{1}{2}$ | 227.7660 | 5256.25 | 381078.125 | 4128.2587 | 64.2495 |
| $\frac{9}{16}$ | 227.9623 | 5265.316 | 382063.521 | 4135.3795 | 64.3049 |
| $\frac{5}{8}$ | 228.1587 | 5274.890 | 383052.617 | 4142.5064 | 64.3603 |
| $\frac{11}{16}$ | 228.3550 | 5283.472 | 384192.414 | 4149.6394 | 64.4157 |
| $\frac{3}{4}$ | 228.5514 | 5292.562 | 385033.921 | 4156.7785 | 64.4711 |
| $\frac{13}{16}$ | 228.7477 | 5301.650 | 386026.397 | 4163.9239 | 64.5264 |
| $\frac{7}{8}$ | 228.9441 | 5310.765 | 387022.043 | 4171.0753 | 64.5818 |
| $\frac{15}{16}$ | 229.1404 | 5319.878 | 388747.938 | 4178.2829 | 64.6372 |
| 73 in. | 229.3368 | 5329 | 389017 | 4185.3966 | 64.6926 |
| $\frac{1}{16}$ | 229.5331 | 5338.128 | 390017.042 | 4192.5665 | 64.7470 |
| $\frac{1}{8}$ | 229.7295 | 5347.265 | 391018.797 | 4199.7424 | 64.8034 |
| $\frac{3}{16}$ | 229.9258 | 5356.410 | 392013.264 | 4206.9230 | 64.8587 |
| $\frac{1}{4}$ | 230.1222 | 5365.562 | 393027.453 | 4214.1107 | 64.9141 |
| $\frac{5}{16}$ | 230.3185 | 5374.722 | 394034.350 | 4221.3027 | 64.9695 |
| $\frac{3}{8}$ | 230.5149 | 5383.890 | 395042.972 | 4228.5077 | 65.0249 |
| $\frac{7}{16}$ | 230.7112 | 5393.066 | 396058.313 | 4235.7109 | 65.0803 |
| $\frac{1}{2}$ | 230.9076 | 5402.25 | 397065.375 | 4242.9271 | 65.1357 |
| $\frac{9}{16}$ | 231.1039 | 5411.441 | 398079.157 | 4250.1461 | 65.1911 |
| $\frac{5}{8}$ | 231.3003 | 5420.640 | 399094.664 | 4257.3711 | 65.2465 |
| $\frac{11}{16}$ | 231.4966 | 5429.847 | 400111.865 | 4264.6023 | 65.3018 |
| $\frac{3}{4}$ | 231.6930 | 5439.062 | 401130.859 | 4271.8396 | 65.3572 |
| $\frac{13}{16}$ | 231.8893 | 5448.275 | 402150.805 | 4279.0831 | 65.4126 |
| $\frac{7}{8}$ | 232.0857 | 5457.515 | 403173.964 | 4286.3327 | 65.4650 |
| $\frac{15}{16}$ | 232.2820 | 5466.753 | 404198.116 | 4293.5886 | 65.5234 |
| 74 in. | 232.4784 | 5476 | 405224 | 4300.8504 | 65.5788 |
| $\frac{1}{16}$ | 232.6747 | 5485.253 | 406251.616 | 4308.1185 | 65.6341 |
| $\frac{1}{8}$ | 232.8711 | 5494.515 | 407280.968 | 4315.3926 | 65.6895 |
| $\frac{3}{16}$ | 233.0674 | 5503.785 | 408312.057 | 4322.1719 | 65.7449 |
| $\frac{1}{4}$ | 233.2638 | 5513.062 | 409344.890 | 4329.9572 | 65.8003 |
| $\frac{5}{16}$ | 233.4601 | 5522.347 | 410379.456 | 4337.2508 | 65.8557 |
| $\frac{3}{8}$ | 233.6565 | 5531.640 | 411415.769 | 4344.5505 | 65.9111 |
| $\frac{7}{16}$ | 233.8528 | 5540.941 | 412453.775 | 4351.8551 | 65.9665 |
| $\frac{1}{2}$ | 234.0492 | 5550.25 | 413493.625 | 4359.1663 | 66.0219 |
| $\frac{9}{16}$ | 234.2455 | 5559.566 | 414535.169 | 4366.4835 | 66.0773 |
| $\frac{5}{8}$ | 234.4419 | 5568.890 | 415578.461 | 4373.8067 | 66.1327 |
| $\frac{11}{16}$ | 234.6382 | 5578.222 | 416613.500 | 4381.1361 | 66.1880 |
| $\frac{3}{4}$ | 234.8346 | 5587.562 | 417670.296 | 4388.4715 | 66.2434 |
| $\frac{13}{16}$ | 235.0309 | 5596.900 | 418719.087 | 4396.8132 | 66.2988 |
| $\frac{7}{8}$ | 235.2273 | 5606.265 | 419769.136 | 4403.1610 | 66.3542 |
| $\frac{15}{16}$ | 235.4236 | 5615.628 | 420821.190 | 4410.5150 | 66.4096 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|----------|----------|------------|-----------|-----------------|
| 75 in. | 235.6200 | 5625 | 421875 | 4417.8750 | 66.4650 |
| $\frac{1}{16}$ | 235.8163 | 5634.378 | 422930.566 | 4425.2412 | 66.5204 |
| $\frac{1}{8}$ | 236.0127 | 5643.765 | 423987.890 | 4432.6135 | 66.5758 |
| $\frac{3}{16}$ | 236.2090 | 5653.160 | 424046.975 | 4439.9910 | 66.6311 |
| $\frac{1}{4}$ | 236.4054 | 5662.562 | 426107.828 | 4447.3745 | 66.6865 |
| $\frac{5}{16}$ | 236.6017 | 5671.972 | 427170.436 | 4454.7663 | 66.7419 |
| $\frac{3}{8}$ | 236.7981 | 5681.390 | 428234.816 | 4462.1642 | 66.7973 |
| $\frac{7}{16}$ | 236.9944 | 5690.816 | 429300.952 | 4469.5672 | 66.8527 |
| $\frac{1}{2}$ | 237.1908 | 5700.25 | 430368.875 | 4476.9763 | 66.9081 |
| $\frac{9}{16}$ | 237.3871 | 5709.691 | 431438.541 | 4484.3916 | 66.9635 |
| $\frac{5}{8}$ | 237.5835 | 5719.140 | 432510.007 | 4491.8130 | 67.0189 |
| $\frac{11}{16}$ | 237.7798 | 5728.597 | 433583.230 | 4499.2406 | 67.0743 |
| $\frac{3}{4}$ | 237.9762 | 5738.062 | 434658.234 | 4506.6742 | 67.1297 |
| $\frac{13}{16}$ | 238.1725 | 5747.525 | 435734.246 | 4514.1141 | 67.1850 |
| $\frac{7}{8}$ | 238.3689 | 5757.015 | 436813.558 | 4521.5600 | 67.2404 |
| $\frac{15}{16}$ | 238.5652 | 5766.503 | 436893.869 | 4528.9622 | 67.2958 |
| 76 in. | 238.7616 | 5776 | 438976 | 4536.4704 | 67.3512 |
| $\frac{1}{16}$ | 238.9579 | 5785.503 | 440059.990 | 4543.9333 | 67.4066 |
| $\frac{1}{8}$ | 239.1543 | 5795.015 | 441145.564 | 4551.4023 | 67.4610 |
| $\frac{3}{16}$ | 239.3506 | 5804.535 | 442233.017 | 4558.8794 | 67.5173 |
| $\frac{1}{4}$ | 239.5470 | 5814.062 | 443322.265 | 4566.3626 | 67.5727 |
| $\frac{5}{16}$ | 239.7433 | 5823.597 | 444413.291 | 4573.8526 | 67.6281 |
| $\frac{3}{8}$ | 239.9397 | 5833.140 | 445506.113 | 4581.3486 | 67.6835 |
| $\frac{7}{16}$ | 240.1360 | 5842.691 | 446600.724 | 4588.8493 | 67.7389 |
| $\frac{1}{2}$ | 240.3324 | 5852.25 | 447697.125 | 4596.3571 | 67.7943 |
| $\frac{9}{16}$ | 240.5287 | 5861.816 | 448795.318 | 4603.8706 | 67.8497 |
| $\frac{5}{8}$ | 240.7251 | 5871.390 | 449895.304 | 4611.3902 | 67.9051 |
| $\frac{11}{16}$ | 240.9214 | 5880.972 | 450997.086 | 4618.9159 | 67.9605 |
| $\frac{3}{4}$ | 241.1178 | 5890.562 | 452100.671 | 4626.4477 | 68.0159 |
| $\frac{13}{16}$ | 241.3141 | 5900.150 | 453205.279 | 4633.9858 | 68.0712 |
| $\frac{7}{8}$ | 241.5105 | 5909.765 | 454313.230 | 4641.5299 | 68.1266 |
| $\frac{15}{16}$ | 241.7068 | 5919.378 | 455422.214 | 4649.0802 | 68.1821 |
| 77 in. | 241.9032 | 5929 | 456533 | 4656.6366 | 68.2374 |
| $\frac{1}{16}$ | 242.0995 | 5938.628 | 457645.589 | 4664.1992 | 68.2928 |
| $\frac{1}{8}$ | 242.2959 | 5948.265 | 458759.984 | 4671.7678 | 68.3482 |
| $\frac{3}{16}$ | 242.4922 | 5957.910 | 459820.610 | 4679.3416 | 68.4035 |
| $\frac{1}{4}$ | 242.6886 | 5967.562 | 460994.203 | 4686.9215 | 68.4589 |
| $\frac{5}{16}$ | 242.8849 | 5977.222 | 462114.022 | 4694.5097 | 68.5143 |
| $\frac{3}{8}$ | 243.0813 | 5986.890 | 463235.660 | 4702.1039 | 68.5697 |
| $\frac{7}{16}$ | 243.2776 | 5996.566 | 464359.110 | 4709.7033 | 68.6251 |
| $\frac{1}{2}$ | 243.4740 | 6006.25 | 465484.375 | 4717.3087 | 68.6805 |
| $\frac{9}{16}$ | 243.6703 | 6015.941 | 466611.474 | 4724.9204 | 68.7359 |
| $\frac{5}{8}$ | 243.8667 | 6025.640 | 467740.351 | 4732.5381 | 68.7913 |
| $\frac{11}{16}$ | 244.0630 | 6035.347 | 468871.166 | 4740.1620 | 68.8467 |
| $\frac{3}{4}$ | 244.2594 | 6045.062 | 470003.609 | 4747.7920 | 68.9021 |
| $\frac{13}{16}$ | 244.4557 | 6054.775 | 471127.187 | 4755.8782 | 68.9574 |
| $\frac{7}{8}$ | 244.6521 | 6064.515 | 472274.152 | 4763.0705 | 69.0128 |
| $\frac{15}{16}$ | 244.8484 | 6074.253 | 473413.963 | 4771.1690 | 69.0682 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|----------|----------|------------|-----------|-----------------|
| 78 in. | 245.0448 | 6084 | 474552 | 4778.3736 | 69.1236 |
| $\frac{1}{16}$ | 245.2411 | 6093.753 | 475693.663 | 4786.0344 | 69.1790 |
| $\frac{1}{8}$ | 245.4375 | 6103.515 | 476837.156 | 4793.7012 | 69.2343 |
| $\frac{3}{16}$ | 245.6338 | 6113.285 | 477982.478 | 4801.3732 | 69.2897 |
| $\frac{1}{4}$ | 245.8302 | 6123.062 | 479129.640 | 4809.0512 | 69.3451 |
| $\frac{5}{16}$ | 246.0265 | 6132.847 | 480277.627 | 4817.1375 | 69.4006 |
| $\frac{3}{8}$ | 246.2229 | 6142.640 | 481429.457 | 4824.4299 | 69.4559 |
| $\frac{7}{16}$ | 246.4192 | 6152.441 | 482582.114 | 4832.1275 | 69.5113 |
| $\frac{1}{2}$ | 246.6156 | 6162.25 | 483736.625 | 4839.8311 | 69.5667 |
| $\frac{9}{16}$ | 246.8119 | 6172.066 | 484752.966 | 4847.5409 | 69.6221 |
| $\frac{5}{8}$ | 247.0083 | 6181.890 | 486051.148 | 4855.2568 | 69.6775 |
| $\frac{11}{16}$ | 247.2046 | 6191.722 | 487211.272 | 4862.9789 | 69.7329 |
| $\frac{3}{4}$ | 247.4010 | 6201.562 | 488373.047 | 4870.7071 | 69.7883 |
| $\frac{13}{16}$ | 247.5973 | 6211.400 | 489736.071 | 4878.4415 | 69.8437 |
| $\frac{7}{8}$ | 247.7937 | 6221.265 | 490702.324 | 4886.1820 | 69.8991 |
| $\frac{15}{16}$ | 247.9900 | 6231.128 | 491769.737 | 4893.9287 | 69.9544 |
| 79 in. | 248.1864 | 6241 | 493039. | 4901.6814 | 70.0098 |
| $\frac{1}{16}$ | 248.3827 | 6250.878 | 494210.113 | 4909.4403 | 70.0652 |
| $\frac{1}{8}$ | 248.5791 | 6260.765 | 495383.078 | 4917.2053 | 70.1206 |
| $\frac{3}{16}$ | 248.7754 | 6270.660 | 496557.896 | 4924.9755 | 70.1760 |
| $\frac{1}{4}$ | 248.9718 | 6280.562 | 497734.578 | 4932.7517 | 70.2314 |
| $\frac{5}{16}$ | 249.1681 | 6290.472 | 498913.108 | 4940.5362 | 70.2867 |
| $\frac{3}{8}$ | 249.3645 | 6300.390 | 500093.504 | 4948.3268 | 70.3421 |
| $\frac{7}{16}$ | 249.5608 | 6310.316 | 501275.757 | 4956.1225 | 70.3975 |
| $\frac{1}{2}$ | 249.7572 | 6320.25 | 502459.875 | 4963.9243 | 70.4529 |
| $\frac{9}{16}$ | 249.9535 | 6330.191 | 503645.853 | 4971.7319 | 70.5083 |
| $\frac{5}{8}$ | 250.1499 | 6340.140 | 504833.695 | 4979.5456 | 70.5637 |
| $\frac{11}{16}$ | 250.3462 | 6350.097 | 506023.401 | 4987.3663 | 70.6191 |
| $\frac{3}{4}$ | 250.5426 | 6360.062 | 507214.992 | 4995.1930 | 70.6745 |
| $\frac{13}{16}$ | 250.7389 | 6370.025 | 508407.621 | 5003.0316 | 70.7298 |
| $\frac{7}{8}$ | 250.9353 | 6380.015 | 509603.746 | 5010.8642 | 70.7853 |
| $\frac{15}{16}$ | 251.1316 | 6390.003 | 510800.936 | 5018.7091 | 70.8406 |
| 80 in. | 251.3280 | 6400 | 512000 | 5026.5600 | 70.8960 |
| $\frac{1}{16}$ | 251.5243 | 6410.003 | 513200.937 | 5034.4171 | 70.9513 |
| $\frac{1}{8}$ | 251.7207 | 6420.015 | 514403.750 | 5042.2803 | 71.0068 |
| $\frac{3}{16}$ | 251.9170 | 6430.035 | 515608.439 | 5050.1486 | 71.0622 |
| $\frac{1}{4}$ | 252.1134 | 6440.062 | 516815.016 | 5058.0230 | 71.1176 |
| $\frac{5}{16}$ | 252.3097 | 6450.097 | 518033.463 | 5065.9027 | 71.1729 |
| $\frac{3}{8}$ | 252.5061 | 6460.140 | 519233.801 | 5073.7944 | 71.2283 |
| $\frac{7}{16}$ | 252.7024 | 6470.191 | 520446.020 | 5081.6883 | 71.2837 |
| $\frac{1}{2}$ | 252.8988 | 6480.25 | 521660.125 | 5089.5883 | 71.3391 |
| $\frac{9}{16}$ | 253.0951 | 6490.316 | 522876.114 | 5097.4941 | 71.3945 |
| $\frac{5}{8}$ | 253.2915 | 6500.390 | 524093.992 | 5105.4060 | 71.4499 |
| $\frac{11}{16}$ | 253.4878 | 6510.472 | 525313.758 | 5113.8248 | 71.5053 |
| $\frac{3}{4}$ | 253.6842 | 6520.562 | 526535.422 | 5121.2497 | 71.5607 |
| $\frac{13}{16}$ | 253.8805 | 6530.660 | 527758.969 | 5129.1855 | 71.6161 |
| $\frac{7}{8}$ | 254.0769 | 6540.765 | 528984.418 | 5137.1173 | 71.6715 |
| $\frac{15}{16}$ | 254.2732 | 6550.878 | 530210.761 | 5145.0603 | 71.7268 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|----------|----------|------------|-----------|-----------------|
| 81 in. | 254.4696 | 6561 | 531441 | 5153.0094 | 71.7822 |
| $\frac{1}{16}$ | 254.6659 | 6571.128 | 532672.136 | 5160.9647 | 71.8376 |
| $\frac{1}{8}$ | 254.8623 | 6581.265 | 533903.172 | 5168.9260 | 71.8930 |
| $\frac{3}{16}$ | 255.0586 | 6591.410 | 535140.107 | 5176.8925 | 71.9484 |
| $\frac{1}{4}$ | 255.2550 | 6601.562 | 536376.953 | 5184.8651 | 72.0037 |
| $\frac{5}{16}$ | 255.4518 | 6611.722 | 537615.694 | 5192.8460 | 72.0591 |
| $\frac{3}{8}$ | 255.6477 | 6621.890 | 538856.347 | 5200.8329 | 72.1145 |
| $\frac{7}{16}$ | 255.8440 | 6632.066 | 540098.907 | 5208.8250 | 72.1699 |
| $\frac{1}{2}$ | 256.0404 | 6642.25 | 541343.375 | 5216.8231 | 72.2253 |
| $\frac{9}{16}$ | 256.2367 | 6652.441 | 542589.751 | 5224.8271 | 72.2807 |
| $\frac{5}{8}$ | 256.4331 | 6662.640 | 543838.039 | 5232.8371 | 72.3361 |
| $\frac{11}{16}$ | 256.6294 | 6672.847 | 545088.238 | 5240.8568 | 72.3915 |
| $\frac{3}{4}$ | 256.8258 | 6683.062 | 546340.359 | 5248.8772 | 72.4469 |
| $\frac{13}{16}$ | 257.0221 | 6693.285 | 547594.387 | 5256.9061 | 72.5023 |
| $\frac{7}{8}$ | 257.2105 | 6703.515 | 548850.339 | 5264.9411 | 72.5577 |
| $\frac{15}{16}$ | 257.4148 | 6713.753 | 550108.211 | 5272.9828 | 72.6130 |
| 82 in. | 257.6112 | 6724 | 551368 | 5281.0296 | 72.6684 |
| $\frac{1}{16}$ | 257.8075 | 6734.253 | 552629.710 | 5289.0781 | 72.7237 |
| $\frac{1}{8}$ | 258.0039 | 6744.515 | 553863.343 | 5297.1426 | 72.7792 |
| $\frac{3}{16}$ | 258.2002 | 6754.785 | 555158.900 | 5305.2073 | 72.8346 |
| $\frac{1}{4}$ | 258.3966 | 6765.062 | 556426.390 | 5313.2780 | 72.8901 |
| $\frac{5}{16}$ | 258.5929 | 6775.347 | 557695.799 | 5321.3570 | 72.9453 |
| $\frac{3}{8}$ | 258.7893 | 6785.640 | 558967.144 | 5329.4421 | 73.0007 |
| $\frac{7}{16}$ | 258.9856 | 6795.941 | 559140.118 | 5337.5324 | 73.0561 |
| $\frac{1}{2}$ | 259.1820 | 6806.25 | 561515.625 | 5345.6287 | 73.1115 |
| $\frac{9}{16}$ | 259.3783 | 6816.566 | 563292.769 | 5353.7809 | 73.1669 |
| $\frac{5}{8}$ | 259.5747 | 6826.890 | 564071.836 | 5361.8391 | 73.2224 |
| $\frac{11}{16}$ | 259.7710 | 6837.222 | 565352.844 | 5369.9543 | 73.2777 |
| $\frac{3}{4}$ | 259.9674 | 6847.562 | 566635.797 | 5378.0755 | 73.3330 |
| $\frac{13}{16}$ | 260.1637 | 6857.910 | 567900.480 | 5386.2026 | 73.3885 |
| $\frac{7}{8}$ | 260.3601 | 6868.265 | 569207.511 | 5394.3358 | 73.4438 |
| $\frac{15}{16}$ | 260.5564 | 6878.628 | 570496.284 | 5402.4552 | 73.4993 |
| 83 in. | 260.7528 | 6889 | 571787 | 5410.6206 | 73.5546 |
| $\frac{1}{16}$ | 260.9491 | 6899.378 | 573079.659 | 5418.7722 | 73.6101 |
| $\frac{1}{8}$ | 261.1455 | 6909.765 | 574374.265 | 5426.9299 | 73.6653 |
| $\frac{3}{16}$ | 261.3418 | 6920.160 | 575670.818 | 5435.0928 | 73.7208 |
| $\frac{1}{4}$ | 261.5382 | 6930.562 | 576969.328 | 5443.2617 | 73.7761 |
| $\frac{5}{16}$ | 261.7345 | 6940.972 | 578269.769 | 5451.4389 | 73.8315 |
| $\frac{3}{8}$ | 261.9309 | 6951.390 | 579572.191 | 5459.6222 | 73.8869 |
| $\frac{7}{16}$ | 262.1272 | 6961.816 | 580876.556 | 5467.8106 | 73.9423 |
| $\frac{1}{2}$ | 262.3236 | 6972.25 | 582182.875 | 5476.0051 | 73.9977 |
| $\frac{9}{16}$ | 262.5199 | 6982.691 | 583491.150 | 5484.2054 | 74.0531 |
| $\frac{5}{8}$ | 262.7163 | 6993.140 | 584801.362 | 5492.4118 | 74.1085 |
| $\frac{11}{16}$ | 262.9126 | 7003.597 | 586113.574 | 5500.6252 | 74.1639 |
| $\frac{3}{4}$ | 263.1090 | 7014.062 | 587427.734 | 5508.8446 | 74.2193 |
| $\frac{13}{16}$ | 263.3053 | 7024.535 | 589067.048 | 5517.0699 | 74.2747 |
| $\frac{7}{8}$ | 263.5017 | 7035.015 | 590061.933 | 5525.3012 | 74.3301 |
| $\frac{15}{16}$ | 263.6980 | 7045.503 | 591381.983 | 5533.5388 | 74.3854 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|----------|----------|------------|-----------|-----------------|
| 84 in. | 263.8944 | 7056 | 592704 | 5541.7824 | 74.4408 |
| $\frac{1}{16}$ | 264.0907 | 7065.503 | 593943.922 | 5550.0322 | 74.4962 |
| $\frac{1}{8}$ | 264.2871 | 7077.015 | 595353.937 | 5558.2081 | 74.5516 |
| $\frac{3}{16}$ | 264.4834 | 7087.535 | 596794.862 | 5566.5491 | 74.6070 |
| $\frac{1}{4}$ | 264.6798 | 7098.062 | 598011.765 | 5574.8162 | 74.6624 |
| $\frac{5}{16}$ | 264.8761 | 7108.597 | 599343.635 | 5583.0916 | 74.7177 |
| $\frac{3}{8}$ | 265.0725 | 7119.140 | 600677.488 | 5591.3730 | 74.7731 |
| $\frac{7}{16}$ | 265.2688 | 7129.691 | 602012.317 | 5599.6596 | 74.8385 |
| $\frac{1}{2}$ | 265.4652 | 7140.25 | 603351.125 | 5607.9523 | 74.8899 |
| $\frac{9}{16}$ | 265.6615 | 7150.816 | 604690.912 | 5616.2508 | 74.9393 |
| $\frac{5}{8}$ | 265.8579 | 7161.390 | 606032.679 | 5624.5554 | 74.9947 |
| $\frac{11}{16}$ | 266.0542 | 7171.972 | 607376.429 | 5632.8662 | 75.0601 |
| $\frac{3}{4}$ | 266.2506 | 7182.562 | 608722.172 | 5641.1845 | 75.1055 |
| $\frac{13}{16}$ | 266.4469 | 7193.160 | 609969.891 | 5649.5071 | 75.1608 |
| $\frac{7}{8}$ | 266.6433 | 7203.765 | 611419.605 | 5657.8357 | 75.2162 |
| $\frac{15}{16}$ | 266.8396 | 7214.378 | 612771.408 | 5666.1723 | 75.2716 |
| 85 in. | 267.0360 | 7225 | 614125 | 5674.5150 | 75.3269 |
| $\frac{1}{16}$ | 267.2323 | 7235.628 | 615480.693 | 5682.8630 | 75.3824 |
| $\frac{1}{8}$ | 267.4287 | 7246.265 | 616838.359 | 5691.2170 | 75.4378 |
| $\frac{3}{16}$ | 267.6250 | 7256.910 | 618198.029 | 5699.5762 | 75.4931 |
| $\frac{1}{4}$ | 267.8214 | 7267.562 | 619559.703 | 5707.9415 | 75.5486 |
| $\frac{5}{16}$ | 268.0177 | 7278.222 | 620923.365 | 5716.3151 | 75.6039 |
| $\frac{3}{8}$ | 268.2141 | 7288.890 | 622289.035 | 5724.6947 | 75.6593 |
| $\frac{7}{16}$ | 268.4104 | 7299.566 | 623656.713 | 5733.0795 | 75.7147 |
| $\frac{1}{2}$ | 268.6068 | 7310.25 | 625026.375 | 5741.4703 | 75.7701 |
| $\frac{9}{16}$ | 268.8031 | 7320.941 | 626398.048 | 5749.8670 | 75.8255 |
| $\frac{5}{8}$ | 268.9997 | 7331.640 | 627771.726 | 5758.2697 | 75.8809 |
| $\frac{11}{16}$ | 269.1958 | 7342.347 | 629147.409 | 5766.6794 | 75.9363 |
| $\frac{3}{4}$ | 269.3922 | 7353.062 | 630525.109 | 5775.0952 | 75.9917 |
| $\frac{13}{16}$ | 269.5885 | 7363.785 | 631904.808 | 5783.5168 | 76.0471 |
| $\frac{7}{8}$ | 269.7849 | 7374.515 | 633286.527 | 5791.9445 | 76.1025 |
| $\frac{15}{16}$ | 269.9812 | 7385.253 | 634670.257 | 5800.3784 | 76.1578 |
| 86 in. | 270.1776 | 7396 | 636056 | 5808.8184 | 76.2132 |
| $\frac{1}{16}$ | 270.3739 | 7406.753 | 637443.757 | 5817.2651 | 76.2686 |
| $\frac{1}{8}$ | 270.5703 | 7417.515 | 638833.531 | 5825.7168 | 76.3240 |
| $\frac{3}{16}$ | 270.7666 | 7428.285 | 640325.320 | 5834.1742 | 76.3794 |
| $\frac{1}{4}$ | 270.9630 | 7439.062 | 641619.140 | 5842.6376 | 76.4347 |
| $\frac{5}{16}$ | 271.1593 | 7449.847 | 643014.971 | 5851.1093 | 76.4901 |
| $\frac{3}{8}$ | 271.3557 | 7460.640 | 644412.832 | 5859.5871 | 76.5455 |
| $\frac{7}{16}$ | 271.5520 | 7471.441 | 645812.722 | 5868.0701 | 76.6009 |
| $\frac{1}{2}$ | 271.7484 | 7482.25 | 647214.625 | 5876.5591 | 76.6563 |
| $\frac{9}{16}$ | 271.9447 | 7493.066 | 648078.560 | 5885.0540 | 76.7117 |
| $\frac{5}{8}$ | 272.1411 | 7503.890 | 650024.523 | 5893.5549 | 76.7671 |
| $\frac{11}{16}$ | 272.3374 | 7514.722 | 651432.515 | 5902.0620 | 76.8225 |
| $\frac{3}{4}$ | 272.5338 | 7525.562 | 652842.547 | 5910.5767 | 76.8779 |
| $\frac{13}{16}$ | 272.7301 | 7536.410 | 654254.601 | 5919.0965 | 76.9333 |
| $\frac{7}{8}$ | 272.9265 | 7547.265 | 655668.699 | 5927.6224 | 76.9887 |
| $\frac{15}{16}$ | 273.1228 | 7558.128 | 656984.831 | 5936.1545 | 77.0441 |

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| Dec. or cent. | Column. | Spans | the | same | le of square. |
|------------------|----------|-------|-----|------|------------------|
| 34 | 253.2944 | 714 | | | 7580 |
| | 254.0907 | 712.5 | | | 8134 |
| | 254.2871 | | | | 8688 |
| | 254.483 | | | | 9242 |
| | 254.679 | | | | 9796 |
| | 254.875 | | | | 0.0349 |
| | 255.071 | | | | 0.0903 |
| | 255.267 | | | | 0.1457 |
| | 255.463 | | | | 0.2011 |
| | 255.659 | | | | 0.2565 |
| | 255.855 | | | | 0.3119 |
| | 256.051 | | | | 0.3673 |
| | 256.247 | | | | 0.4227 |
| | 256.443 | | | | 0.4781 |
| | 256.639 | | | | 0.5335 |
| | 256.835 | | | | 0.5888 |
| 35 | 257.031 | | | | 0.6442 |
| | 257.227 | | | | 0.6996 |
| | 257.423 | | | | 0.7550 |
| | 257.619 | | | | 0.8104 |
| | 257.815 | | | | 0.8658 |
| | 258.011 | | | | 0.9211 |
| | 258.207 | | | | 0.9765 |
| | 258.403 | | | | 1.0319 |
| | 258.599 | | | | 1.0873 |
| | 258.795 | | | | 1.1427 |
| | 258.991 | | | | 1.1981 |
| | 259.187 | | | | 1.2535 |
| | 259.383 | | | | 1.3089 |
| | 259.579 | | | | 1.3643 |
| | 259.775 | | | | 1.4197 |
| | 259.971 | | | | 1.4750 |
| | 260.167 | | | | 1.5304 |
| | 260.363 | | | | 1.5858 |
| | 260.559 | | | | 1.6412 |
| | 260.755 | | | | 1.6966 |
| | 260.951 | | | | 1.7519 |
| | 261.147 | | | | 1.8073 |
| | 261.343 | | | | 1.8627 |
| | 261.539 | | | | 1.9181 |
| | 261.735 | | | | 1.9735 |
| | 261.931 | | | | 2.0289 |
| | 262.127 | | | | 2.0843 |
| | 262.323 | | | | 2.1397 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of square. |
|-----------------|----------|----------|------------|-----------|-----------------|
| 87 in. | 273.3192 | 7569 | 658503 | 5944.6926 | 77.0994 |
| $\frac{1}{16}$ | 273.5155 | 7579.878 | 659913.206 | 5953.2369 | 77.1548 |
| $\frac{1}{8}$ | 273.7119 | 7590.765 | 661345.453 | 5961.7873 | 77.2102 |
| $\frac{3}{16}$ | 273.9082 | 7601.660 | 662769.740 | 5970.3429 | 77.2655 |
| $\frac{1}{4}$ | 274.1046 | 7612.562 | 664196.078 | 5978.9045 | 77.3210 |
| $\frac{5}{16}$ | 274.3009 | 7623.472 | 665618.451 | 5987.4749 | 77.3763 |
| $\frac{3}{8}$ | 274.4973 | 7634.390 | 667054.878 | 5996.0504 | 77.4317 |
| $\frac{7}{16}$ | 274.6936 | 7645.316 | 668487.353 | 6004.6315 | 77.4871 |
| $\frac{1}{2}$ | 274.8900 | 7656.25 | 669921.875 | 6013.2187 | 77.5425 |
| $\frac{9}{16}$ | 275.0863 | 7667.191 | 671368.487 | 6021.8117 | 77.5979 |
| $\frac{5}{8}$ | 275.2827 | 7678.140 | 672797.070 | 6030.4108 | 77.6533 |
| $\frac{11}{16}$ | 275.4790 | 7689.097 | 674237.746 | 6039.0169 | 77.7086 |
| $\frac{3}{4}$ | 275.6754 | 7700.062 | 675680.484 | 6047.6290 | 77.7640 |
| $\frac{13}{16}$ | 275.8717 | 7711.035 | 677125.269 | 6056.2470 | 77.8194 |
| $\frac{7}{8}$ | 276.0681 | 7722.015 | 678572.121 | 6064.8710 | 77.8748 |
| $\frac{15}{16}$ | 276.2644 | 7733.003 | 680021.030 | 6073.5013 | 77.9302 |
| 88 in. | 276.4608 | 7744 | 681472 | 6082.1376 | 77.9856 |
| $\frac{1}{16}$ | 276.6671 | 7755.003 | 682925.031 | 6090.7801 | 78.0409 |
| $\frac{1}{8}$ | 276.8535 | 7766.015 | 684380.125 | 6099.4287 | 78.0964 |
| $\frac{3}{16}$ | 277.0498 | 7777.035 | 685837.283 | 6108.0824 | 78.1518 |
| $\frac{1}{4}$ | 277.2462 | 7788.062 | 687296.516 | 6116.7422 | 78.2071 |
| $\frac{5}{16}$ | 277.4425 | 7799.097 | 688757.807 | 6125.4103 | 78.2625 |
| $\frac{3}{8}$ | 277.6389 | 7810.140 | 690221.175 | 6134.0844 | 78.3179 |
| $\frac{7}{16}$ | 277.8352 | 7821.191 | 691686.614 | 6142.7637 | 78.3733 |
| $\frac{1}{2}$ | 278.0316 | 7832.25 | 693154.125 | 6151.4491 | 78.4287 |
| $\frac{9}{16}$ | 278.2279 | 7843.316 | 694623.708 | 6160.1403 | 78.4841 |
| $\frac{5}{8}$ | 278.4243 | 7854.390 | 696095.367 | 6169.8376 | 78.5395 |
| $\frac{11}{16}$ | 278.6206 | 7865.472 | 697569.001 | 6177.5418 | 78.5949 |
| $\frac{3}{4}$ | 278.8170 | 7876.562 | 699044.922 | 6186.2521 | 78.6503 |
| $\frac{13}{16}$ | 279.0133 | 7887.660 | 700522.883 | 6194.9683 | 78.7057 |
| $\frac{7}{8}$ | 279.2097 | 7898.765 | 702002.793 | 6203.6905 | 78.7610 |
| $\frac{15}{16}$ | 279.4060 | 7909.878 | 703484.744 | 6212.4189 | 78.8164 |
| 89 in. | 279.6024 | 7921 | 704969. | 6221.1534 | 78.8718 |
| $\frac{1}{16}$ | 279.7987 | 7932.128 | 706455.230 | 6229.8941 | 78.9272 |
| $\frac{1}{8}$ | 279.9951 | 7943.265 | 707943.547 | 6238.6408 | 78.9826 |
| $\frac{3}{16}$ | 280.1914 | 7954.410 | 709434.951 | 6247.3927 | 79.0379 |
| $\frac{1}{4}$ | 280.3878 | 7965.562 | 710926.453 | 6256.1507 | 79.0934 |
| $\frac{5}{16}$ | 280.5841 | 7976.722 | 712421.027 | 6264.9170 | 79.1487 |
| $\frac{3}{8}$ | 280.7805 | 7987.890 | 713907.722 | 6273.6893 | 79.2041 |
| $\frac{7}{16}$ | 280.9768 | 7999.066 | 715405.501 | 6282.4668 | 79.2595 |
| $\frac{1}{2}$ | 281.1732 | 8010.25 | 716917.375 | 6291.2503 | 79.3149 |
| $\frac{9}{16}$ | 281.3695 | 8021.441 | 718420.345 | 6300.0397 | 79.3703 |
| $\frac{5}{8}$ | 281.5659 | 8032.640 | 719925.414 | 6308.8351 | 79.4258 |
| $\frac{11}{16}$ | 281.7622 | 8043.847 | 721432.542 | 6317.6375 | 79.4811 |
| $\frac{3}{4}$ | 281.9586 | 8055.062 | 722905.859 | 6326.4460 | 79.5364 |
| $\frac{13}{16}$ | 282.1549 | 8066.285 | 724253.230 | 6335.2603 | 79.5919 |
| $\frac{7}{8}$ | 282.3513 | 8077.515 | 725966.714 | 6344.0807 | 79.6473 |
| $\frac{15}{16}$ | 282.5476 | 8088.753 | 727482.304 | 6352.9073 | 79.7026 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|-----------------|----------|----------|------------|-----------|-------------------|
| 90 in. | 282.7440 | 8100 | 729000 | 6361.7400 | 79.7580 |
| $\frac{1}{16}$ | 282.9403 | 8111.253 | 730519.804 | 6370.5789 | 79.8134 |
| $\frac{1}{8}$ | 283.1367 | 8122.515 | 732041.718 | 6379.4238 | 79.8688 |
| $\frac{3}{16}$ | 283.3330 | 8133.785 | 733565.644 | 6388.7739 | 79.9242 |
| $\frac{1}{4}$ | 283.5294 | 8145.062 | 735091.890 | 6397.1300 | 79.9796 |
| $\frac{5}{16}$ | 283.7257 | 8156.347 | 736619.742 | 6405.9944 | 80.0349 |
| $\frac{3}{8}$ | 283.9221 | 8167.640 | 738150.519 | 6414.8649 | 80.0903 |
| $\frac{7}{16}$ | 284.1184 | 8178.941 | 739683.013 | 6423.7906 | 80.1457 |
| $\frac{1}{2}$ | 284.3148 | 8190.25 | 741217.625 | 6432.6223 | 80.2011 |
| $\frac{9}{16}$ | 284.5111 | 8201.566 | 742754.357 | 6441.5101 | 80.2565 |
| $\frac{5}{8}$ | 284.7075 | 8212.890 | 744293.210 | 6450.4039 | 80.3119 |
| $\frac{11}{16}$ | 284.9038 | 8224.222 | 745824.187 | 6459.3043 | 80.3673 |
| $\frac{3}{4}$ | 285.1002 | 8235.562 | 747377.297 | 6468.2107 | 80.4227 |
| $\frac{13}{16}$ | 285.2965 | 8246.910 | 748922.523 | 6477.1232 | 80.4781 |
| $\frac{7}{8}$ | 285.4929 | 8258.265 | 750469.886 | 6486.0418 | 80.5335 |
| $\frac{15}{16}$ | 285.6892 | 8269.628 | 752019.378 | 6494.9566 | 80.5888 |
| 91 in. | 285.8856 | 8281 | 753571 | 6503.8974 | 80.6442 |
| $\frac{1}{16}$ | 286.0819 | 8292.378 | 755124.753 | 6512.8344 | 80.6996 |
| $\frac{1}{8}$ | 286.2783 | 8303.765 | 756680.640 | 6521.7775 | 80.7550 |
| $\frac{3}{16}$ | 286.4746 | 8315.160 | 758238.661 | 6530.7258 | 80.8104 |
| $\frac{1}{4}$ | 286.6710 | 8326.562 | 759798.828 | 6539.6801 | 80.8658 |
| $\frac{5}{16}$ | 286.8673 | 8337.972 | 761361.123 | 6548.6427 | 80.9211 |
| $\frac{3}{8}$ | 287.0637 | 8349.390 | 762925.566 | 6557.6114 | 80.9765 |
| $\frac{7}{16}$ | 287.2600 | 8360.816 | 764492.149 | 6566.5857 | 81.0319 |
| $\frac{1}{2}$ | 287.4564 | 8372.25 | 766060.875 | 6573.5651 | 81.0873 |
| $\frac{9}{16}$ | 287.6527 | 8383.691 | 767631.744 | 6584.5511 | 81.1427 |
| $\frac{5}{8}$ | 287.8491 | 8395.140 | 769204.757 | 6593.5431 | 81.1981 |
| $\frac{11}{16}$ | 288.0454 | 8406.597 | 770779.917 | 6602.5443 | 81.2535 |
| $\frac{3}{4}$ | 288.2418 | 8418.062 | 772357.234 | 6611.5462 | 81.3089 |
| $\frac{13}{16}$ | 288.4381 | 8429.535 | 773935.773 | 6620.5569 | 81.3643 |
| $\frac{7}{8}$ | 288.6345 | 8441.015 | 775518.308 | 6629.5736 | 81.4197 |
| $\frac{15}{16}$ | 288.8388 | 8452.503 | 777102.077 | 6638.5967 | 81.4750 |
| 92 in. | 289.0272 | 8464 | 778688 | 6647.6258 | 81.5304 |
| $\frac{1}{16}$ | 289.2235 | 8475.503 | 780276.077 | 6656.6609 | 81.5858 |
| $\frac{1}{8}$ | 289.4199 | 8487.015 | 781866.312 | 6665.7021 | 81.6412 |
| $\frac{3}{16}$ | 289.6162 | 8498.535 | 783448.704 | 6674.7485 | 81.6966 |
| $\frac{1}{4}$ | 289.8125 | 8510.062 | 785053.265 | 6683.8010 | 81.7519 |
| $\frac{5}{16}$ | 290.0089 | 8521.597 | 786649.978 | 6692.8618 | 81.8073 |
| $\frac{3}{8}$ | 290.2053 | 8533.140 | 788248.863 | 6701.9286 | 81.8627 |
| $\frac{7}{16}$ | 290.4016 | 8544.691 | 789849.911 | 6711.5001 | 81.9181 |
| $\frac{1}{2}$ | 290.5980 | 8556.25 | 791453.125 | 6720.0787 | 81.9735 |
| $\frac{9}{16}$ | 290.7943 | 8567.816 | 793057.505 | 6729.6628 | 82.0289 |
| $\frac{5}{8}$ | 290.9907 | 8579.390 | 794666.054 | 6738.2530 | 82.0843 |
| $\frac{11}{16}$ | 291.1870 | 8590.972 | 796275.773 | 6747.3497 | 82.1397 |
| $\frac{3}{4}$ | 291.3834 | 8602.562 | 797887.672 | 6756.4525 | 82.1950 |
| $\frac{13}{16}$ | 291.5797 | 8614.160 | 799501.734 | 6765.5614 | 82.2505 |
| $\frac{7}{8}$ | 291.7761 | 8625.765 | 801117.980 | 6774.6763 | 82.3059 |
| $\frac{15}{16}$ | 291.9724 | 8637.378 | 802736.411 | 6783.7975 | 82.3612 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|-----------------|----------|----------|------------|-----------|-------------------|
| 93 in. | 292.1688 | 8649 | 804357 | 6792.9248 | 82.4166 |
| $\frac{1}{16}$ | 292.3651 | 8660.628 | 805979.777 | 6802.0581 | 82.4720 |
| $\frac{1}{8}$ | 292.5615 | 8672.265 | 807604.734 | 6811.1974 | 82.5274 |
| $\frac{3}{16}$ | 292.7578 | 8683.910 | 809231.872 | 6820.3420 | 82.5828 |
| $\frac{1}{4}$ | 292.9542 | 8695.562 | 810861.203 | 6829.4927 | 82.6382 |
| $\frac{5}{16}$ | 293.1505 | 8707.222 | 812492.708 | 6838.6517 | 82.6935 |
| $\frac{3}{8}$ | 293.3469 | 8718.890 | 814126.410 | 6847.8167 | 82.7489 |
| $\frac{7}{16}$ | 293.5432 | 8730.566 | 815762.298 | 6856.9869 | 82.8043 |
| $\frac{1}{2}$ | 293.7396 | 8742.25 | 817400.375 | 6866.1631 | 82.8597 |
| $\frac{9}{16}$ | 293.9359 | 8753.941 | 819040.642 | 6875.3454 | 82.9151 |
| $\frac{5}{8}$ | 294.1323 | 8765.640 | 820683.101 | 6884.5338 | 82.9705 |
| $\frac{11}{16}$ | 294.3286 | 8777.347 | 822328.353 | 6893.7337 | 83.0259 |
| $\frac{3}{4}$ | 294.5350 | 8789.062 | 823974.610 | 6902.9296 | 83.0813 |
| $\frac{13}{16}$ | 294.7213 | 8800.785 | 825623.652 | 6912.1366 | 83.1367 |
| $\frac{7}{8}$ | 294.9177 | 8812.515 | 827274.902 | 6921.3497 | 83.1921 |
| $\frac{15}{16}$ | 295.1140 | 8824.253 | 828928.351 | 6930.5691 | 83.2475 |
| 94 in. | 295.3104 | 8836 | 830584 | 6939.7946 | 83.3028 |
| $\frac{1}{16}$ | 295.5067 | 8847.753 | 832041.851 | 6949.5261 | 83.3582 |
| $\frac{1}{8}$ | 295.7031 | 8859.515 | 833901.906 | 6958.2636 | 83.4136 |
| $\frac{3}{16}$ | 295.8994 | 8871.285 | 835564.165 | 6968.0064 | 83.4690 |
| $\frac{1}{4}$ | 296.0958 | 8883.062 | 837228.640 | 6976.7552 | 83.5244 |
| $\frac{5}{16}$ | 296.2921 | 8894.847 | 838885.214 | 6986.0123 | 83.5797 |
| $\frac{3}{8}$ | 296.4885 | 8906.640 | 840564.207 | 6995.2755 | 83.6351 |
| $\frac{7}{16}$ | 296.6848 | 8918.441 | 842235.209 | 7004.5439 | 83.6905 |
| $\frac{1}{2}$ | 296.8812 | 8930.25 | 843908.625 | 7013.8183 | 83.7459 |
| $\frac{9}{16}$ | 297.0775 | 8942.066 | 845621.988 | 7023.0988 | 83.8013 |
| $\frac{5}{8}$ | 297.2739 | 8953.890 | 847261.898 | 7032.3853 | 83.8567 |
| $\frac{11}{16}$ | 297.4702 | 8965.722 | 848831.858 | 7041.6784 | 83.9121 |
| $\frac{3}{4}$ | 297.6666 | 8977.562 | 850624.047 | 7050.9775 | 83.9675 |
| $\frac{13}{16}$ | 297.8629 | 8989.410 | 852206.445 | 7060.2827 | 84.0229 |
| $\frac{7}{8}$ | 298.0593 | 9001.265 | 853995.074 | 7069.5940 | 84.0783 |
| $\frac{15}{16}$ | 298.2556 | 9013.128 | 856491.925 | 7075.9116 | 84.1336 |
| 95 in. | 298.4520 | 9025 | 857375 | 7088.2352 | 84.1890 |
| $\frac{1}{16}$ | 298.6483 | 9036.878 | 859068.300 | 7097.5738 | 84.2444 |
| $\frac{1}{8}$ | 298.8447 | 9048.765 | 860763.828 | 7106.9005 | 84.2998 |
| $\frac{3}{16}$ | 299.0400 | 9060.660 | 862461.583 | 7116.7415 | 84.3552 |
| $\frac{1}{4}$ | 299.2374 | 9072.562 | 864161.578 | 7125.5885 | 84.4106 |
| $\frac{5}{16}$ | 299.4337 | 9084.472 | 865863.794 | 7134.9443 | 84.4660 |
| $\frac{3}{8}$ | 299.6301 | 9096.390 | 867568.253 | 7144.3052 | 84.5213 |
| $\frac{7}{16}$ | 299.8264 | 9108.316 | 869274.947 | 7153.6717 | 84.5767 |
| $\frac{1}{2}$ | 300.0228 | 9120.25 | 870983.875 | 7163.0443 | 84.6321 |
| $\frac{9}{16}$ | 300.2191 | 9132.191 | 872695.140 | 7172.4230 | 84.6875 |
| $\frac{5}{8}$ | 300.4155 | 9144.140 | 874408.445 | 7181.8077 | 84.7429 |
| $\frac{11}{16}$ | 300.6118 | 9156.097 | 876124.009 | 7191.1989 | 84.7983 |
| $\frac{3}{4}$ | 300.8082 | 9168.062 | 877841.984 | 7200.5962 | 84.8537 |
| $\frac{13}{16}$ | 301.0045 | 9180.035 | 879566.903 | 7209.9096 | 84.9091 |
| $\frac{7}{8}$ | 301.2009 | 9192.015 | 881284.495 | 7219.4090 | 84.9645 |
| $\frac{15}{16}$ | 301.3972 | 9204.003 | 883009.124 | 7228.8248 | 85.0199 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|-----------------|----------|----------|------------|-----------|-------------------|
| 96 in. | 301.5936 | 9216 | 884736 | 7238.2466 | 85.0752 |
| $\frac{1}{16}$ | 301.7899 | 9228.003 | 886465.124 | 7247.6741 | 85.1306 |
| $\frac{1}{8}$ | 301.9863 | 9248.015 | 888965.499 | 7257.1083 | 85.1860 |
| $\frac{3}{16}$ | 302.1826 | 9252.035 | 889930.126 | 7266.5474 | 85.2414 |
| $\frac{1}{4}$ | 302.3790 | 9264.062 | 891666.015 | 7275.9926 | 85.2967 |
| $\frac{5}{16}$ | 302.5753 | 9276.097 | 893401.160 | 7285.4461 | 85.3521 |
| $\frac{3}{8}$ | 302.7717 | 9288.140 | 894944.550 | 7294.9056 | 85.4075 |
| $\frac{7}{16}$ | 302.9680 | 9300.191 | 896887.208 | 7304.3703 | 85.4629 |
| $\frac{1}{2}$ | 303.1644 | 9312.25 | 898632.125 | 7313.8411 | 85.5183 |
| $\frac{9}{16}$ | 303.3607 | 9324.316 | 900379.302 | 7323.3179 | 85.5737 |
| $\frac{5}{8}$ | 303.5571 | 9336.390 | 902128.742 | 7332.8008 | 85.6291 |
| $\frac{11}{16}$ | 303.7534 | 9348.472 | 903786.444 | 7342.2902 | 85.6845 |
| $\frac{3}{4}$ | 303.9498 | 9360.562 | 905634.422 | 7351.7857 | 85.7399 |
| $\frac{13}{16}$ | 304.1461 | 9372.660 | 907397.655 | 7361.2873 | 85.7952 |
| $\frac{7}{8}$ | 304.3425 | 9384.765 | 909149.167 | 7370.7949 | 85.8506 |
| $\frac{15}{16}$ | 304.5388 | 9396.878 | 910909.948 | 7380.3068 | 85.9060 |
| 97 in. | 304.7352 | 9409 | 912673 | 7389.8288 | 85.9614 |
| $\frac{1}{16}$ | 304.9315 | 9421.128 | 914438.324 | 7399.3548 | 86.0167 |
| $\frac{1}{8}$ | 305.1279 | 9433.265 | 916205.921 | 7408.8868 | 86.0722 |
| $\frac{3}{16}$ | 305.3242 | 9445.410 | 916974.794 | 7418.6241 | 86.1276 |
| $\frac{1}{4}$ | 305.5206 | 9457.562 | 919747.953 | 7427.9675 | 86.1830 |
| $\frac{5}{16}$ | 305.7169 | 9469.722 | 921522.380 | 7437.5192 | 86.2383 |
| $\frac{3}{8}$ | 305.9133 | 9481.890 | 923299.097 | 7447.0769 | 86.2937 |
| $\frac{7}{16}$ | 306.1096 | 9494.066 | 924072.095 | 7456.6398 | 86.3491 |
| $\frac{1}{2}$ | 306.3060 | 9506.25 | 926859.375 | 7466.2087 | 86.4045 |
| $\frac{9}{16}$ | 306.5023 | 9518.441 | 928642.939 | 7475.7837 | 86.4599 |
| $\frac{5}{8}$ | 306.6987 | 9530.640 | 930428.788 | 7485.3648 | 86.5153 |
| $\frac{11}{16}$ | 306.8950 | 9542.847 | 932215.924 | 7494.9524 | 86.5670 |
| $\frac{3}{4}$ | 307.0914 | 9555.062 | 934007.359 | 7504.5460 | 86.6226 |
| $\frac{13}{16}$ | 307.2877 | 9567.285 | 935800.073 | 7514.1457 | 86.6814 |
| $\frac{7}{8}$ | 307.4841 | 9579.515 | 937595.089 | 7523.7515 | 86.7368 |
| $\frac{15}{16}$ | 307.6804 | 9591.753 | 939392.397 | 7533.3636 | 86.7922 |
| 98 in. | 307.8763 | 9604 | 941192 | 7542.9818 | 86.8476 |
| $\frac{1}{16}$ | 308.0731 | 9616.253 | 942993.898 | 7552.6060 | 86.9030 |
| $\frac{1}{8}$ | 308.2695 | 9628.515 | 944789.093 | 7562.2362 | 86.9584 |
| $\frac{3}{16}$ | 308.4658 | 9640.785 | 946604.587 | 7571.8717 | 87.0138 |
| $\frac{1}{4}$ | 308.6622 | 9653.062 | 948413.390 | 7581.5132 | 87.0692 |
| $\frac{5}{16}$ | 308.8585 | 9665.347 | 950224.485 | 7591.1630 | 87.1245 |
| $\frac{3}{8}$ | 309.0549 | 9677.640 | 952037.894 | 7600.8189 | 87.1799 |
| $\frac{7}{16}$ | 309.2512 | 9689.941 | 953852.606 | 7610.4800 | 87.2353 |
| $\frac{1}{2}$ | 309.4476 | 9702.25 | 955671.625 | 7620.1471 | 87.2907 |
| $\frac{9}{16}$ | 309.6439 | 9714.566 | 957591.730 | 7629.8203 | 87.3461 |
| $\frac{5}{8}$ | 309.8403 | 9726.890 | 959314.585 | 7639.4995 | 87.4015 |
| $\frac{11}{16}$ | 310.0366 | 9739.222 | 961139.530 | 7649.1853 | 87.4569 |
| $\frac{3}{4}$ | 310.2330 | 9751.562 | 962966.797 | 7658.8771 | 87.5123 |
| $\frac{13}{16}$ | 310.4293 | 9763.910 | 964956.366 | 7668.5750 | 87.5677 |
| $\frac{7}{8}$ | 310.6257 | 9776.265 | 966628.261 | 7678.2790 | 87.6231 |
| $\frac{15}{16}$ | 310.8220 | 9788.628 | 968362.471 | 7687.9893 | 87.6785 |

| Dia. or Root. | Circum. | Square. | Cube. | Area. | Side of = square. |
|------------------|----------|-----------|-------------|-----------|----------------------|
| 99 in. | 311.0184 | 9801 | 970299 | 7697.7056 | 87.7338 |
| $\frac{1}{16}$ | 311.2147 | 9813.378 | 972137.847 | 7707.4279 | 87.7892 |
| $\frac{1}{8}$ | 311.4111 | 9825.765 | 973979.015 | 7717.1563 | 87.8446 |
| $\frac{3}{16}$ | 311.6074 | 9838.160 | 975821.504 | 7726.8900 | 87.9001 |
| $\frac{1}{4}$ | 311.8038 | 9850.562 | 977668.328 | 7736.6297 | 87.9554 |
| $\frac{5}{16}$ | 312.0001 | 9862.972 | 979516.476 | 7746.3777 | 88.0107 |
| $\frac{3}{8}$ | 312.1965 | 9875.390 | 981366.941 | 7756.1318 | 88.0661 |
| $\frac{7}{16}$ | 312.3928 | 9887.816 | 983218.743 | 7765.8910 | 88.1215 |
| $\frac{1}{2}$ | 312.5892 | 9900.25 | 985074.875 | 7775.6563 | 88.1769 |
| $\frac{9}{16}$ | 312.7855 | 9912.691 | 986932.337 | 7785.4277 | 88.2323 |
| $\frac{5}{8}$ | 312.9819 | 9925.140 | 988792.132 | 7795.2051 | 88.2877 |
| $\frac{11}{16}$ | 313.0782 | 9937.597 | 990654.210 | 7804.9890 | 88.3431 |
| $\frac{3}{4}$ | 313.3746 | 9950.062 | 992518.734 | 7814.7790 | 88.3985 |
| $\frac{13}{16}$ | 313.5709 | 9962.535 | 994385.534 | 7824.5751 | 88.4539 |
| $\frac{7}{8}$ | 313.7673 | 9975.015 | 996254.683 | 7834.3772 | 88.5093 |
| $\frac{15}{16}$ | 313.9636 | 9987.503 | 998122.170 | 7844.1856 | 88.5646 |
| 100 in. | 314.1600 | 10000 | 1000000 | 7854.0000 | 88.6200 |
| $\frac{1}{4}$ | 314.9454 | 10050.062 | 1007518.765 | 7893.3190 | 88.8415 |
| $\frac{1}{2}$ | 315.7308 | 10100.25 | 1015075.125 | 7932.7360 | 89.0631 |
| $\frac{3}{4}$ | 316.5162 | 10150.562 | 1022669.171 | 7972.2120 | 89.2847 |
| 101 in. | 317.3016 | 10201 | 1030301 | 8011.8652 | 89.5062 |
| $\frac{1}{4}$ | 318.0870 | 10251.562 | 1037970.703 | 8051.5772 | 89.7278 |
| $\frac{1}{2}$ | 318.8724 | 10302.25 | 1045678.37 | 8091.3870 | 89.9493 |
| $\frac{3}{4}$ | 319.6578 | 10353.062 | 1053424.109 | 8131.2953 | 90.1709 |
| 102 in. | 320.4432 | 10404 | 1061208 | 8171.3016 | 90.3924 |
| $\frac{1}{4}$ | 321.2286 | 10455.062 | 1069030.140 | 8211.4060 | 90.6140 |
| $\frac{1}{2}$ | 322.0140 | 10506.25 | 1076890.625 | 8251.6084 | 90.8355 |
| $\frac{3}{4}$ | 322.7994 | 10557.562 | 1084789.546 | 8291.8696 | 91.0571 |
| 103 in. | 323.5848 | 10609 | 1092727 | 8332.3085 | 91.2786 |
| $\frac{1}{4}$ | 324.3702 | 10660.562 | 1100703.078 | 8372.8056 | 91.5002 |
| $\frac{1}{2}$ | 325.1556 | 10712.25 | 1108717.875 | 8413.4008 | 91.7217 |
| $\frac{3}{4}$ | 325.9410 | 10764.059 | 1116771.173 | 8454.0944 | 91.9433 |
| 104 in. | 326.7264 | 10816 | 1124864 | 8494.8864 | 92.1648 |
| $\frac{1}{4}$ | 327.5118 | 10868.062 | 1132995.526 | 8535.7760 | 92.3864 |
| $\frac{1}{2}$ | 328.2972 | 10920.25 | 1141166.125 | 8576.7640 | 92.6079 |
| $\frac{3}{4}$ | 329.0826 | 11032.562 | 1155660.921 | 8617.8504 | 92.8295 |
| 105 in. | 329.8680 | 11025 | 1157625 | 8659.0348 | 93.0510 |
| $\frac{1}{4}$ | 330.6534 | 11077.562 | 1165913.453 | 8700.3176 | 93.2726 |
| $\frac{1}{2}$ | 331.4388 | 11130.25 | 1174241.375 | 8741.6980 | 93.4941 |
| $\frac{3}{4}$ | 332.2242 | 11183.062 | 1182608.859 | 8783.1772 | 93.7157 |
| 106 in. | 333.0096 | 11236 | 1191016 | 8824.7544 | 93.9372 |
| $\frac{1}{4}$ | 334.5804 | 11342.25 | 1207949.625 | 8908.2028 | 94.3803 |
| 107 in. | 336.1512 | 11449 | 1225043 | 8992.0444 | 94.8234 |
| $\frac{1}{2}$ | 337.7220 | 11556.25 | 1242296.875 | 9076.2784 | 95.2665 |
| 108 in. | 339.2928 | 11664 | 1259712 | 9160.9056 | 95.7096 |
| $\frac{1}{4}$ | 340.8636 | 11772.25 | 1277289.125 | 9245.9248 | 96.1527 |
| 109 in. | 342.4344 | 11881 | 1295029 | 9331.3372 | 96.5958 |
| $\frac{1}{2}$ | 344.0052 | 11990.25 | 1312932.375 | 9417.1420 | 97.0389 |
| 110 in. | 345.5760 | 12100 | 1331000 | 9503.3400 | 97.4820 |

A TABLE
CONTAINING
THE CIRCUMFERENCES & AREAS OF CIRCLES,
From 1 to 50 Feet, advancing by an Inch ;
ALSO,
THE SIDE OF A SQUARE OF EQUAL AREA,
AND THE
*Content of each in Imperial Gallons and Cubic Yards, at 1 Foot
in depth.*

| Dia. in feet & inches. | Circum. in feet and inches. | Area in feet. | Side of — square in ft. and in. | Gallons at 1 foot in depth. | Cubicyards at 1 foot in depth. |
|------------------------------|-----------------------------------|---------------|---------------------------------------|--------------------------------|--------------------------------------|
| 1 ft. | 3 1% | .7854 | 0 10% | 4.8946 | .0291 |
| 1 | 3 4% | .9217 | 0 11½ | 5.7440 | .0341 |
| 2 | 3 8 | 1.0690 | 1 0% | 6.6620 | .0395 |
| 3 | 3 11 | 1.2271 | 1 1¼ | 7.6472 | .0454 |
| 4 | 4 2% | 1.3962 | 1 2½ | 8.7011 | .0517 |
| 5 | 4 5% | 1.5761 | 1 3 | 9.8222 | .0583 |
| 6 | 4 8½ | 1.7671 | 1 3¾ | 11.0125 | .0654 |
| 7 | 4 11% | 1.9689 | 1 4% | 12.2701 | .0729 |
| 8 | 5 2% | 2.1816 | 1 5% | 13.5957 | .0808 |
| 9 | 5 5% | 2.4052 | 1 6½ | 14.9892 | .0890 |
| 10 | 5 9 | 2.6398 | 1 7½ | 16.4512 | .0977 |
| 11 | 6 2¼ | 2.8852 | 1 8% | 17.9025 | .1068 |
| 2 ft. | 6 3% | 3.1416 | 1 9¼ | 19.5784 | .1163 |
| 1 | 6 6% | 3.4087 | 1 10½ | 21.2430 | .1262 |
| 2 | 6 9% | 3.6869 | 1 11 | 22.9767 | .1365 |
| 3 | 7 0% | 3.9760 | 1 11½ | 24.7784 | .1472 |
| 4 | 7 3% | 4.2760 | 2 0% | 27.2480 | .1583 |
| 5 | 7 7 | 4.5869 | 2 1% | 28.5855 | .1698 |
| 6 | 7 10¼ | 4.9087 | 2 2½ | 30.5910 | .1818 |
| 7 | 8 1% | 5.2413 | 2 3% | 32.6637 | .1941 |
| 8 | 8 4½ | 5.5850 | 2 4¼ | 34.8057 | .2068 |
| 9 | 8 7% | 5.9398 | 2 5¼ | 37.0149 | .2199 |
| 10 | 8 10% | 6.3049 | 2 6½ | 39.2921 | .2335 |
| 11 | 9 1% | 6.6813 | 2 7 | 41.6378 | .2474 |
| 3 ft. | 9 5 | 7.0686 | 2 7½ | 44.0515 | .2618 |
| 1 | 9 8¼ | 7.4666 | 2 8% | 46.5318 | .2765 |
| 2 | 9 11% | 7.8757 | 2 9¼ | 49.0818 | .2916 |
| 3 | 10 2% | 8.2957 | 2 10¼ | 51.6988 | .3072 |
| 4 | 10 5% | 8.7265 | 2 11% | 54.3835 | .3232 |
| 5 | 10 8% | 9.1683 | 3 0¼ | 57.0994 | .3395 |
| 6 | 10 11% | 9.6211 | 3 1½ | 60.9587 | .3565 |
| 7 | 11 3 | 10.0846 | 3 2 | 62.8472 | .3733 |
| 8 | 11 6% | 10.5591 | 3 3 | 65.8043 | .3911 |
| 9 | 11 9% | 11.0446 | 3 3¾ | 68.8299 | .4090 |
| 10 | 12 5% | 11.5409 | 3 4% | 71.9228 | .4274 |
| 11 | 12 8% | 12.0481 | 3 5% | 75.0837 | .4462 |
| 4 ft. | 12 6% | 12.5664 | 3 6½ | 78.3128 | .4654 |
| 1 | 12 9% | 13.0952 | 3 7% | 81.6092 | .4851 |
| 2 | 13 1 | 13.6353 | 3 8¼ | 84.9751 | .5050 |
| 3 | 13 4% | 14.1862 | 3 9% | 85.8583 | .5254 |
| 4 | 13 7¼ | 14.7479 | 3 10 | 91.9089 | .5462 |
| 5 | 13 10% | 15.3206 | 3 10½ | 95.4779 | .5674 |
| 6 | 14 1% | 15.9043 | 3 11% | 99.1155 | .5893 |
| 7 | 14 4% | 16.4986 | 4 0% | 102.8192 | .6111 |
| 8 | 14 7% | 17.1041 | 4 1% | 106.5927 | .6334 |
| 9 | 14 11 | 17.7205 | 4 2½ | 110.4341 | .6563 |
| 10 | 15 2% | 18.3476 | 4 3% | 114.3421 | .6795 |
| 11 | 15 5¼ | 18.9858 | 4 4¼ | 118.3818 | .7032 |

| Dia. in feet & inches. | Circum. in feet & inches. | Area in feet. | Side of — square in ft. and in. | Gallons at 1 foot in depth. | Cubic yards at 1 foot in depth. |
|------------------------------|---------------------------------|---------------|---------------------------------------|--------------------------------|---------------------------------------|
| 5 ft. | 15 8% | 19.6350 | 4 5% | 122.3653 | .7272 |
| 1 | 15 11% | 20.2947 | 4 6 | 126.4765 | .7516 |
| 2 | 16 2% | 20.9656 | 4 6% | 130.6576 | .7764 |
| 3 | 16 5% | 21.6475 | 4 7% | 134.9072 | .8017 |
| 4 | 16 9 | 22.3400 | 4 8% | 139.2228 | .8275 |
| 5 | 17 0% | 23.0437 | 4 9% | 143.6083 | .8534 |
| 6 | 17 3% | 23.7583 | 4 10% | 148.0617 | .8800 |
| 7 | 17 6% | 24.4835 | 4 11% | 152.5811 | .9071 |
| 8 | 17 9% | 25.2199 | 5 0% | 157.1704 | .9340 |
| 9 | 18 0% | 25.9672 | 5 1% | 161.8275 | .9617 |
| 10 | 18 3% | 26.7251 | 5 2 | 166.5508 | .9897 |
| 11 | 18 7% | 27.4943 | 5 2% | 171.3444 | 1.0184 |
| 6 ft. | 18 10% | 28.2744 | 5 3% | 176.2060 | 1.0472 |
| 1 | 19 1% | 29.0649 | 5 4% | 181.1324 | 1.0764 |
| 2 | 19 4% | 29.8668 | 5 5% | 185.1298 | 1.1042 |
| 3 | 19 7% | 30.6796 | 5 6% | 191.1952 | 1.1363 |
| 4 | 19 10% | 31.5029 | 5 7% | 196.3320 | 1.1667 |
| 5 | 20 1% | 32.3376 | 5 8% | 201.5279 | 1.1976 |
| 6 | 20 4% | 33.1831 | 5 9% | 206.7970 | 1.2290 |
| 7 | 20 8% | 34.0391 | 5 10 | 212.1376 | 1.2607 |
| 8 | 20 11% | 34.9065 | 5 10% | 217.5373 | 1.2928 |
| 9 | 21 2% | 35.7847 | 5 11% | 223.0102 | 1.3253 |
| 10 | 21 5% | 36.6735 | 6 0% | 228.4492 | 1.3582 |
| 11 | 21 8% | 37.5736 | 6 1% | 234.1586 | 1.3926 |
| 7 ft. | 21 11% | 38.4846 | 6 2% | 239.8360 | 1.4254 |
| 1 | 22 3 | 39.4060 | 6 3% | 245.5781 | 1.4602 |
| 2 | 22 6% | 40.3388 | 6 4% | 251.3914 | 1.4940 |
| 3 | 22 9% | 41.2825 | 6 5% | 257.2725 | 1.5300 |
| 4 | 23 0% | 42.2367 | 6 6 | 263.2191 | 1.5643 |
| 5 | 23 2% | 43.2022 | 6 6% | 269.2361 | 1.6001 |
| 6 | 23 6% | 44.1787 | 6 7% | 275.3216 | 1.6361 |
| 7 | 23 11 | 45.1656 | 6 8% | 281.4720 | 1.6728 |
| 8 | 24 1% | 46.1638 | 6 9% | 287.6928 | 1.7098 |
| 9 | 24 4% | 47.1730 | 6 10% | 293.9721 | 1.7471 |
| 10 | 24 7% | 48.1926 | 6 11% | 300.3362 | 1.7849 |
| 11 | 24 10% | 49.2236 | 7 0 | 306.7614 | 1.8231 |
| 8 ft. | 25 1% | 50.2656 | 7 0% | 313.2552 | 1.8617 |
| 1 | 25 4% | 51.3173 | 7 1% | 319.8125 | 1.9007 |
| 2 | 25 7% | 52.3816 | 7 2% | 326.4421 | 1.9394 |
| 3 | 25 11 | 53.4562 | 7 3% | 333.1390 | 1.9800 |
| 4 | 26 2% | 54.5412 | 7 4% | 339.9007 | 2.0201 |
| 5 | 26 5% | 55.6377 | 7 5% | 346.7341 | 2.0607 |
| 6 | 26 8% | 56.7451 | 7 6% | 353.6354 | 2.1017 |
| 7 | 26 11% | 57.8628 | 7 7% | 360.6009 | 2.1430 |
| 8 | 27 2% | 58.9920 | 7 8% | 367.6381 | 2.1850 |
| 9 | 27 5% | 60.1321 | 7 9% | 374.3432 | 2.2698 |
| 10 | 27 9 | 61.2826 | 7 9% | 381.9031 | 2.3128 |
| 11 | 28 0% | 62.4445 | 7 10% | 389.1541 | 2.4001 |

4.434
4.484
4.545
4.605
4.667
4.729
4.791
4.853

| Dia. in feet & inches. | Circum. in feet and inches. | Area in feet. | Side of = square in ft. and in. | Gallons at 1 foot in depth. | Cubic yards at 1 foot in depth. |
|------------------------|-----------------------------|---------------|---------------------------------|-----------------------------|---------------------------------|
| 13 ft. | 40 10 | 132.7326 | 11 6 1/4 | 827.1895 | 4.9160 |
| 1 | 41 1 1/2 | 134.4391 | 11 7 1/2 | 837.8244 | 4.9792 |
| 2 | 41 4 1/2 | 136.1574 | 11 8 3/8 | 848.5329 | 5.0428 |
| 3 | 41 7 1/2 | 137.8867 | 11 8 7/8 | 859.3099 | 5.1106 |
| 4 | 41 10 1/2 | 139.6260 | 11 9 1/4 | 870.1492 | 5.1713 |
| 5 | 42 1 1/2 | 141.3771 | 11 10 1/8 | 881.0620 | 5.2361 |
| 6 | 42 4 1/2 | 143.1391 | 11 11 1/8 | 892.0428 | 5.3014 |
| 7 | 42 8 | 144.9111 | 12 0 1/2 | 907.0859 | 5.3670 |
| 8 | 42 11 1/2 | 146.6949 | 12 1 1/4 | 914.2026 | 5.4331 |
| 9 | 43 2 1/2 | 148.4896 | 12 2 1/8 | 923.3871 | 5.4996 |
| 10 | 43 5 1/2 | 150.2943 | 12 3 1/8 | 936.6340 | 5.5653 |
| 11 | 43 8 1/2 | 152.1109 | 12 4 | 947.9551 | 5.6337 |
| 14 ft. | 43 11 1/2 | 153.9384 | 12 4 1/2 | 959.3441 | 5.7014 |
| 1 | 44 2 1/2 | 155.7758 | 12 5 1/8 | 970.7947 | 5.7694 |
| 2 | 44 6 | 157.6250 | 12 6 1/8 | 982.3190 | 5.8369 |
| 3 | 44 9 1/2 | 159.4852 | 12 7 1/8 | 993.9117 | 5.9069 |
| 4 | 45 0 1/2 | 161.3553 | 12 8 1/8 | 1005.5662 | 5.9761 |
| 5 | 45 3 1/2 | 163.2373 | 12 9 1/8 | 1017.2958 | 6.0458 |
| 6 | 45 6 1/2 | 165.1303 | 12 10 1/8 | 1029.0920 | 6.1159 |
| 7 | 45 9 1/2 | 167.0331 | 12 11 1/8 | 1040.9502 | 6.1864 |
| 8 | 46 0 1/2 | 168.9479 | 13 0 | 1052.8733 | 6.2578 |
| 9 | 46 4 | 170.8735 | 13 1 1/8 | 1064.8846 | 6.3286 |
| 10 | 46 7 1/2 | 172.8091 | 13 1 1/2 | 1076.9462 | 6.4410 |
| 11 | 46 11 1/2 | 174.7565 | 13 2 1/8 | 1089.0825 | 6.4724 |
| 15 ft. | 47 1 1/2 | 176.7150 | 13 3 1/8 | 1101.2878 | 6.5450 |
| 1 | 47 4 1/2 | 178.6832 | 13 4 1/8 | 1113.4537 | 6.6178 |
| 2 | 47 7 1/2 | 180.6634 | 13 5 1/8 | 1125.8943 | 6.6912 |
| 3 | 47 10 1/2 | 182.6545 | 13 6 1/8 | 1138.3028 | 6.7649 |
| 4 | 48 2 1/2 | 184.6555 | 13 7 1/8 | 1149.7730 | 6.8390 |
| 5 | 48 5 1/2 | 186.6684 | 13 8 | 1163.3174 | 6.9126 |
| 6 | 48 8 1/2 | 188.6923 | 13 8 1/8 | 1172.9304 | 6.9886 |
| 7 | 48 11 1/2 | 190.7260 | 13 9 1/8 | 1188.6954 | 7.0639 |
| 8 | 49 2 1/2 | 192.7716 | 13 10 1/8 | 1201.3626 | 7.1396 |
| 9 | 49 5 1/2 | 194.8262 | 13 11 1/8 | 1214.1693 | 7.2158 |
| 10 | 49 8 1/2 | 196.8946 | 14 0 1/8 | 1227.0471 | 7.2923 |
| 11 | 50 0 | 198.9730 | 14 1 1/8 | 1236.9997 | 7.3698 |
| 16 ft. | 50 3 1/2 | 201.0624 | 14 2 1/8 | 1253.0208 | 7.4467 |
| 1 | 50 6 1/2 | 203.1615 | 14 3 | 1266.1023 | 7.5245 |
| 2 | 50 9 1/2 | 205.2726 | 14 3 1/8 | 1279.2588 | 7.6026 |
| 3 | 51 0 1/2 | 207.3946 | 14 4 1/8 | 1292.4831 | 7.6812 |
| 4 | 51 3 1/2 | 209.5264 | 14 5 1/8 | 1306.7685 | 7.7602 |
| 5 | 51 6 1/2 | 211.6703 | 14 6 1/8 | 1319.1293 | 7.8306 |
| 6 | 51 10 | 213.8251 | 14 7 1/8 | 1332.5580 | 7.9104 |
| 7 | 52 1 1/2 | 215.9896 | 14 8 1/8 | 1346.0471 | 7.9900 |
| 8 | 52 4 1/2 | 218.1662 | 14 9 1/8 | 1359.6138 | 8.0696 |
| 9 | 52 7 1/2 | 220.3537 | 14 10 1/8 | 1373.2442 | |
| 10 | 52 10 1/2 | 222.5510 | 14 11 | 1386.9378 | |
| 11 | 53 1 1/2 | 224.7603 | 14 11 1/8 | 1400.7061 | |

| Dis. in feet & inches. | Circum. in feet and inches. | Area in feet. | Side of square in ft. and in. | Gallons at 1 foot in depth. | Cubicyards at 1 foot in depth. |
|------------------------|-----------------------------|---------------|-------------------------------|-----------------------------|--------------------------------|
| 9 ft. | 28 3 1/4 | 63.6174 | 7 11 1/4 | 396.4636 | 2.3562 |
| 1 | 28 6 1/4 | 64.8006 | 8 0 1/4 | 403.8378 | 2.4000 |
| 2 | 28 9 1/4 | 65.9951 | 8 1 1/4 | 411.2814 | 2.4443 |
| 3 | 29 0 1/4 | 67.2007 | 8 2 1/4 | 418.7947 | 2.4889 |
| 4 | 29 3 1/4 | 68.4166 | 8 3 1/4 | 426.3722 | 2.5339 |
| 5 | 29 7 | 69.6440 | 8 4 1/4 | 434.0214 | 2.5795 |
| 6 | 29 10 1/4 | 70.8823 | 8 5 | 441.7384 | 2.6263 |
| 7 | 30 1 1/4 | 72.1309 | 8 5 1/4 | 449.5197 | 2.6715 |
| 8 | 30 4 1/4 | 73.3910 | 8 6 1/4 | 457.3727 | 2.7183 |
| 9 | 30 7 1/4 | 74.6620 | 8 7 1/4 | 465.2935 | 2.7653 |
| 10 | 30 11 1/4 | 75.9433 | 8 8 1/4 | 473.2786 | 2.8128 |
| 11 | 31 1 1/4 | 77.2362 | 8 9 1/4 | 481.3359 | 2.8607 |
| 10 ft. | 31 5 | 78.5400 | 8 10 1/4 | 489.4612 | 2.9089 |
| 1 | 31 8 1/4 | 79.8540 | 8 11 1/4 | 497.6501 | 2.9575 |
| 2 | 31 11 1/4 | 81.1795 | 9 0 1/4 | 505.9106 | 3.0066 |
| 3 | 32 2 1/4 | 82.5160 | 9 1 | 514.2397 | 3.0561 |
| 4 | 32 5 1/4 | 83.8627 | 9 1 1/4 | 522.6323 | 3.1060 |
| 5 | 32 8 1/4 | 85.2211 | 9 2 1/4 | 530.9978 | 3.1563 |
| 6 | 32 11 1/4 | 86.5903 | 9 3 1/4 | 539.6307 | 3.2070 |
| 7 | 33 2 1/4 | 87.9697 | 9 4 1/4 | 548.2271 | 3.2211 |
| 8 | 33 6 1/4 | 89.3608 | 9 5 1/4 | 556.8965 | 3.3096 |
| 9 | 33 9 1/4 | 90.7627 | 9 6 1/4 | 565.2331 | 3.3615 |
| 10 | 34 0 1/4 | 92.1749 | 9 7 1/4 | 574.4339 | 3.4138 |
| 11 | 34 3 1/4 | 93.5986 | 9 8 1/4 | 583.8064 | 3.4665 |
| 11 ft. | 34 6 1/4 | 95.0334 | 9 8 1/2 | 592.2481 | 3.5197 |
| 1 | 34 9 1/4 | 96.4783 | 9 9 1/2 | 601.2529 | 3.5733 |
| 2 | 35 0 1/4 | 97.9347 | 9 10 1/2 | 610.3290 | 3.6272 |
| 3 | 35 4 1/4 | 99.4021 | 9 11 1/2 | 619.4738 | 3.6815 |
| 4 | 35 7 1/4 | 100.8797 | 10 0 1/2 | 628.6822 | 3.7362 |
| 5 | 35 10 1/4 | 102.3689 | 10 1 1/2 | 637.9629 | 3.7914 |
| 6 | 36 1 1/4 | 103.8691 | 10 2 1/2 | 647.3122 | 3.8470 |
| 7 | 36 4 1/4 | 105.3794 | 10 3 1/2 | 656.7244 | 3.9029 |
| 8 | 36 7 1/4 | 106.9013 | 10 4 | 666.2089 | 3.9593 |
| 9 | 36 10 1/4 | 108.4342 | 10 5 | 675.7619 | 4.0160 |
| 10 | 37 2 1/4 | 109.9772 | 10 5 1/2 | 685.3779 | 4.0732 |
| 11 | 37 5 1/4 | 111.5319 | 10 6 1/2 | 695.0668 | 4.1308 |
| 12 ft. | 37 8 1/4 | 113.0976 | 10 7 1/2 | 706.8242 | 4.1888 |
| 1 | 37 11 1/4 | 114.6732 | 10 8 1/2 | 714.6433 | 4.2471 |
| 2 | 38 2 1/4 | 116.2607 | 10 9 1/2 | 724.5366 | 4.3059 |
| 3 | 38 5 1/4 | 117.8590 | 10 10 1/2 | 734.4972 | 4.3651 |
| 4 | 38 8 1/4 | 119.4674 | 10 11 1/2 | 744.5208 | 4.4241 |
| 5 | 39 0 | 121.0876 | 11 0 | 754.5179 | 4.4847 |
| 6 | 39 3 1/4 | 122.7187 | 11 0 1/2 | 764.7829 | 4.5451 |
| 7 | 39 6 1/4 | 124.3598 | 11 1 1/2 | 775.0102 | 4.6059 |
| 8 | 39 9 1/4 | 126.0127 | 11 2 1/2 | 785.3111 | 4.6671 |
| 9 | 40 0 1/4 | 127.6765 | 11 3 1/2 | 795.6799 | 4.7287 |
| 10 | 40 3 1/4 | 129.3504 | 11 4 1/2 | 806.1116 | 4.7907 |
| 11 | 40 6 1/4 | 131.0360 | 11 5 1/2 | 816.6163 | 4.8531 |

| Dia. in feet & inches. | Circum. in feet and inches. | Area in feet. | Side of = square in ft. and in. | Gallons at 1 foot in depth. | Cubic yards at 1 foot in depth. |
|------------------------|-----------------------------|---------------|---------------------------------|-----------------------------|---------------------------------|
| 13 ft. | 40 10 | 132.7526 | 11 6% | 827.1895 | 4.9160 |
| 1 | 41 1 ½ | 134.4391 | 11 7% | 837.8244 | 4.9792 |
| 2 | 41 4% | 136.1574 | 11 8% | 848.5329 | 5.0428 |
| 3 | 41 7% | 137.8867 | 11 8% | 859.3099 | 5.1106 |
| 4 | 41 10% | 139.6260 | 11 9% | 870.1492 | 5.1713 |
| 5 | 42 1% | 141.3771 | 11 10% | 881.0620 | 5.2361 |
| 6 | 42 4% | 143.1391 | 11 11% | 892.0428 | 5.3014 |
| 7 | 42 8 | 144.9111 | 12 0% | 907.0859 | 5.3670 |
| 8 | 42 11 ½ | 146.6949 | 12 1% | 914.2026 | 5.4331 |
| 9 | 43 2 ½ | 148.4896 | 12 2% | 923.3871 | 5.4996 |
| 10 | 43 5% | 150.2943 | 12 3% | 936.6340 | 5.5653 |
| 11 | 43 8% | 152.1109 | 12 4 | 947.9551 | 5.6337 |
| 14 ft. | 43 11 ½ | 153.9384 | 12 4% | 959.3441 | 5.7014 |
| 1 | 44 2% | 155.7758 | 12 5% | 970.7947 | 5.7694 |
| 2 | 44 6 | 157.6250 | 12 6% | 982.3190 | 5.8369 |
| 3 | 44 9% | 159.4852 | 12 7 ½ | 993.9117 | 5.9069 |
| 4 | 45 0 ½ | 161.3553 | 12 8% | 1005.5662 | 5.9761 |
| 5 | 45 3% | 163.2373 | 12 9% | 1017.2958 | 6.0458 |
| 6 | 45 6% | 165.1303 | 12 10 ½ | 1029.0920 | 6.1159 |
| 7 | 45 9% | 167.0331 | 12 11 ½ | 1040.9502 | 6.1864 |
| 8 | 46 0% | 168.9479 | 13 0 | 1052.8733 | 6.2573 |
| 9 | 46 4 | 170.8735 | 13 1 ½ | 1064.8846 | 6.3286 |
| 10 | 46 7 ½ | 172.8091 | 13 1% | 1076.9462 | 6.4410 |
| 11 | 46 11 ½ | 174.7565 | 13 2% | 1089.0825 | 6.4724 |
| 15 ft. | 47 1 ½ | 176.7150 | 13 3% | 1101.2878 | 6.5450 |
| 1 | 47 4% | 178.6832 | 13 4% | 1113.4537 | 6.6178 |
| 2 | 47 7% | 180.6634 | 13 5% | 1125.8943 | 6.6912 |
| 3 | 47 10% | 182.6545 | 13 6% | 1138.3028 | 6.7649 |
| 4 | 48 2% | 184.6555 | 13 7% | 1149.7730 | 6.8390 |
| 5 | 48 5% | 186.6684 | 13 8 | 1163.3174 | 6.9126 |
| 6 | 48 8 ½ | 188.6923 | 13 8% | 1172.9304 | 6.9886 |
| 7 | 48 11 ½ | 190.7260 | 13 9% | 1188.6954 | 7.0639 |
| 8 | 49 2% | 192.7716 | 13 10% | 1201.3626 | 7.1396 |
| 9 | 49 5% | 194.8282 | 13 11 ½ | 1214.1693 | 7.2158 |
| 10 | 49 8% | 196.8946 | 14 0% | 1227.0471 | 7.2923 |
| 11 | 50 0 | 198.9730 | 14 1 ½ | 1236.9997 | 7.3693 |
| 16 ft. | 50 3 ½ | 201.0624 | 14 2% | 1253.0208 | 7.4467 |
| 1 | 50 6 ½ | 203.1615 | 14 3 | 1266.1023 | 7.5245 |
| 2 | 50 9% | 205.2726 | 14 3% | 1279.2588 | 7.6026 |
| 3 | 51 0 ½ | 207.3946 | 14 4% | 1292.4831 | 7.6812 |
| 4 | 51 3% | 209.5264 | 14 5% | 1306.7685 | 7.7602 |
| 5 | 51 6% | 211.6703 | 14 6% | 1319.1293 | 7.8396 |
| 6 | 51 10 | 213.8251 | 14 7 ½ | 1332.5580 | 7.9194 |
| 7 | 52 1 ½ | 215.9896 | 14 8% | 1346.0471 | 7.9996 |
| 8 | 52 4 ½ | 218.1662 | 14 9 ½ | 1359.6138 | 8.0802 |
| 9 | 52 7% | 220.3537 | 14 10 ½ | 1373.2442 | 8.1612 |
| 10 | 52 10 ½ | 222.5510 | 14 11 | 1386.9378 | 8.2426 |
| 11 | 53 1% | 224.7603 | 14 11 ½ | 1400.7061 | 8.3444 |

| Dia. in feet & inches. | Circum. in feet & inches. | Area in feet. | Side of square in ft. and in. | Gallons at 1 foot in depth. | Cubic yards at 1 foot in depth. |
|------------------------|---------------------------|---------------|-------------------------------|-----------------------------|---------------------------------|
| 17 ft. | 53 4% | 226.9806 | 15 0% | 1414.5430 | 8.4067 |
| 1 | 53 8 | 229.2105 | 15 1% | 1428.4398 | 8.4890 |
| 2 | 53 11% | 231.4525 | 15 2% | 1442.4119 | 8.5352 |
| 3 | 54 2% | 233.7055 | 15 3% | 1456.4526 | 8.6557 |
| 4 | 54 5% | 235.9682 | 15 4% | 1470.5538 | 8.7395 |
| 5 | 54 8% | 238.2430 | 15 5% | 1484.6303 | 8.8238 |
| 6 | 54 11% | 240.5287 | 15 6% | 1498.9748 | 8.9081 |
| 7 | 55 2% | 242.8241 | 15 7 | 1513.2792 | 8.9234 |
| 8 | 55 6 | 245.1316 | 15 7% | 1527.6601 | 9.0789 |
| 9 | 55 9% | 247.4500 | 15 8% | 1542.1084 | 9.1648 |
| 10 | 56 0% | 249.7781 | 15 9% | 1566.6171 | 9.2510 |
| 11 | 56 3% | 252.1184 | 15 10% | 1571.2018 | 9.3377 |
| 18 ft. | 56 6% | 254.4696 | 15 11% | 1585.8545 | 9.4248 |
| 1 | 56 9% | 256.8303 | 16 0% | 1600.5664 | 9.5122 |
| 2 | 57 0% | 259.2033 | 16 1% | 1615.3549 | 9.6000 |
| 3 | 57 4 | 261.5872 | 16 2% | 1630.2114 | 9.6884 |
| 4 | 57 7% | 263.9807 | 16 3% | 1645.1277 | 9.7252 |
| 5 | 57 10% | 266.3864 | 16 3% | 1660.1200 | 9.8661 |
| 6 | 58 1% | 268.8031 | 16 4% | 1675.1809 | 9.9556 |
| 7 | 58 4% | 271.2293 | 16 5% | 1690.3009 | 10.0451 |
| 8 | 58 7% | 273.6678 | 16 6% | 1705.4977 | 10.1358 |
| 9 | 58 10% | 276.1171 | 16 7% | 1720.7617 | 10.2264 |
| 10 | 59 2 | 278.5761 | 16 8% | 1736.0862 | 10.3176 |
| 11 | 59 5% | 281.0472 | 16 9% | 1751.4861 | 10.4091 |
| 19 ft. | 59 8% | 283.5294 | 16 10 | 1766.9552 | 10.5011 |
| 1 | 59 11% | 286.0210 | 16 11 | 1782.4828 | 10.5933 |
| 2 | 60 2% | 288.5249 | 16 11% | 1798.0871 | 10.6861 |
| 3 | 60 5% | 291.0397 | 17 0% | 1813.7594 | 10.7792 |
| 4 | 60 8% | 293.5641 | 17 1% | 1829.4914 | 10.8727 |
| 5 | 60 11% | 296.1107 | 17 2% | 1845.3005 | 10.9665 |
| 6 | 61 3% | 298.6483 | 17 3% | 1861.0762 | 11.0610 |
| 7 | 61 6% | 301.2054 | 17 4% | 1877.1120 | 11.1668 |
| 8 | 61 9% | 303.7747 | 17 5% | 1893.1239 | 11.2509 |
| 9 | 62 0% | 306.3550 | 17 6 | 1909.2043 | 11.3464 |
| 10 | 62 3% | 308.9448 | 17 7 | 1925.3439 | 11.4424 |
| 11 | 62 6% | 311.5469 | 17 7% | 1941.5602 | 11.5384 |
| 20 ft. | 62 9% | 314.1600 | 17 8% | 1957.8451 | 11.6355 |
| 1 | 63 1% | 316.7824 | 17 9% | 1974.1879 | 11.7326 |
| 2 | 63 4% | 319.4173 | 17 10% | 1990.6086 | 11.8302 |
| 3 | 63 7% | 322.0630 | 17 11% | 2007.0966 | 11.9282 |
| 4 | 63 11% | 324.7182 | 18 0% | 2023.6438 | 12.0266 |
| 5 | 64 1% | 327.3858 | 18 1% | 2040.2683 | 12.1254 |
| 6 | 64 4% | 330.0643 | 18 2 | 2056.9607 | 12.2246 |
| 7 | 64 7% | 332.7522 | 18 2% | 2073.7117 | 12.3241 |
| 8 | 64 11 | 335.4525 | 18 3% | 2090.5399 | 12.4241 |
| 9 | 65 2% | 338.1637 | 18 4% | 2107.4361 | 12.5245 |
| 10 | 65 5% | 340.8844 | 18 5% | 2124.3915 | 12.6253 |
| 11 | 65 8% | 343.6174 | 18 6% | 2141.4236 | 12.7265 |

| Dia. in feet & inches. | Circum. in feet and inches. | Area in feet. | Side of = square in ft. and in. | Gallons at 1 foot in depth. | Cubicyards at 1 foot in depth. |
|------------------------------|-----------------------------------|---------------|---------------------------------------|--------------------------------|--------------------------------------|
| 21 ft. | 65 11 $\frac{1}{2}$ | 346.3614 | 18 7 $\frac{1}{2}$ | 2158.5242 | 12.8282 |
| 1 | 66 2 $\frac{1}{2}$ | 349.1147 | 18 8 $\frac{1}{2}$ | 2175.6828 | 12.9301 |
| 2 | 66 5 $\frac{1}{2}$ | 351.8804 | 18 9 $\frac{1}{2}$ | 2192.9186 | 13.0326 |
| 3 | 66 9 | 354.6571 | 18 10 | 2210.2110 | 13.1354 |
| 4 | 66 0 $\frac{1}{2}$ | 357.4432 | 18 10 $\frac{1}{2}$ | 2227.5860 | 13.2386 |
| 5 | 67 3 $\frac{1}{2}$ | 360.2417 | 18 11 $\frac{1}{2}$ | 2245.0362 | 13.3422 |
| 6 | 67 6 $\frac{1}{2}$ | 363.0511 | 19 0 $\frac{1}{2}$ | 2262.5344 | 13.4463 |
| 7 | 67 9 $\frac{1}{2}$ | 365.8698 | 19 1 $\frac{1}{2}$ | 2280.1004 | 13.5507 |
| 8 | 68 0 $\frac{1}{2}$ | 368.7011 | 19 2 $\frac{1}{2}$ | 2297.7452 | 13.6555 |
| 9 | 68 3 $\frac{1}{2}$ | 371.5432 | 19 3 $\frac{1}{2}$ | 2315.4572 | 13.7608 |
| 10 | 68 7 | 374.3947 | 19 4 $\frac{1}{2}$ | 2333.2277 | 13.8664 |
| 11 | 68 10 $\frac{1}{2}$ | 377.2587 | 19 5 $\frac{1}{2}$ | 2351.0762 | 13.9725 |
| 22 ft. | 69 1 $\frac{1}{2}$ | 380.1336 | 19 5 $\frac{1}{2}$ | 2368.9925 | 14.0800 |
| 1 | 69 4 $\frac{1}{2}$ | 383.0177 | 19 6 $\frac{1}{2}$ | 2386.9669 | 14.1858 |
| 2 | 69 7 $\frac{1}{2}$ | 385.9144 | 19 7 $\frac{1}{2}$ | 2405.0185 | 14.2931 |
| 3 | 69 10 $\frac{1}{2}$ | 388.8220 | 19 8 $\frac{1}{2}$ | 2423.1387 | 14.4008 |
| 4 | 70 1 $\frac{1}{2}$ | 391.7389 | 19 9 $\frac{1}{2}$ | 2441.3168 | 14.5088 |
| 5 | 70 5 | 394.6683 | 19 10 $\frac{1}{2}$ | 2458.5728 | 14.6173 |
| 6 | 70 8 $\frac{1}{2}$ | 397.6087 | 19 11 $\frac{1}{2}$ | 2477.9074 | 14.7262 |
| 7 | 70 11 $\frac{1}{2}$ | 400.5583 | 20 0 $\frac{1}{2}$ | 2496.2793 | 14.8354 |
| 8 | 71 2 $\frac{1}{2}$ | 403.5204 | 20 1 $\frac{1}{2}$ | 2514.7391 | 14.9452 |
| 9 | 71 5 $\frac{1}{2}$ | 406.4935 | 20 2 | 2533.2674 | 15.0558 |
| 10 | 71 8 $\frac{1}{2}$ | 409.4759 | 20 2 $\frac{1}{2}$ | 2551.8538 | 15.1657 |
| 11 | 71 11 $\frac{1}{2}$ | 412.4707 | 20 3 $\frac{1}{2}$ | 2570.5174 | 15.2766 |
| 23 ft. | 72 3 | 415.4766 | 20 4 $\frac{1}{2}$ | 2589.2501 | 15.3880 |
| 1 | 72 6 $\frac{1}{2}$ | 418.4915 | 20 5 $\frac{1}{2}$ | 2607.9390 | 15.4996 |
| 2 | 72 9 $\frac{1}{2}$ | 421.5192 | 20 6 $\frac{1}{2}$ | 2626.9076 | 15.6118 |
| 3 | 73 0 $\frac{1}{2}$ | 424.5577 | 20 7 $\frac{1}{2}$ | 2645.8435 | 15.7243 |
| 4 | 73 3 $\frac{1}{2}$ | 427.6055 | 20 8 $\frac{1}{2}$ | 2664.8374 | 15.8372 |
| 5 | 73 6 $\frac{1}{2}$ | 430.6658 | 20 9 $\frac{1}{2}$ | 2683.9092 | 15.9505 |
| 6 | 73 9 $\frac{1}{2}$ | 433.7371 | 20 10 | 2703.0496 | 16.0643 |
| 7 | 74 1 | 436.8175 | 20 10 $\frac{1}{2}$ | 2722.2466 | 16.1784 |
| 8 | 74 4 $\frac{1}{2}$ | 439.9106 | 20 11 $\frac{1}{2}$ | 2741.5228 | 16.2929 |
| 9 | 74 7 $\frac{1}{2}$ | 443.0146 | 21 0 $\frac{1}{2}$ | 2760.8669 | 16.4079 |
| 10 | 74 10 $\frac{1}{2}$ | 446.1278 | 21 1 $\frac{1}{2}$ | 2780.2684 | 16.5232 |
| 11 | 75 1 $\frac{1}{2}$ | 449.2536 | 21 2 $\frac{1}{2}$ | 2799.7484 | 16.6390 |
| 24 ft. | 75 4 $\frac{1}{2}$ | 452.3904 | 21 3 $\frac{1}{2}$ | 2819.2969 | 16.7556 |
| 1 | 75 7 $\frac{1}{2}$ | 455.5362 | 21 4 $\frac{1}{2}$ | 2838.9015 | 16.8717 |
| 2 | 75 11 | 458.6948 | 21 5 | 2858.5859 | 16.9886 |
| 3 | 76 2 $\frac{1}{2}$ | 461.8642 | 21 6 | 2878.3376 | 17.1060 |
| 4 | 76 5 $\frac{1}{2}$ | 465.0428 | 21 6 $\frac{1}{2}$ | 2898.1467 | 17.2608 |
| 5 | 76 8 $\frac{1}{2}$ | 468.2341 | 21 7 $\frac{1}{2}$ | 2918.0349 | 17.3420 |
| 6 | 76 11 $\frac{1}{2}$ | 471.4363 | 21 8 $\frac{1}{2}$ | 2937.9941 | 17.4606 |
| 7 | 77 2 $\frac{1}{2}$ | 474.6476 | 21 9 $\frac{1}{2}$ | 2958.0038 | 17.5795 |
| 8 | 77 5 $\frac{1}{2}$ | 477.8716 | 21 10 $\frac{1}{2}$ | 2978.0958 | 17.6989 |
| 9 | 77 9 | 481.1065 | 21 11 $\frac{1}{2}$ | 2998.2557 | 17.8187 |
| 10 | 78 0 $\frac{1}{2}$ | 484.3506 | 22 0 $\frac{1}{2}$ | 3018.4729 | 17.9389 |
| 11 | 78 3 $\frac{1}{2}$ | 487.6073 | 22 1 | 3038.8686 | 18.3019 |

| Dia. in feet & inches. | Circum. in feet and inches. | Area in feet. | Side of = square in ft. and in. | Gallons at 1 foot in depth. | Cubic yards at 1 foot in depth. |
|------------------------|-----------------------------|---------------|---------------------------------|-----------------------------|---------------------------------|
| 25 ft. | 78 6% | 490.8750 | 22 1% | 3059.1330 | 18.1805 |
| 1 | 78 9% | 494.1516 | 22 2% | 3079.5527 | 18.2385 |
| 2 | 79 0% | 497.4411 | 22 3% | 3100.0529 | 18.4237 |
| 3 | 79 3% | 500.7415 | 22 4% | 3120.6210 | 18.6687 |
| 4 | 79 7% | 504.0510 | 22 6% | 3141.2458 | 18.7196 |
| 5 | 79 11% | 507.3732 | 22 6% | 3161.9497 | 18.7916 |
| 6 | 80 1% | 510.7063 | 22 7% | 3182.7214 | 18.9150 |
| 7 | 80 4% | 514.0484 | 22 8% | 3203.5496 | 19.0388 |
| 8 | 80 7% | 517.4034 | 22 9 | 3224.4579 | 19.1630 |
| 9 | 80 10% | 520.7692 | 22 9% | 3245.4336 | 19.2877 |
| 10 | 81 1% | 524.1441 | 22 10% | 3266.4860 | 19.4127 |
| 11 | 81 5 | 527.5318 | 22 11% | 3287.6381 | 19.5382 |
| 26 ft. | 81 8% | 530.9304 | 23 0% | 3308.7582 | 19.6640 |
| 1 | 81 11% | 534.3379 | 23 1% | 3329.9937 | 19.7902 |
| 2 | 82 2% | 537.7583 | 23 2% | 3351.3097 | 19.9169 |
| 3 | 82 5% | 541.1896 | 23 3% | 3372.6935 | 20.0440 |
| 4 | 82 8% | 544.6299 | 23 4% | 3394.1535 | 20.1714 |
| 5 | 82 11% | 548.0830 | 23 5 | 3415.6532 | 20.2993 |
| 6 | 83 3 | 551.5471 | 23 5% | 3437.2415 | 20.4276 |
| 7 | 83 6% | 555.0201 | 23 6% | 3458.8852 | 20.5562 |
| 8 | 83 9% | 558.5059 | 23 7% | 3480.6087 | 20.6854 |
| 9 | 84 0% | 562.0027 | 23 8% | 3502.3008 | 20.8149 |
| 10 | 84 3% | 565.5084 | 23 9% | 3524.2483 | 20.9447 |
| 11 | 84 6% | 569.0270 | 23 10% | 3546.1762 | 21.0750 |
| 27 ft. | 84 9% | 572.5566 | 23 11% | 3568.1727 | 21.2058 |
| 1 | 85 1 | 576.0949 | 24 0% | 3590.2234 | 21.3368 |
| 2 | 85 4% | 579.6463 | 24 1 | 3612.3557 | 21.4683 |
| 3 | 85 8% | 583.2085 | 24 1% | 3634.5553 | 21.6003 |
| 4 | 85 11% | 586.7796 | 24 2% | 3656.8104 | 21.7325 |
| 5 | 86 1% | 590.3637 | 24 3% | 3679.1465 | 21.8653 |
| 6 | 86 4% | 593.9587 | 24 4% | 3701.5506 | 21.9984 |
| 7 | 86 7% | 597.5625 | 24 5% | 3724.0094 | 22.1319 |
| 8 | 86 11 | 601.1793 | 24 6% | 3746.5493 | 22.2669 |
| 9 | 87 2% | 604.8070 | 24 7% | 3769.1572 | 22.4002 |
| 10 | 87 5% | 608.4436 | 24 8% | 3791.8205 | 22.5349 |
| 11 | 87 8% | 612.0931 | 24 9 | 3814.5641 | 22.6701 |
| 28 ft. | 87 11% | 615.7536 | 24 9% | 3837.3764 | 22.8056 |
| 1 | 88 2% | 619.4228 | 24 10% | 3860.2428 | 22.9415 |
| 2 | 88 5% | 623.1050 | 24 11% | 3883.1903 | 23.0779 |
| 3 | 88 9 | 626.7982 | 25 0% | 3905.4063 | 23.2147 |
| 4 | 89 0% | 630.5002 | 25 1% | 3929.2772 | 23.3515 |
| 5 | 89 3% | 634.2152 | 25 2% | 3952.4291 | 23.4894 |
| 6 | 89 6% | 637.9411 | 25 3% | 3975.6489 | 23.6274 |
| 7 | 89 9% | 641.6758 | 25 4 | 3998.9235 | 23.7657 |
| 8 | 90 0% | 645.4235 | 25 4% | 4022.4662 | 23.9045 |
| 9 | 90 3% | 649.1821 | 25 5% | 4045.7028 | 24.0437 |
| 10 | 90 6% | 652.9495 | 25 6% | 4069.1813 | 24.1833 |
| 11 | 90 11% | 656.7300 | 25 7% | 4092.8413 | 24.3249 |

| Dia. in feet & inches. | Circum. in feet and inches. | Area in feet. | Side of = square in ft. and in. | Gallens at 1 foot in depth. | Cubicyards at 1 foot in depth. |
|------------------------|-----------------------------|---------------|---------------------------------|-----------------------------|--------------------------------|
| 29 ft. | 91 1 1/4 | 660.5214 | 25 8 1/2 | 4116.3693 | 24.4637 |
| 1 | 91 4 1/2 | 664.3214 | 25 9 1/2 | 4140.0509 | 24.6044 |
| 2 | 91 7 1/2 | 668.1346 | 25 10 1/2 | 4163.8148 | 24.7457 |
| 3 | 91 10 1/2 | 671.9587 | 25 11 1/2 | 4187.6466 | 24.8873 |
| 4 | 92 1 1/4 | 675.7915 | 26 0 | 4211.5326 | 25.0293 |
| 5 | 92 4 1/2 | 679.6375 | 26 0 1/2 | 4234.4839 | 25.1717 |
| 6 | 92 8 1/2 | 683.4943 | 26 1 1/2 | 4259.5364 | 25.2405 |
| 7 | 92 11 1/2 | 687.3598 | 26 2 1/2 | 4283.6263 | 25.4577 |
| 8 | 93 2 1/4 | 691.2385 | 26 3 1/2 | 4308.7983 | 25.6014 |
| 9 | 93 5 1/2 | 695.1280 | 26 4 1/2 | 4332.0376 | 25.7454 |
| 10 | 93 8 1/2 | 699.0263 | 26 5 1/2 | 4356.3319 | 25.8898 |
| 11 | 93 11 1/2 | 702.9377 | 26 6 1/2 | 4380.7077 | 26.0347 |
| 30 ft. | 94 2 1/4 | 706.8600 | 26 7 1/2 | 4405.1515 | 26.1800 |
| 1 | 94 6 | 710.7909 | 26 8 | 4429.6488 | 26.3255 |
| 2 | 94 9 1/4 | 714.7350 | 26 8 1/2 | 4454.2285 | 26.4716 |
| 3 | 95 0 1/2 | 718.6900 | 26 9 1/2 | 4478.8760 | 26.6181 |
| 4 | 95 3 1/2 | 722.6537 | 26 10 1/2 | 4503.5779 | 26.7649 |
| 5 | 95 6 1/2 | 726.6305 | 26 11 1/2 | 4528.3612 | 26.9122 |
| 6 | 95 9 1/2 | 730.6183 | 27 0 1/2 | 4553.2132 | 27.0599 |
| 7 | 96 0 1/2 | 734.6147 | 27 1 1/2 | 4578.1188 | 27.2079 |
| 8 | 96 4 | 738.6242 | 27 2 1/2 | 4603.1060 | 27.3934 |
| 9 | 96 7 1/4 | 742.6447 | 27 3 1/2 | 4628.1617 | 27.5153 |
| 10 | 96 10 1/2 | 746.6738 | 27 4 1/2 | 4653.2711 | 27.6545 |
| 11 | 97 1 1/2 | 750.7161 | 27 5 1/2 | 4678.4627 | 27.8043 |
| 31 ft. | 97 4 1/2 | 754.7694 | 27 6 1/2 | 4703.7229 | 27.9544 |
| 1 | 97 7 1/2 | 758.8311 | 27 7 1/2 | 4729.0354 | 28.1048 |
| 2 | 97 10 1/2 | 762.9062 | 27 8 1/2 | 4754.4314 | 28.2557 |
| 3 | 98 2 | 766.9921 | 27 9 1/2 | 4779.8947 | 28.4070 |
| 4 | 98 5 1/2 | 771.0866 | 27 10 1/2 | 4805.4116 | 28.5587 |
| 5 | 98 8 1/2 | 775.1944 | 27 11 1/2 | 4831.0115 | 28.7109 |
| 6 | 98 11 1/2 | 779.3131 | 28 0 | 4856.6792 | 28.8634 |
| 7 | 99 2 1/4 | 783.4403 | 28 0 1/2 | 4882.3999 | 29.0163 |
| 8 | 99 5 1/2 | 787.5808 | 28 1 1/2 | 4908.2035 | 29.1696 |
| 9 | 99 8 1/2 | 791.7322 | 28 2 1/2 | 4934.0750 | 29.3234 |
| 10 | 100 0 | 795.8922 | 28 3 1/2 | 4960.0001 | 29.4774 |
| 11 | 100 3 1/4 | 800.0654 | 28 4 1/2 | 4986.0075 | 29.6320 |
| 32 ft. | 100 6 1/2 | 804.2496 | 28 5 1/2 | 5012.0835 | 29.7870 |
| 1 | 100 9 1/2 | 808.4422 | 28 6 1/2 | 5038.2117 | 29.9423 |
| 2 | 101 0 1/2 | 812.6481 | 28 7 1/2 | 5064.4229 | 30.0980 |
| 3 | 101 3 1/2 | 816.8650 | 28 8 1/2 | 5090.7026 | 30.2543 |
| 4 | 101 6 1/2 | 821.0904 | 28 9 1/2 | 5117.0358 | 30.4107 |
| 5 | 101 10 | 825.3291 | 28 10 1/2 | 5143.4509 | 30.5677 |
| 6 | 102 1 1/4 | 829.5787 | 28 11 1/2 | 5169.9344 | 30.7251 |
| 7 | 102 4 1/2 | 833.8368 | 29 0 1/2 | 5196.4709 | 30.8828 |
| 8 | 102 7 1/2 | 838.1082 | 29 1 1/2 | 5223.0903 | 31.0410 |
| 9 | 102 10 1/2 | 842.3905 | 29 2 1/2 | 5249.7775 | 31.1996 |
| 10 | 103 1 1/4 | 846.6813 | 29 3 1/2 | 5277.0178 | 31.3585 |
| 11 | 103 4 1/2 | 850.9855 | 29 4 1/2 | 5303.3416 | 31.5179 |

| Dia. in feet & inches. | Circum. in feet and inches. | Area in feet. | Side of = square in ft. and in. | Gallons at 1 foot in depth. | Cubicyards at 1 foot in depth. |
|------------------------------|-----------------------------------|---------------|---------------------------------------|--------------------------------|--------------------------------------|
| 33 ft. | 103 8 | 855.3006 | 29 2% | 5330.2333 | 31.6778 |
| 1 | 103 11% | 859.6240 | 29 3% | 5317.1767 | 31.8379 |
| 2 | 104 2% | 863.9609 | 29 4% | 5384.2043 | 31.9948 |
| 3 | 104 5% | 868.3087 | 29 5% | 5411.2998 | 32.1595 |
| 4 | 104 8% | 872.6649 | 29 6% | 5438.4476 | 32.3579 |
| 5 | 104 11% | 877.0346 | 29 7% | 5465.6796 | 32.4827 |
| 6 | 105 2% | 881.4151 | 29 8% | 5492.9789 | 32.6450 |
| 7 | 105 6 | 885.8040 | 29 9% | 5520.3305 | 32.8075 |
| 8 | 105 9% | 890.2064 | 29 10 ¹ / ₈ | 5547.7662 | 32.9706 |
| 9 | 106 0% | 894.6196 | 29 11 | 5575.2693 | 33.1340 |
| 10 | 106 3% | 899.0413 | 29 11% | 5602.8253 | 33.2978 |
| 11 | 106 6% | 903.4763 | 30 0% | 5630.4643 | 33.4613 |
| 34 ft. | 106 9% | 907.9224 | 30 1% | 5658.1723 | 33.6267 |
| 1 | 107 0% | 912.3767 | 30 2% | 5685.9315 | 33.7917 |
| 2 | 107 4 | 916.8445 | 30 3% | 5713.7749 | 33.9572 |
| 3 | 107 7% | 921.3232 | 30 4% | 5741.6861 | 34.1231 |
| 4 | 107 10% | 925.8103 | 30 5% | 5769.6497 | 34.2892 |
| 5 | 108 1% | 930.3108 | 30 6 ¹ / ₈ | 5797.6969 | 34.4559 |
| 6 | 108 4% | 934.8223 | 30 7 | 5825.8115 | 34.6230 |
| 7 | 108 7% | 939.3421 | 30 7% | 5853.9699 | 34.7904 |
| 8 | 108 10% | 943.8753 | 30 8% | 5882.2308 | 34.9583 |
| 9 | 109 2 | 948.4195 | 30 9% | 5910.5503 | 35.1266 |
| 10 | 109 5% | 952.9720 | 30 10% | 5938.9215 | 35.2952 |
| 11 | 109 8% | 957.5380 | 30 11% | 5967.3768 | 35.4643 |
| 35 ft. | 109 11% | 962.1150 | 31 0% | 5989.9006 | 35.6339 |
| 1 | 110 2% | 966.7001 | 31 1% | 6024.4750 | 35.8037 |
| 2 | 110 5% | 971.2989 | 31 2 ¹ / ₈ | 6053.1347 | 35.9740 |
| 3 | 110 8% | 975.9085 | 31 3 | 6081.8617 | 36.1447 |
| 4 | 111 0 | 980.5264 | 31 3% | 6110.6405 | 36.3158 |
| 5 | 111 3% | 985.1579 | 31 4% | 6139.5040 | 36.4873 |
| 6 | 111 6% | 989.8003 | 31 5% | 6168.4354 | 36.6592 |
| 7 | 111 9% | 994.4509 | 31 6% | 6197.4180 | 36.8315 |
| 8 | 112 0% | 999.1151 | 31 7% | 6226.4833 | 37.0042 |
| 9 | 112 3% | 1003.7902 | 31 8% | 6256.6205 | 37.1404 |
| 10 | 112 6% | 1008.4736 | 31 9 ¹ / ₈ | 6284.8074 | 37.3509 |
| 11 | 112 10 | 1013.1705 | 31 10 ¹ / ₈ | 6314.0785 | 37.5248 |
| 36 ft. | 113 1% | 1017.8784 | 31 10% | 6343.4181 | 37.6992 |
| 1 | 113 4% | 1022.5944 | 31 11% | 6372.8083 | 37.8738 |
| 2 | 113 7% | 1027.3240 | 32 0% | 6403.2831 | 38.0490 |
| 3 | 113 10% | 1032.0646 | 32 1% | 6431.8265 | 38.2246 |
| 4 | 114 1% | 1036.8134 | 32 2% | 6461.4211 | 38.4005 |
| 5 | 114 4% | 1041.5758 | 32 3% | 6491.1003 | 38.5761 |
| 6 | 114 8 | 1046.3491 | 32 4% | 6520.8475 | 38.7537 |
| 7 | 114 11% | 1051.1306 | 32 5 ¹ / ₈ | 6550.6458 | 38.9307 |
| 8 | 115 2% | 1055.9257 | 32 6 | 6580.5289 | 39.1083 |
| 9 | 115 5% | 1060.7317 | 32 6% | 6610.4799 | 39.2863 |
| 10 | 115 9% | 1065.5459 | 32 7% | 6640.4820 | 39.4646 |
| 11 | 115 11% | 1070.3738 | 32 8% | 6670.5695 | 39.6435 |

| Dia. in feet & inches. | Circum. in feet and inches. | Area in feet. | Side of = square in ft. and in. | Gallons at 1 foot in depth. | Cubicyards at 1 foot in depth. |
|------------------------------|-----------------------------------|---------------|---------------------------------------|--------------------------------|--------------------------------------|
| 37 ft. | 116 2% | 1075.2126 | 32 9% | 6700.7249 | 39.8227 |
| 1 | 116 6 | 1080.0594 | 32 10% | 6730.9301 | 40.0220 |
| 2 | 116 9 ¹ / ₈ | 1084.9201 | 32 11% | 6762.2220 | 40.1822 |
| 3 | 117 0% | 1089.7915 | 33 0% | 6791.5806 | 40.3626 |
| 4 | 117 3% | 1094.6711 | 33 1 ¹ / ₈ | 6821.9902 | 40.5434 |
| 5 | 117 6% | 1099.5644 | 33 2 | 6852.4853 | 40.7246 |
| 6 | 117 9% | 1104.4687 | 33 2% | 6883.0489 | 40.9062 |
| 7 | 118 0% | 1109.3810 | 33 3% | 6913.6623 | 41.0882 |
| 8 | 118 4 | 1114.3071 | 33 4% | 6944.3618 | 41.2706 |
| 9 | 118 7 ¹ / ₈ | 1119.2440 | 33 5% | 6975.1286 | 41.4535 |
| 10 | 118 10% | 1124.1891 | 33 6% | 7005.9464 | 41.6366 |
| 11 | 119 1% | 1129.1478 | 33 7% | 7036.8490 | 41.8203 |
| 38 ft. | 119 4% | 1134.1176 | 33 8 ¹ / ₈ | 7067.8208 | 42.0043 |
| 1 | 119 7% | 1139.0953 | 33 9 ¹ / ₈ | 7098.8419 | 42.1887 |
| 2 | 119 10% | 1144.0868 | 33 10 | 7129.9489 | 42.3736 |
| 3 | 120 2 | 1149.0892 | 33 10% | 7161.1238 | 42.5588 |
| 4 | 120 5 ¹ / ₈ | 1154.0997 | 33 11% | 7192.3493 | 42.7444 |
| 5 | 120 8% | 1159.1239 | 34 0% | 7223.6601 | 42.9305 |
| 6 | 120 11% | 1164.1591 | 34 1% | 7255.0395 | 43.1169 |
| 7 | 121 2% | 1169.2023 | 34 2% | 7286.4687 | 43.3034 |
| 8 | 121 5% | 1174.2592 | 34 3% | 7317.9833 | 43.4911 |
| 9 | 121 8% | 1179.3271 | 34 4% | 7349.5664 | 43.6817 |
| 10 | 121 11% | 1184.4030 | 34 5 ¹ / ₈ | 7381.1994 | 43.8668 |
| 11 | 122 8 ¹ / ₈ | 1189.4927 | 34 6 | 7412.9185 | 44.0553 |
| 39 ft. | 122 6% | 1194.5934 | 34 6% | 7444.7054 | 44.2442 |
| 1 | 122 9% | 1199.7195 | 34 7% | 7476.6519 | 44.4340 |
| 2 | 123 0% | 1204.8244 | 34 8% | 7478.4626 | 44.6231 |
| 3 | 123 3% | 1209.9577 | 34 9 ¹ / ₈ | 7540.4563 | 44.8123 |
| 4 | 123 6% | 1215.0990 | 34 10% | 7572.4969 | 45.0036 |
| 5 | 123 9% | 1220.2542 | 34 11% | 7604.6239 | 45.1946 |
| 6 | 124 1 ¹ / ₈ | 1225.4203 | 35 0 ¹ / ₈ | 7636.8193 | 45.3859 |
| 7 | 124 4% | 1230.5943 | 35 1 ¹ / ₈ | 7669.0636 | 45.5775 |
| 8 | 124 7% | 1235.7822 | 35 2 | 7701.3946 | 45.7697 |
| 9 | 124 10% | 1240.9810 | 35 2% | 7733.7935 | 45.9622 |
| 10 | 125 1% | 1246.1878 | 35 3% | 7766.2423 | 46.1551 |
| 11 | 125 4% | 1251.4084 | 35 4% | 7798.7771 | 46.3484 |
| 40 ft. | 125 7% | 1256.6400 | 35 5% | 7831.3804 | 46.5422 |
| 1 | 125 11 | 1261.8794 | 35 6% | 7864.0324 | 46.7362 |
| 2 | 126 2% | 1267.1327 | 35 7% | 7896.7709 | 46.9308 |
| 3 | 126 5% | 1272.3970 | 35 8 ¹ / ₈ | 7929.5781 | 47.1257 |
| 4 | 126 8% | 1277.6692 | 35 9 | 7962.4344 | 47.3211 |
| 5 | 126 11% | 1282.9553 | 35 10 | 7995.3774 | 47.5168 |
| 6 | 127 2% | 1288.2523 | 35 10% | 8028.2883 | 47.7130 |
| 7 | 127 5% | 1293.5572 | 35 11% | 8061.4484 | 47.9095 |
| 8 | 127 9 | 1298.8760 | 36 0% | 8094.5952 | 48.1065 |
| 9 | 128 0% | 1304.2057 | 36 1 ¹ / ₈ | 8127.8099 | 48.3039 |
| 10 | 128 3% | 1309.5433 | 36 2% | 8161.0738 | 48.5016 |
| 11 | 128 6% | 1314.8949 | 36 3% | 8194.4250 | 48.6998 |

| Dia. in feet & inches. | Circum. in feet and inches. | Area in feet. | Side of square in ft. and in. | Gallons at 1 foot in depth. | Cubic yards at 1 foot in depth. |
|------------------------|-----------------------------|---------------|-------------------------------|-----------------------------|---------------------------------|
| 41 ft. | 128 9% | 1320.2574 | 36 4% | 8227.8441 | 48.8984 |
| 1 | 129 0% | 1325.6276 | 36 5 | 8261.3112 | 49.0973 |
| 2 | 129 3% | 1331.0119 | 36 5% | 8294.8661 | 49.2967 |
| 3 | 129 7 | 1336.4071 | 36 6% | 8328.4890 | 49.4965 |
| 4 | 129 10% | 1341.8101 | 36 7% | 8362.1605 | 49.6967 |
| 5 | 130 1% | 1347.2271 | 36 8% | 8395.9192 | 49.8973 |
| 6 | 130 4% | 1352.6551 | 36 9% | 8429.7465 | 50.0983 |
| 7 | 130 7% | 1358.0908 | 36 10% | 8463.6218 | 50.2997 |
| 8 | 130 10% | 1363.5406 | 36 11% | 8497.5850 | 50.5015 |
| 9 | 131 1% | 1369.0012 | 37 0% | 8531.6154 | 50.7037 |
| 10 | 131 5 | 1374.4697 | 37 1 | 8565.6951 | 50.9063 |
| 11 | 131 8% | 1379.9521 | 37 1% | 8599.8614 | 51.1093 |
| 42 ft. | 131 11% | 1385.4456 | 37 2% | 8634.0969 | 51.3128 |
| 1 | 132 2% | 1390.2467 | 37 3% | 8664.0174 | 51.4906 |
| 2 | 132 5% | 1396.4619 | 37 4% | 8702.7505 | 51.7208 |
| 3 | 132 8% | 1401.9880 | 37 5% | 8737.1892 | 51.9257 |
| 4 | 132 11% | 1407.5219 | 37 6% | 8771.6764 | 52.1304 |
| 5 | 133 3 | 1413.0698 | 37 7% | 8806.2509 | 52.3355 |
| 6 | 133 6% | 1418.6287 | 37 8% | 8840.8940 | 52.5418 |
| 7 | 133 9% | 1424.1952 | 37 9 | 8875.5844 | 52.7479 |
| 8 | 134 0% | 1429.7759 | 37 9% | 8910.3634 | 52.9546 |
| 9 | 134 3% | 1435.3675 | 37 10% | 8945.2102 | 53.1618 |
| 10 | 134 6% | 1440.9668 | 37 11% | 8980.1050 | 53.3691 |
| 11 | 134 9% | 1446.5802 | 38 0% | 9015.0878 | 53.5770 |
| 43 ft. | 135 1 | 1452.2046 | 38 1% | 9050.1390 | 53.7858 |
| 1 | 135 4% | 1457.8365 | 38 2% | 9085.2370 | 53.9939 |
| 2 | 135 7% | 1463.4827 | 38 3% | 9120.3741 | 54.2030 |
| 3 | 135 10% | 1469.1397 | 38 4% | 9155.6786 | 54.4126 |
| 4 | 136 1% | 1474.8044 | 38 5 | 9190.9810 | 54.6224 |
| 5 | 136 4% | 1480.4833 | 38 5% | 9226.3719 | 54.8323 |
| 6 | 136 7% | 1486.1731 | 38 6% | 9261.7307 | 55.0434 |
| 7 | 136 11 | 1491.8705 | 38 7% | 9297.3369 | 55.2544 |
| 8 | 137 2% | 1497.5821 | 38 8% | 9332.9316 | 55.4663 |
| 9 | 137 5% | 1503.3046 | 38 9% | 9368.5942 | 55.6779 |
| 10 | 137 8% | 1509.0348 | 38 10% | 9404.3048 | 55.8902 |
| 11 | 137 11% | 1514.7791 | 38 11% | 9440.1033 | 56.1029 |
| 44 ft. | 138 2% | 1520.5344 | 38 11% | 9475.9703 | 56.3161 |
| 1 | 138 5% | 1526.2971 | 39 1 | 9511.8835 | 56.5295 |
| 2 | 138 9 | 1532.0742 | 39 1% | 9547.8864 | 56.7435 |
| 3 | 139 0% | 1537.8622 | 39 2% | 9583.9572 | 56.9578 |
| 4 | 139 3% | 1543.6578 | 39 3% | 9620.0754 | 57.1725 |
| 5 | 139 6% | 1549.4676 | 39 4% | 9656.2820 | 57.3877 |
| 6 | 139 9% | 1555.2883 | 39 5% | 9692.5566 | 57.6033 |
| 7 | 140 0% | 1561.1165 | 39 6% | 9728.8780 | 57.8191 |
| 8 | 140 3% | 1566.9591 | 39 7% | 9765.2891 | 58.0355 |
| 9 | 140 7% | 1572.8125 | 39 8 | 9801.7675 | 58.2523 |
| 10 | 140 10% | 1578.6735 | 39 8% | 9838.2932 | 58.4693 |
| 11 | 141 1% | 1584.5488 | 39 9% | 9874.9081 | 58.6869 |

| Dia. in feet & inches. | Circum. in feet and inches. | Area in feet. | Side of = square in ft. and in. | Gallons at 1 foot in depth. | Cubicyards at 1 foot in depth. |
|------------------------------|-----------------------------------|---------------|---------------------------------------|--------------------------------|--------------------------------------|
| 45 ft. | 141 4% | 1590.4350 | 39 10% | 9911.5909 | 58.9050 |
| 1 | 141 7% | 1596.3286 | 39 11% | 9948.3198 | 59.1233 |
| 2 | 141 10% | 1602.2366 | 40 0% | 9985.1364 | 59.3421 |
| 3 | 142 1% | 1608.1555 | 40 1% | 10022.025 | 59.5613 |
| 4 | 142 5 | 1614.0819 | 40 2% | 10058.958 | 59.7808 |
| 5 | 142 8% | 1620.0226 | 40 3% | 10095.980 | 60.0008 |
| 6 | 142 11% | 1625.9743 | 40 4 | 10133.071 | 60.2212 |
| 7 | 143 2% | 1631.9334 | 40 4% | 10170.208 | 60.4420 |
| 8 | 143 5% | 1637.9068 | 40 5% | 10207.435 | 60.6632 |
| 9 | 143 8% | 1643.8912 | 40 6% | 10244.729 | 60.8848 |
| 10 | 143 11% | 1649.8831 | 40 7% | 10277.070 | 61.1068 |
| 11 | 144 3 | 1655.8892 | 40 8% | 10319.501 | 61.3292 |
| 46 ft. | 144 6% | 1661.9064 | 40 9% | 10357.000 | 61.5521 |
| 1 | 144 9% | 1667.9308 | 40 10% | 10394.544 | 61.7752 |
| 2 | 145 0% | 1673.9698 | 40 11% | 10432.179 | 61.9989 |
| 3 | 145 3% | 1680.0196 | 41 0 | 10469.880 | 62.2229 |
| 4 | 145 6% | 1686.0769 | 41 0% | 10507.631 | 62.4473 |
| 5 | 145 9% | 1692.1485 | 41 1% | 10546.469 | 62.6722 |
| 6 | 146 1% | 1698.2311 | 41 2% | 10583.376 | 62.8974 |
| 7 | 146 4% | 1704.3210 | 41 3% | 10621.328 | 63.1230 |
| 8 | 146 7% | 1710.4254 | 41 4% | 10659.371 | 63.3491 |
| 9 | 146 10% | 1716.5407 | 41 5% | 10697.481 | 63.5756 |
| 10 | 147 1% | 1722.6634 | 41 6% | 10735.638 | 63.8021 |
| 11 | 147 4% | 1728.8005 | 41 7% | 10773.884 | 64.0296 |
| 47 ft. | 147 7% | 1734.9486 | 41 7% | 10812.199 | 64.2573 |
| 1 | 147 11 | 1741.1039 | 41 8% | 10850.559 | 64.4853 |
| 2 | 148 2% | 1747.2738 | 41 9% | 10889.010 | 64.7138 |
| 3 | 148 5% | 1753.4545 | 41 10% | 10927.528 | 64.9427 |
| 4 | 148 8% | 1759.6426 | 41 11% | 10966.092 | 65.1719 |
| 5 | 148 11% | 1765.8452 | 42 0% | 11004.747 | 65.4017 |
| 6 | 149 2% | 1772.0587 | 42 1% | 11043.469 | 65.6318 |
| 7 | 149 5% | 1778.2795 | 42 2% | 11082.237 | 65.8622 |
| 8 | 149 8% | 1784.5148 | 42 3% | 11121.096 | 66.0931 |
| 9 | 150 0% | 1790.7610 | 42 4 | 11160.022 | 66.3245 |
| 10 | 150 3% | 1797.0145 | 42 4% | 11197.994 | 66.5561 |
| 11 | 150 6% | 1803.2826 | 42 5% | 11238.057 | 66.7882 |
| 48 ft. | 150 9% | 1809.5616 | 42 6% | 11287.187 | 67.0208 |
| 1 | 151 0% | 1815.8477 | 42 7% | 11316.362 | 67.2536 |
| 2 | 151 3% | 1822.1485 | 42 8% | 11336.629 | 67.4870 |
| 3 | 151 6% | 1828.4602 | 42 9% | 11394.963 | 67.7209 |
| 4 | 151 10% | 1834.7791 | 42 10 ¹ / ₈ | 11434.343 | 67.9548 |
| 5 | 152 1% | 1841.1127 | 42 11 | 11473.814 | 68.1893 |
| 6 | 152 4% | 1847.4571 | 43 0 | 11513.352 | 68.4243 |
| 7 | 152 7% | 1853.8087 | 43 0% | 11552.935 | 68.6560 |
| 8 | 152 10% | 1860.1750 | 43 1% | 11592.610 | 68.8953 |
| 9 | 153 1% | 1866.5521 | 43 2% | 11632.352 | 69.1315 |
| 10 | 153 4% | 1872.9365 | 43 3% | 11672.140 | 69.3680 |
| 11 | 153 8% | 1879.3355 | 43 4% | 11712.018 | 69.6050 |

| Dia. in feet & inches. | Circum. in feet and inches. | Area in feet. | Side of = square in ft. and in. | Gallons at 1 foot in depth. | Cubicyards at 1 foot in depth. |
|------------------------------|-----------------------------------|---------------|---------------------------------------|--------------------------------|--------------------------------------|
| 49 ft. | 153 11 $\frac{1}{4}$ | 1885.7454 | 43 5 $\frac{1}{8}$ | 11750.964 | 69.8424 |
| 1 | 154 2 $\frac{1}{2}$ | 1892.1724 | 43 6 $\frac{1}{8}$ | 11792.018 | 70.0804 |
| 2 | 154 5 $\frac{1}{2}$ | 1898.5041 | 43 7 | 11831.477 | 70.3150 |
| 3 | 154 8 $\frac{1}{4}$ | 1905.0367 | 43 7 $\frac{1}{2}$ | 11872.188 | 70.5569 |
| 4 | 154 11 $\frac{1}{4}$ | 1911.4965 | 43 8 $\frac{1}{4}$ | 11912.446 | 70.7961 |
| 5 | 155 2 $\frac{1}{2}$ | 1917.9609 | 43 9 $\frac{1}{4}$ | 11952.732 | 71.0356 |
| 6 | 155 6 | 1924.4263 | 43 10 $\frac{1}{8}$ | 11993.824 | 71.2750 |
| 7 | 155 9 $\frac{1}{4}$ | 1930.9188 | 43 11 $\frac{1}{8}$ | 12033.485 | 71.5155 |
| 8 | 156 0 $\frac{1}{8}$ | 1937.3159 | 44 0 $\frac{1}{2}$ | 12073.352 | 71.7524 |
| 9 | 156 3 $\frac{1}{2}$ | 1943.9140 | 44 1 $\frac{1}{4}$ | 12114.472 | 71.9968 |
| 10 | 156 6 $\frac{1}{4}$ | 1950.4892 | 44 2 $\frac{1}{8}$ | 12155.137 | 72.2385 |
| 11 | 156 9 $\frac{1}{4}$ | 1956.9691 | 44 3 | 12195.831 | 72.4808 |
| 50 ft. | 157 0 $\frac{1}{2}$ | 1963.5000 | 44 3 $\frac{1}{4}$ | 12236.532 | 72.7222 |

T A B L E
 CONTAINING
THE SQUARE & CUBE ROOTS OF ALL NUMBERS
From 1 to 1000; and the
DIFFERENCE EXISTING BETWEEN EACH ROOT,
 BY WHICH
The process for obtaining the roots of numbers, consisting of
integers and decimals, is considerably facilitated.

RULE.—Multiply the difference between the root of the integer part of the given number, and the root of the next higher integer number, by the decimal part of the given number, and add the product to the root of the integer number given, the sum is the root required.

EXAMPLE 1.—Required the square root of 53.75.

Difference by table = $.0683 \times .75 = .051225$,
 and the root of 53 = 7.2801,—hence, $7.2801 + .051225 = 7.3313$, the root required.

EXAMPLE 2.—Required the cube root of the number 734.26.

Difference by table = $.0041 \times .26 = .001066$,
 and the root of 734 = 9.0205,—hence, $9.0205 + .001066 = 9.0215$, the root required.

| No. | Sqr. Rta. | Diff. | C. Rta. | Diff. | No. | Sqr. Rta. | Diff. | C. Rta. | Diff. |
|-----|-----------|-------|---------|-------|-----|-----------|-------|---------|-------|
| 1 | 1.0000 | | 1.0000 | | 45 | 6.7082 | .0741 | 3.5568 | .0262 |
| 2 | 1.4142 | .4142 | 1.2599 | .2599 | 46 | 6.7823 | .0733 | 3.5830 | .0258 |
| 3 | 1.7320 | .3178 | 1.4422 | .1823 | 47 | 6.8556 | .0726 | 3.6088 | .0254 |
| 4 | 2.0000 | .2680 | 1.5874 | .1452 | 48 | 6.9282 | .0718 | 3.6342 | .0251 |
| 5 | 2.2360 | .2360 | 1.7099 | .1225 | 49 | 7.0000 | .0710 | 3.6593 | .0247 |
| 6 | 2.4494 | .2134 | 1.8171 | .1072 | 50 | 7.0710 | .0704 | 3.6840 | .0244 |
| 7 | 2.6457 | .1963 | 1.9129 | .0950 | 51 | 7.1414 | .0697 | 3.7084 | .0241 |
| 8 | 2.8284 | .1827 | 2.0000 | .0871 | 52 | 7.2111 | .0690 | 3.7325 | .0237 |
| 9 | 3.0000 | .1716 | 2.0800 | .0800 | 53 | 7.2801 | .0683 | 3.7562 | .0236 |
| 10 | 3.1622 | .1622 | 2.1544 | .0744 | 54 | 7.3484 | .0677 | 3.7797 | .0232 |
| 11 | 3.3166 | .1544 | 2.2239 | .0685 | 55 | 7.4161 | .0672 | 3.8029 | .0229 |
| 12 | 3.4641 | .1475 | 2.2894 | .0619 | 56 | 7.4833 | .0665 | 3.8258 | .0227 |
| 13 | 3.6055 | .1414 | 2.3513 | .0588 | 57 | 7.5498 | .0659 | 3.8485 | .0223 |
| 14 | 3.7416 | .1361 | 2.4101 | .0551 | 58 | 7.6157 | .0654 | 3.8708 | .0221 |
| 15 | 3.8729 | .1313 | 2.4662 | .0514 | 59 | 7.6811 | .0648 | 3.8929 | .0219 |
| 16 | 4.0000 | .1271 | 2.5198 | .0477 | 60 | 7.7459 | .0643 | 3.9148 | .0216 |
| 17 | 4.1231 | .1231 | 2.5712 | .0445 | 61 | 7.8102 | .0638 | 3.9364 | .0214 |
| 18 | 4.2426 | .1195 | 2.6207 | .0418 | 62 | 7.8740 | .0632 | 3.9578 | .0212 |
| 19 | 4.3588 | .1162 | 2.6684 | .0396 | 63 | 7.9372 | .0628 | 3.9790 | .0210 |
| 20 | 4.4721 | .1133 | 2.7144 | .0384 | 64 | 8.0000 | .0622 | 4.0000 | .0207 |
| 21 | 4.5825 | .1104 | 2.7589 | .0365 | 65 | 8.0622 | .0618 | 4.0217 | .0205 |
| 22 | 4.6904 | .1079 | 2.8020 | .0358 | 66 | 8.1240 | .0613 | 4.0412 | .0203 |
| 23 | 4.7958 | .1054 | 2.8438 | .0349 | 67 | 8.1853 | .0609 | 4.0615 | .0201 |
| 24 | 4.8989 | .1031 | 2.8844 | .0341 | 68 | 8.2462 | .0604 | 4.0816 | .0199 |
| 25 | 5.0000 | .1011 | 2.9240 | .0332 | 69 | 8.3066 | .0600 | 4.1015 | .0197 |
| 26 | 5.0990 | .0990 | 2.9624 | .0325 | 70 | 8.3666 | .0595 | 4.1212 | .0196 |
| 27 | 5.1961 | .0971 | 3.0000 | .0317 | 71 | 8.4261 | .0591 | 4.1408 | .0193 |
| 28 | 5.2915 | .0954 | 3.0365 | .0310 | 72 | 8.4852 | .0588 | 4.1601 | .0192 |
| 29 | 5.3851 | .0936 | 3.0723 | .0303 | 73 | 8.5440 | .0583 | 4.1793 | .0190 |
| 30 | 5.4772 | .0921 | 3.1072 | .0297 | 74 | 8.6023 | .0579 | 4.1983 | .0188 |
| 31 | 5.5677 | .0905 | 3.1413 | .0291 | 75 | 8.6602 | .0565 | 4.2171 | .0187 |
| 32 | 5.6568 | .0891 | 3.1748 | .0285 | 76 | 8.7177 | .0572 | 4.2358 | .0185 |
| 33 | 5.7445 | .0877 | 3.2075 | .0279 | 77 | 8.7749 | .0568 | 4.2543 | .0183 |
| 34 | 5.8309 | .0864 | 3.2396 | .0273 | 78 | 8.8317 | .0564 | 4.2726 | .0182 |
| 35 | 5.9160 | .0851 | 3.2710 | .0267 | 79 | 8.8881 | .0561 | 4.2908 | .0180 |
| 36 | 6.0000 | .0840 | 3.3019 | .0261 | 80 | 8.9442 | .0558 | 4.3088 | .0179 |
| 37 | 6.0827 | .0827 | 3.3322 | .0255 | 81 | 9.0000 | .0553 | 4.3267 | .0177 |
| 38 | 6.1644 | .0817 | 3.3619 | .0249 | 82 | 9.0553 | .0551 | 4.3444 | .0176 |
| 39 | 6.2449 | .0805 | 3.3912 | .0243 | 83 | 9.1104 | .0547 | 4.3620 | .0175 |
| 40 | 6.3245 | .0796 | 3.4199 | .0237 | 84 | 9.1651 | .0544 | 4.3795 | .0173 |
| 41 | 6.4031 | .0786 | 3.4482 | .0231 | 85 | 9.2195 | .0541 | 4.3968 | .0172 |
| 42 | 6.4807 | .0776 | 3.4760 | .0225 | 86 | 9.2736 | .0537 | 4.4140 | .0170 |
| 43 | 6.5574 | .0767 | 3.5033 | .0219 | 87 | 9.3273 | .0535 | 4.4310 | .0169 |
| 44 | 6.6332 | .0758 | 3.5303 | .0213 | 88 | 9.3808 | .0531 | 4.4479 | .0168 |
| 45 | 6.7082 | .0750 | 3.5568 | .0207 | 89 | 9.4339 | | 4.4647 | |

| No. | Sqr. Rts. | Diff. | C. Rts. | Diff. | No. | Sqr. Rts. | Diff. | C. Rts. | Diff. |
|-----|-----------|-------|---------|-------|-----|-----------|-------|---------|-------|
| 89 | 9.4339 | .0529 | 4.4647 | .0167 | 137 | 11.7046 | .0427 | 5.1551 | .0125 |
| 90 | 9.4868 | .0525 | 4.4814 | .0165 | 138 | 11.7473 | .0425 | 5.1676 | .0125 |
| 91 | 9.5393 | .0523 | 4.4979 | .0164 | 139 | 11.7898 | .0423 | 5.1801 | .0123 |
| 92 | 9.5916 | .0520 | 4.5143 | .0163 | 140 | 11.8321 | .0422 | 5.1924 | .0124 |
| 93 | 9.6436 | .0517 | 4.5306 | .0162 | 141 | 11.8743 | .0420 | 5.2048 | .0123 |
| 94 | 9.6953 | .0514 | 4.5468 | .0161 | 142 | 11.9163 | .0419 | 5.2171 | .0122 |
| 95 | 9.7467 | .0512 | 4.5629 | .0159 | 143 | 11.9582 | .0418 | 5.2293 | .0121 |
| 96 | 9.7979 | .0509 | 4.5788 | .0157 | 144 | 12.0000 | .0415 | 5.2414 | .0121 |
| 97 | 9.8488 | .0506 | 4.5947 | .0157 | 145 | 12.0415 | .0414 | 5.2535 | .0121 |
| 98 | 9.8994 | .0504 | 4.6104 | .0156 | 146 | 12.0830 | .0413 | 5.2656 | .0120 |
| 99 | 9.9498 | .0502 | 4.6260 | .0155 | 147 | 12.1243 | .0412 | 5.2776 | .0119 |
| 100 | 10.0000 | .0498 | 4.6415 | .0155 | 148 | 12.1655 | .0410 | 5.2895 | .0119 |
| 101 | 10.0498 | .0497 | 4.6570 | .0153 | 149 | 12.2065 | .0409 | 5.3014 | .0118 |
| 102 | 10.0995 | .0493 | 4.6723 | .0153 | 150 | 12.2474 | .0408 | 5.3132 | .0118 |
| 103 | 10.1488 | .0492 | 4.6875 | .0151 | 151 | 12.2882 | .0406 | 5.3250 | .0118 |
| 104 | 10.1980 | .0489 | 4.7026 | .0150 | 152 | 12.3288 | .0405 | 5.3368 | .0116 |
| 105 | 10.2469 | .0487 | 4.7176 | .0150 | 153 | 12.3693 | .0403 | 5.3484 | .0117 |
| 106 | 10.2956 | .0484 | 4.7326 | .0148 | 154 | 12.4096 | .0402 | 5.3601 | .0115 |
| 107 | 10.3440 | .0483 | 4.7474 | .0148 | 155 | 12.4498 | .0401 | 5.3716 | .0116 |
| 108 | 10.3923 | .0480 | 4.7622 | .0146 | 156 | 12.4899 | .0400 | 5.3832 | .0114 |
| 109 | 10.4403 | .0477 | 4.7768 | .0146 | 157 | 12.5299 | .0399 | 5.3946 | .0115 |
| 110 | 10.4880 | .0476 | 4.7914 | .0144 | 158 | 12.5698 | .0397 | 5.4061 | .0115 |
| 111 | 10.5356 | .0474 | 4.8058 | .0144 | 159 | 12.6095 | .0396 | 5.4175 | .0114 |
| 112 | 10.5830 | .0471 | 4.8202 | .0143 | 160 | 12.6491 | .0394 | 5.4288 | .0113 |
| 113 | 10.6301 | .0469 | 4.8345 | .0143 | 161 | 12.6885 | .0394 | 5.4401 | .0112 |
| 114 | 10.6770 | .0468 | 4.8488 | .0141 | 162 | 12.7279 | .0392 | 5.4513 | .0112 |
| 115 | 10.7238 | .0465 | 4.8629 | .0140 | 163 | 12.7671 | .0391 | 5.4625 | .0112 |
| 116 | 10.7703 | .0463 | 4.8769 | .0140 | 164 | 12.8062 | .0390 | 5.4737 | .0111 |
| 117 | 10.8166 | .0461 | 4.8909 | .0139 | 165 | 12.8452 | .0389 | 5.4848 | .0110 |
| 118 | 10.8627 | .0460 | 4.9048 | .0138 | 166 | 12.8840 | .0388 | 5.4958 | .0110 |
| 119 | 10.9087 | .0467 | 4.9186 | .0138 | 167 | 12.9228 | .0387 | 5.5068 | .0110 |
| 120 | 10.9544 | .0466 | 4.9324 | .0136 | 168 | 12.9614 | .0386 | 5.5178 | .0109 |
| 121 | 11.0000 | .0456 | 4.9460 | .0136 | 169 | 13.0000 | .0384 | 5.5287 | .0109 |
| 122 | 11.0453 | .0452 | 4.9596 | .0135 | 170 | 13.0384 | .0382 | 5.5396 | .0108 |
| 123 | 11.0905 | .0450 | 4.9731 | .0135 | 171 | 13.0766 | .0382 | 5.5504 | .0108 |
| 124 | 11.1355 | .0448 | 4.9866 | .0134 | 172 | 13.1148 | .0381 | 5.5612 | .0108 |
| 125 | 11.1803 | .0446 | 5.0000 | .0132 | 173 | 13.1529 | .0380 | 5.5720 | .0107 |
| 126 | 11.2249 | .0445 | 5.0132 | .0133 | 174 | 13.1909 | .0378 | 5.5827 | .0107 |
| 127 | 11.2694 | .0443 | 5.0265 | .0131 | 175 | 13.2287 | .0377 | 5.5934 | .0106 |
| 128 | 11.3137 | .0441 | 5.0396 | .0131 | 176 | 13.2664 | .0376 | 5.6040 | .0106 |
| 129 | 11.3578 | .0439 | 5.0527 | .0130 | 177 | 13.3041 | .0375 | 5.6146 | .0106 |
| 130 | 11.4017 | .0438 | 5.0657 | .0130 | 178 | 13.3416 | .0374 | 5.6252 | .0105 |
| 131 | 11.4455 | .0436 | 5.0787 | .0129 | 179 | 13.3790 | .0373 | 5.6357 | .0105 |
| 132 | 11.4891 | .0434 | 5.0916 | .0128 | 180 | 13.4164 | .0372 | 5.6462 | .0104 |
| 133 | 11.5325 | .0433 | 5.1044 | .0128 | 181 | 13.4536 | .0371 | 5.6566 | .0104 |
| 134 | 11.5758 | .0431 | 5.1172 | .0127 | 182 | 13.4907 | .0370 | 5.6670 | .0104 |
| 135 | 11.6189 | .0430 | 5.1299 | .0126 | 183 | 13.5277 | .0369 | 5.6774 | .0103 |
| 136 | 11.6619 | .0428 | 5.1425 | .0126 | 184 | 13.5646 | .0368 | 5.6877 | .0103 |
| 137 | 11.7046 | | 5.1551 | | 185 | 13.6014 | | 5.6980 | |

| No. | Sqr. Rta. | Diff. | C. Rta. | Diff. | No. | Sqr. Rta. | Diff. | C. Rta. | Diff. |
|-----|-----------|-------|---------|-------|-----|-----------|-------|---------|-------|
| 185 | 13.6014 | | 5.6980 | | 233 | 15.2643 | | 6.1534 | |
| 186 | 13.6381 | .0367 | 5.7082 | .0102 | 234 | 15.2970 | .0327 | 6.1622 | .0088 |
| 187 | 13.6747 | .0366 | 5.7184 | .0102 | 235 | 15.3297 | .0327 | 6.1710 | .0088 |
| 188 | 13.7113 | .0365 | 5.7286 | .0102 | 236 | 15.3622 | .0325 | 6.1797 | .0087 |
| 189 | 13.7477 | .0364 | 5.7387 | .0101 | 237 | 15.3948 | .0326 | 6.1884 | .0087 |
| 190 | 13.7840 | .0363 | 5.7488 | .0101 | 238 | 15.4272 | .0324 | 6.1971 | .0087 |
| 191 | 13.8202 | .0362 | 5.7589 | .0101 | 239 | 15.4596 | .0324 | 6.2058 | .0086 |
| 192 | 13.8564 | .0361 | 5.7689 | .0100 | 240 | 15.4919 | .0323 | 6.2144 | .0086 |
| 193 | 13.8924 | .0360 | 5.7789 | .0100 | 241 | 15.5241 | .0322 | 6.2230 | .0086 |
| 194 | 13.9283 | .0359 | 5.7889 | .0100 | 242 | 15.5563 | .0322 | 6.2316 | .0086 |
| 195 | 13.9642 | .0358 | 5.7988 | .0099 | 243 | 15.5884 | .0321 | 6.2402 | .0086 |
| 196 | 14.0000 | .0357 | 5.8087 | .0099 | 244 | 15.6204 | .0320 | 6.2487 | .0085 |
| 197 | 14.0356 | .0356 | 5.8186 | .0098 | 245 | 15.6524 | .0320 | 6.2573 | .0085 |
| 198 | 14.0712 | .0355 | 5.8284 | .0098 | 246 | 15.6843 | .0319 | 6.2658 | .0085 |
| 199 | 14.1067 | .0355 | 5.8382 | .0098 | 247 | 15.7162 | .0319 | 6.2743 | .0085 |
| 200 | 14.1421 | .0354 | 5.8480 | .0097 | 248 | 15.7480 | .0318 | 6.2827 | .0084 |
| 201 | 14.1774 | .0353 | 5.8577 | .0097 | 249 | 15.7797 | .0317 | 6.2911 | .0084 |
| 202 | 14.2126 | .0352 | 5.8674 | .0097 | 250 | 15.8113 | .0316 | 6.2996 | .0083 |
| 203 | 14.2478 | .0351 | 5.8771 | .0096 | 251 | 15.8429 | .0316 | 6.3079 | .0083 |
| 204 | 14.2828 | .0350 | 5.8867 | .0096 | 252 | 15.8745 | .0316 | 6.3163 | .0084 |
| 205 | 14.3178 | .0349 | 5.8963 | .0096 | 253 | 15.9059 | .0314 | 6.3247 | .0083 |
| 206 | 14.3527 | .0348 | 5.9059 | .0095 | 254 | 15.9373 | .0314 | 6.3330 | .0083 |
| 207 | 14.3874 | .0347 | 5.9154 | .0095 | 255 | 15.9687 | .0313 | 6.3413 | .0083 |
| 208 | 14.4222 | .0346 | 5.9249 | .0095 | 256 | 16.0000 | .0312 | 6.3496 | .0082 |
| 209 | 14.4568 | .0345 | 5.9344 | .0095 | 257 | 16.0312 | .0311 | 6.3578 | .0082 |
| 210 | 14.4913 | .0345 | 5.9439 | .0094 | 258 | 16.0623 | .0311 | 6.3660 | .0083 |
| 211 | 14.5258 | .0344 | 5.9533 | .0094 | 259 | 16.0934 | .0311 | 6.3743 | .0082 |
| 212 | 14.5602 | .0343 | 5.9627 | .0093 | 260 | 16.1245 | .0309 | 6.3825 | .0081 |
| 213 | 14.5945 | .0342 | 5.9720 | .0094 | 261 | 16.1554 | .0310 | 6.3906 | .0082 |
| 214 | 14.6287 | .0341 | 5.9814 | .0093 | 262 | 16.1864 | .0308 | 6.3988 | .0081 |
| 215 | 14.6628 | .0341 | 5.9907 | .0093 | 263 | 16.2172 | .0308 | 6.4069 | .0081 |
| 216 | 14.6969 | .0340 | 6.0000 | .0093 | 264 | 16.2480 | .0308 | 6.4150 | .0081 |
| 217 | 14.7309 | .0339 | 6.0092 | .0092 | 265 | 16.2788 | .0308 | 6.4231 | .0081 |
| 218 | 14.7648 | .0338 | 6.0184 | .0092 | 266 | 16.3095 | .0307 | 6.4312 | .0080 |
| 219 | 14.7986 | .0337 | 6.0276 | .0092 | 267 | 16.3401 | .0306 | 6.4392 | .0081 |
| 220 | 14.8323 | .0337 | 6.0368 | .0091 | 268 | 16.3707 | .0306 | 6.4473 | .0080 |
| 221 | 14.8660 | .0336 | 6.0459 | .0091 | 269 | 16.4012 | .0305 | 6.4553 | .0080 |
| 222 | 14.8996 | .0335 | 6.0550 | .0091 | 270 | 16.4316 | .0304 | 6.4633 | .0078 |
| 223 | 14.9331 | .0335 | 6.0641 | .0090 | 271 | 16.4620 | .0304 | 6.4712 | .0080 |
| 224 | 14.9666 | .0334 | 6.0731 | .0091 | 272 | 16.4924 | .0303 | 6.4792 | .0079 |
| 225 | 15.0000 | .0332 | 6.0822 | .0089 | 273 | 16.5227 | .0302 | 6.4871 | .0079 |
| 226 | 15.0332 | .0333 | 6.0911 | .0090 | 274 | 16.5529 | .0302 | 6.4950 | .0079 |
| 227 | 15.0665 | .0331 | 6.1001 | .0090 | 275 | 16.5831 | .0301 | 6.5029 | .0079 |
| 228 | 15.0996 | .0331 | 6.1091 | .0089 | 276 | 16.6132 | .0301 | 6.5108 | .0078 |
| 229 | 15.1327 | .0330 | 6.1180 | .0089 | 277 | 16.6433 | .0300 | 6.5186 | .0079 |
| 230 | 15.1657 | .0329 | 6.1269 | .0088 | 278 | 16.6733 | .0299 | 6.5265 | .0078 |
| 231 | 15.1986 | .0329 | 6.1357 | .0089 | 279 | 16.7032 | .0299 | 6.5343 | .0078 |
| 232 | 15.2315 | .0328 | 6.1446 | .0088 | 280 | 16.7332 | .0298 | 6.5421 | .0078 |
| 233 | 15.2643 | | 6.1534 | | 281 | 16.7630 | | 6.5499 | |

| No. | Sqr. Rta. | Diff. | C. Rta. | Diff. | No. | Sqr. Rta. | Diff. | C. Rta. | Diff. |
|-----|-----------|-------|---------|-------|-----|-----------|-------|---------|-------|
| 281 | 16.7630 | .0298 | 6.5499 | .0077 | 329 | 18.1383 | .0276 | 6.9084 | .0070 |
| 282 | 16.7928 | .0298 | 6.5576 | .0078 | 330 | 18.1659 | .0275 | 6.9104 | .0069 |
| 283 | 16.8226 | .0296 | 6.5654 | .0077 | 331 | 18.1934 | .0274 | 6.9173 | .0070 |
| 284 | 16.8522 | .0297 | 6.5731 | .0077 | 332 | 18.2208 | .0274 | 6.9243 | .0070 |
| 285 | 16.8819 | .0296 | 6.5808 | .0077 | 333 | 18.2482 | .0274 | 6.9313 | .0070 |
| 286 | 16.9115 | .0295 | 6.5885 | .0077 | 334 | 18.2756 | .0274 | 6.9383 | .0068 |
| 287 | 16.9410 | .0295 | 6.5962 | .0076 | 335 | 18.3030 | .0273 | 6.9451 | .0069 |
| 288 | 16.9705 | .0295 | 6.6038 | .0076 | 336 | 18.3303 | .0272 | 6.9520 | .0069 |
| 289 | 17.0000 | .0293 | 6.6114 | .0077 | 337 | 18.3575 | .0272 | 6.9589 | .0069 |
| 290 | 17.0293 | .0294 | 6.6191 | .0076 | 338 | 18.3847 | .0272 | 6.9658 | .0068 |
| 291 | 17.0587 | .0293 | 6.6267 | .0075 | 339 | 18.4119 | .0271 | 6.9726 | .0069 |
| 292 | 17.0880 | .0292 | 6.6342 | .0076 | 340 | 18.4390 | .0271 | 6.9795 | .0068 |
| 293 | 17.1172 | .0292 | 6.6418 | .0075 | 341 | 18.4661 | .0271 | 6.9863 | .0068 |
| 294 | 17.1464 | .0291 | 6.6493 | .0076 | 342 | 18.4932 | .0270 | 6.9931 | .0069 |
| 295 | 17.1755 | .0291 | 6.6569 | .0075 | 343 | 18.5202 | .0270 | 7.0000 | .0067 |
| 296 | 17.2046 | .0290 | 6.6644 | .0075 | 344 | 18.5472 | .0269 | 7.0067 | .0068 |
| 297 | 17.2336 | .0290 | 6.6719 | .0075 | 345 | 18.5741 | .0269 | 7.0135 | .0068 |
| 298 | 17.2626 | .0290 | 6.6794 | .0074 | 346 | 18.6010 | .0269 | 7.0203 | .0068 |
| 299 | 17.2916 | .0289 | 6.6868 | .0075 | 347 | 18.6279 | .0268 | 7.0271 | .0067 |
| 300 | 17.3205 | .0288 | 6.6943 | .0074 | 348 | 18.6547 | .0268 | 7.0338 | .0067 |
| 301 | 17.3493 | .0288 | 6.7017 | .0074 | 349 | 18.6815 | .0267 | 7.0405 | .0067 |
| 302 | 17.3781 | .0287 | 6.7091 | .0074 | 350 | 18.7082 | .0267 | 7.0472 | .0068 |
| 303 | 17.4068 | .0287 | 6.7165 | .0074 | 351 | 18.7349 | .0267 | 7.0540 | .0066 |
| 304 | 17.4355 | .0287 | 6.7239 | .0074 | 352 | 18.7616 | .0266 | 7.0606 | .0067 |
| 305 | 17.4642 | .0286 | 6.7313 | .0073 | 353 | 18.7882 | .0266 | 7.0673 | .0067 |
| 306 | 17.4928 | .0286 | 6.7386 | .0073 | 354 | 18.8148 | .0266 | 7.0740 | .0066 |
| 307 | 17.5214 | .0285 | 6.7459 | .0074 | 355 | 18.8414 | .0265 | 7.0806 | .0067 |
| 308 | 17.5499 | .0284 | 6.7533 | .0073 | 356 | 18.8679 | .0265 | 7.0873 | .0066 |
| 309 | 17.5783 | .0285 | 6.7606 | .0072 | 357 | 18.8944 | .0264 | 7.0939 | .0066 |
| 310 | 17.6068 | .0283 | 6.7678 | .0073 | 358 | 18.9208 | .0264 | 7.1005 | .0066 |
| 311 | 17.6351 | .0284 | 6.7751 | .0073 | 359 | 18.9472 | .0264 | 7.1071 | .0066 |
| 312 | 17.6635 | .0283 | 6.7824 | .0072 | 360 | 18.9736 | .0264 | 7.1137 | .0066 |
| 313 | 17.6918 | .0282 | 6.7896 | .0072 | 361 | 19.0000 | .0263 | 7.1203 | .0066 |
| 314 | 17.7200 | .0282 | 6.7968 | .0072 | 362 | 19.0262 | .0263 | 7.1269 | .0065 |
| 315 | 17.7482 | .0281 | 6.8040 | .0072 | 363 | 19.0525 | .0262 | 7.1334 | .0066 |
| 316 | 17.7763 | .0281 | 6.8112 | .0072 | 364 | 19.0787 | .0262 | 7.1400 | .0065 |
| 317 | 17.8044 | .0281 | 6.8184 | .0072 | 365 | 19.1049 | .0262 | 7.1465 | .0065 |
| 318 | 17.8325 | .0280 | 6.8256 | .0071 | 366 | 19.1311 | .0261 | 7.1530 | .0065 |
| 319 | 17.8605 | .0280 | 6.8327 | .0072 | 367 | 19.1572 | .0261 | 7.1595 | .0065 |
| 320 | 17.8885 | .0279 | 6.8399 | .0071 | 368 | 19.1833 | .0260 | 7.1660 | .0065 |
| 321 | 17.9164 | .0279 | 6.8470 | .0071 | 369 | 19.2093 | .0260 | 7.1725 | .0065 |
| 322 | 17.9443 | .0279 | 6.8541 | .0071 | 370 | 19.2353 | .0260 | 7.1790 | .0065 |
| 323 | 17.9722 | .0278 | 6.8612 | .0070 | 371 | 19.2613 | .0260 | 7.1855 | .0064 |
| 324 | 18.0000 | .0277 | 6.8682 | .0071 | 372 | 19.2873 | .0259 | 7.1919 | .0065 |
| 325 | 18.0277 | .0277 | 6.8753 | .0070 | 373 | 19.3132 | .0258 | 7.1984 | .0064 |
| 326 | 18.0554 | .0277 | 6.8823 | .0071 | 374 | 19.3390 | .0259 | 7.2048 | .0064 |
| 327 | 18.0831 | .0276 | 6.8894 | .0070 | 375 | 19.3649 | .0258 | 7.2112 | .0064 |
| 328 | 18.1107 | .0276 | 6.8964 | .0070 | 376 | 19.3907 | .0257 | 7.2176 | .0064 |
| 329 | 18.1383 | .0276 | 6.9034 | .0070 | 377 | 19.4164 | | 7.2240 | |

| No. | Sqr. Rta. | Diff. | C. Rta. | Diff. | No. | Sqr. Rta. | Diff. | C. Rta. | Diff. |
|-----|-----------|-------|---------|-------|-----|-----------|-------|---------|-------|
| 377 | 19.4164 | .0258 | 7.2240 | .0064 | 425 | 20.6155 | .0242 | 7.5184 | .0059 |
| 378 | 19.4422 | .0257 | 7.2304 | .0063 | 426 | 20.6397 | .0242 | 7.5243 | .0059 |
| 379 | 19.4679 | .0256 | 7.2367 | .0064 | 427 | 20.6639 | .0242 | 7.5302 | .0059 |
| 380 | 19.4935 | .0257 | 7.2431 | .0064 | 428 | 20.6881 | .0242 | 7.5361 | .0058 |
| 381 | 19.5192 | .0256 | 7.2495 | .0063 | 429 | 20.7123 | .0241 | 7.5419 | .0059 |
| 382 | 19.5448 | .0255 | 7.2558 | .0063 | 430 | 20.7364 | .0241 | 7.5478 | .0058 |
| 383 | 19.5703 | .0256 | 7.2621 | .0063 | 431 | 20.7605 | .0241 | 7.5536 | .0059 |
| 384 | 19.5959 | .0255 | 7.2684 | .0063 | 432 | 20.7846 | .0240 | 7.5595 | .0058 |
| 385 | 19.6214 | .0254 | 7.2747 | .0063 | 433 | 20.8086 | .0240 | 7.5653 | .0058 |
| 386 | 19.6468 | .0255 | 7.2810 | .0063 | 434 | 20.8326 | .0240 | 7.5711 | .0058 |
| 387 | 19.6723 | .0254 | 7.2873 | .0063 | 435 | 20.8566 | .0240 | 7.5769 | .0058 |
| 388 | 19.6977 | .0253 | 7.2936 | .0062 | 436 | 20.8806 | .0239 | 7.5827 | .0058 |
| 389 | 19.7230 | .0254 | 7.2998 | .0063 | 437 | 20.9045 | .0239 | 7.5885 | .0058 |
| 390 | 19.7484 | .0253 | 7.3061 | .0062 | 438 | 20.9284 | .0239 | 7.5943 | .0058 |
| 391 | 19.7737 | .0252 | 7.3123 | .0063 | 439 | 20.9523 | .0238 | 7.6001 | .0058 |
| 392 | 19.7989 | .0253 | 7.3186 | .0062 | 440 | 20.9761 | .0239 | 7.6059 | .0057 |
| 393 | 19.8242 | .0252 | 7.3248 | .0062 | 441 | 21.0000 | .0237 | 7.6116 | .0058 |
| 394 | 19.8494 | .0252 | 7.3310 | .0062 | 442 | 21.0237 | .0220 | 7.6174 | .0057 |
| 395 | 19.8746 | .0251 | 7.3372 | .0062 | 443 | 21.0475 | .0256 | 7.6231 | .0057 |
| 396 | 19.8997 | .0251 | 7.3434 | .0061 | 444 | 21.0713 | .0237 | 7.6288 | .0058 |
| 397 | 19.9248 | .0251 | 7.3495 | .0062 | 445 | 21.0950 | .0237 | 7.6346 | .0057 |
| 398 | 19.9499 | .0250 | 7.3557 | .0062 | 446 | 21.1187 | .0236 | 7.6403 | .0057 |
| 399 | 19.9749 | .0251 | 7.3619 | .0061 | 447 | 21.1423 | .0237 | 7.6460 | .0057 |
| 400 | 20.0000 | .0249 | 7.3680 | .0061 | 448 | 21.1660 | .0236 | 7.6517 | .0057 |
| 401 | 20.0249 | .0250 | 7.3741 | .0062 | 449 | 21.1896 | .0236 | 7.6574 | .0056 |
| 402 | 20.0499 | .0249 | 7.3803 | .0061 | 450 | 21.2132 | .0225 | 7.6630 | .0057 |
| 403 | 20.0748 | .0249 | 7.3864 | .0061 | 451 | 21.2367 | .0235 | 7.6687 | .0057 |
| 404 | 20.0997 | .0249 | 7.3925 | .0061 | 452 | 21.2602 | .0235 | 7.6744 | .0056 |
| 405 | 20.1246 | .0248 | 7.3986 | .0061 | 453 | 21.2837 | .0235 | 7.6800 | .0057 |
| 406 | 20.1494 | .0248 | 7.4047 | .0060 | 454 | 21.3072 | .0235 | 7.6857 | .0056 |
| 407 | 20.1742 | .0248 | 7.4107 | .0061 | 455 | 21.3307 | .0234 | 7.6913 | .0057 |
| 408 | 20.1990 | .0247 | 7.4168 | .0061 | 456 | 21.3541 | .0234 | 7.6970 | .0056 |
| 409 | 20.2237 | .0247 | 7.4229 | .0060 | 457 | 21.3775 | .0234 | 7.7026 | .0056 |
| 410 | 20.2484 | .0247 | 7.4289 | .0060 | 458 | 21.4009 | .0233 | 7.7082 | .0056 |
| 411 | 20.2731 | .0246 | 7.4349 | .0061 | 459 | 21.4242 | .0234 | 7.7138 | .0056 |
| 412 | 20.2977 | .0247 | 7.4410 | .0060 | 460 | 21.4476 | .0233 | 7.7194 | .0056 |
| 413 | 20.3224 | .0245 | 7.4470 | .0060 | 461 | 21.4709 | .0232 | 7.7250 | .0056 |
| 414 | 20.3469 | .0246 | 7.4530 | .0060 | 462 | 21.4941 | .0233 | 7.7306 | .0055 |
| 415 | 20.3715 | .0245 | 7.4590 | .0060 | 463 | 21.5174 | .0232 | 7.7361 | .0056 |
| 416 | 20.3960 | .0245 | 7.4650 | .0059 | 464 | 21.5406 | .0232 | 7.7417 | .0056 |
| 417 | 20.4205 | .0245 | 7.4709 | .0060 | 465 | 21.5638 | .0232 | 7.7473 | .0055 |
| 418 | 20.4450 | .0244 | 7.4769 | .0060 | 466 | 21.5870 | .0231 | 7.7528 | .0056 |
| 419 | 20.4694 | .0245 | 7.4829 | .0059 | 467 | 21.6101 | .0232 | 7.7584 | .0055 |
| 420 | 20.4939 | .0243 | 7.4888 | .0060 | 468 | 21.6333 | .0231 | 7.7639 | .0055 |
| 421 | 20.5182 | .0244 | 7.4948 | .0059 | 469 | 21.6564 | .0230 | 7.7694 | .0055 |
| 422 | 20.5426 | .0243 | 7.5007 | .0059 | 470 | 21.6794 | .0231 | 7.7749 | .0055 |
| 423 | 20.5669 | .0243 | 7.5066 | .0059 | 471 | 21.7025 | .0230 | 7.7804 | .0055 |
| 424 | 20.5912 | .0243 | 7.5125 | .0059 | 472 | 21.7255 | .0230 | 7.7859 | .0055 |
| 425 | 20.6155 | | 7.5184 | | 473 | 21.7485 | | 7.7914 | |

| No. | Sqr. Rta. | Diff. | C. Rta. | Diff. | No. | Sqr. Rta. | Diff. | C. Rta. | Diff. |
|-----|-----------|-------|---------|-------|-----|-----------|-------|---------|-------|
| 473 | 21.7485 | .0230 | 7.7914 | .0055 | 521 | 22.8254 | | 8.0466 | |
| 474 | 21.7715 | .0229 | 7.7969 | .0055 | 522 | 22.8473 | .0219 | 8.0517 | .0051 |
| 475 | 21.7944 | .0230 | 7.8024 | .0055 | 523 | 22.8691 | .0218 | 8.0568 | .0051 |
| 476 | 21.8174 | .0229 | 7.8079 | .0055 | 524 | 22.8910 | .0219 | 8.0620 | .0052 |
| 477 | 21.8403 | .0229 | 7.8133 | .0055 | 525 | 22.9128 | .0218 | 8.0671 | .0051 |
| 478 | 21.8632 | .0228 | 7.8188 | .0054 | 526 | 22.9346 | .0218 | 8.0722 | .0051 |
| 479 | 21.8860 | .0229 | 7.8242 | .0055 | 527 | 22.9564 | .0218 | 8.0773 | .0051 |
| 480 | 21.9089 | .0228 | 7.8297 | .0054 | 528 | 22.9782 | .0218 | 8.0824 | .0051 |
| 481 | 21.9317 | .0227 | 7.8351 | .0055 | 529 | 23.0000 | .0218 | 8.0875 | .0051 |
| 482 | 21.9544 | .0228 | 7.8405 | .0054 | 530 | 23.0217 | .0217 | 8.0926 | .0051 |
| 483 | 21.9772 | .0228 | 7.8460 | .0055 | 531 | 23.0434 | .0217 | 8.0977 | .0051 |
| 484 | 22.0000 | .0227 | 7.8514 | .0054 | 532 | 23.0651 | .0217 | 8.1028 | .0051 |
| 485 | 22.0227 | .0227 | 7.8568 | .0054 | 533 | 23.0867 | .0216 | 8.1079 | .0051 |
| 486 | 22.0454 | .0226 | 7.8622 | .0054 | 534 | 23.1084 | .0216 | 8.1129 | .0051 |
| 487 | 22.0680 | .0227 | 7.8676 | .0054 | 535 | 23.1300 | .0216 | 8.1180 | .0050 |
| 488 | 22.0907 | .0226 | 7.8729 | .0053 | 536 | 23.1516 | .0216 | 8.1230 | .0050 |
| 489 | 22.1133 | .0226 | 7.8783 | .0054 | 537 | 23.1732 | .0216 | 8.1281 | .0051 |
| 490 | 22.1359 | .0226 | 7.8827 | .0054 | 538 | 23.1948 | .0216 | 8.1331 | .0051 |
| 491 | 22.1585 | .0225 | 7.8890 | .0053 | 539 | 23.2163 | .0215 | 8.1382 | .0051 |
| 492 | 22.1810 | .0226 | 7.8944 | .0054 | 540 | 23.2379 | .0216 | 8.1432 | .0050 |
| 493 | 22.2036 | .0225 | 7.8997 | .0053 | 541 | 23.2594 | .0215 | 8.1482 | .0050 |
| 494 | 22.2261 | .0224 | 7.9051 | .0054 | 542 | 23.2808 | .0215 | 8.1532 | .0051 |
| 495 | 22.2485 | .0224 | 7.9104 | .0053 | 543 | 23.3023 | .0215 | 8.1583 | .0050 |
| 496 | 22.2710 | .0225 | 7.9157 | .0053 | 544 | 23.3238 | .0215 | 8.1633 | .0050 |
| 497 | 22.2934 | .0224 | 7.9210 | .0053 | 545 | 23.3452 | .0214 | 8.1683 | .0050 |
| 498 | 22.3159 | .0225 | 7.9264 | .0054 | 546 | 23.3666 | .0214 | 8.1733 | .0049 |
| 499 | 22.3383 | .0223 | 7.9317 | .0053 | 547 | 23.3880 | .0213 | 8.1782 | .0050 |
| 500 | 22.3606 | .0224 | 7.9370 | .0052 | 548 | 23.4093 | .0214 | 8.1832 | .0050 |
| 501 | 22.3830 | .0223 | 7.9422 | .0053 | 549 | 23.4307 | .0213 | 8.1882 | .0050 |
| 502 | 22.4053 | .0223 | 7.9475 | .0053 | 550 | 23.4520 | .0213 | 8.1932 | .0049 |
| 503 | 22.4276 | .0223 | 7.9528 | .0053 | 551 | 23.4733 | .0213 | 8.1981 | .0050 |
| 504 | 22.4499 | .0223 | 7.9581 | .0052 | 552 | 23.4946 | .0213 | 8.2031 | .0049 |
| 505 | 22.4722 | .0222 | 7.9633 | .0053 | 553 | 23.5159 | .0213 | 8.2080 | .0050 |
| 506 | 22.4944 | .0222 | 7.9686 | .0052 | 554 | 23.5372 | .0212 | 8.2130 | .0049 |
| 507 | 22.5166 | .0222 | 7.9738 | .0053 | 555 | 23.5584 | .0212 | 8.2179 | .0049 |
| 508 | 22.5388 | .0222 | 7.9791 | .0052 | 556 | 23.5796 | .0212 | 8.2228 | .0050 |
| 509 | 22.5610 | .0221 | 7.9843 | .0052 | 557 | 23.6008 | .0212 | 8.2278 | .0049 |
| 510 | 22.5831 | .0222 | 7.9895 | .0052 | 558 | 23.6220 | .0211 | 8.2327 | .0049 |
| 511 | 22.6053 | .0221 | 7.9947 | .0053 | 559 | 23.6431 | .0212 | 8.2376 | .0049 |
| 512 | 22.6274 | .0221 | 8.0000 | .0052 | 560 | 23.6643 | .0211 | 8.2425 | .0049 |
| 513 | 22.6495 | .0220 | 8.0052 | .0052 | 561 | 23.6854 | .0211 | 8.2474 | .0049 |
| 514 | 22.6715 | .0221 | 8.0104 | .0051 | 562 | 23.7065 | .0211 | 8.2523 | .0049 |
| 515 | 22.6936 | .0220 | 8.0155 | .0052 | 563 | 23.7276 | .0210 | 8.2572 | .0049 |
| 516 | 22.7156 | .0220 | 8.0207 | .0052 | 564 | 23.7486 | .0211 | 8.2621 | .0049 |
| 517 | 22.7376 | .0220 | 8.0259 | .0052 | 565 | 23.7697 | .0210 | 8.2670 | .0049 |
| 518 | 22.7596 | .0219 | 8.0311 | .0051 | 566 | 23.7907 | .0210 | 8.2719 | .0048 |
| 519 | 22.7815 | .0220 | 8.0362 | .0052 | 567 | 23.8117 | .0210 | 8.2767 | .0049 |
| 520 | 22.8035 | .0219 | 8.0414 | .0052 | 568 | 23.8327 | .0210 | 8.2816 | .0048 |
| 521 | 22.8254 | | 8.0466 | | 569 | 23.8537 | | 8.2864 | |

| No. | Sqr. Rta. | Diff. | C. Rta. | Diff. | No. | Sqr. Rta. | Diff. | C. Rta. | Diff. |
|-----|-----------|-------|---------|-------|-----|-----------|-------|---------|-------|
| 569 | 23.8537 | | 8.2864 | | 617 | 24.8394 | | 8.5132 | |
| 570 | 23.8746 | .0209 | 8.2913 | .0049 | 618 | 24.8596 | .0202 | 8.5178 | .0046 |
| 571 | 23.8956 | .0210 | 8.2961 | .0048 | 619 | 24.8797 | .0201 | 8.5224 | .0046 |
| 572 | 23.9165 | .0209 | 8.3010 | .0049 | 620 | 24.8997 | .0200 | 8.5270 | .0046 |
| 573 | 23.9374 | .0209 | 8.3058 | .0048 | 621 | 24.9198 | .0201 | 8.5316 | .0046 |
| 574 | 23.9582 | .0208 | 8.3106 | .0048 | 622 | 24.9399 | .0201 | 8.5361 | .0045 |
| 575 | 23.9791 | .0209 | 8.3155 | .0049 | 623 | 24.9599 | .0200 | 8.5407 | .0046 |
| 576 | 24.0000 | .0209 | 8.3203 | .0048 | 624 | 24.9799 | .0200 | 8.5453 | .0046 |
| 577 | 24.0208 | .0208 | 8.3251 | .0048 | 625 | 25.0010 | .0201 | 8.5498 | .0045 |
| 578 | 24.0416 | .0208 | 8.3299 | .0048 | 626 | 25.0199 | .0199 | 8.5544 | .0046 |
| 579 | 24.0624 | .0208 | 8.3347 | .0048 | 627 | 25.0399 | .0200 | 8.5589 | .0046 |
| 580 | 24.0831 | .0207 | 8.3395 | .0048 | 628 | 25.0599 | .0200 | 8.5635 | .0046 |
| 581 | 24.1039 | .0207 | 8.3443 | .0048 | 629 | 25.0798 | .0199 | 8.5680 | .0045 |
| 582 | 24.1246 | .0207 | 8.3491 | .0048 | 630 | 25.0998 | .0200 | 8.5726 | .0046 |
| 583 | 24.1453 | .0207 | 8.3539 | .0047 | 631 | 25.1197 | .0209 | 8.5771 | .0045 |
| 584 | 24.1660 | .0207 | 8.3586 | .0048 | 632 | 25.1396 | .0199 | 8.5816 | .0045 |
| 585 | 24.1867 | .0207 | 8.3634 | .0048 | 633 | 25.1594 | .0198 | 8.5862 | .0046 |
| 586 | 24.2074 | .0206 | 8.3682 | .0048 | 634 | 25.1793 | .0199 | 8.5907 | .0045 |
| 587 | 24.2280 | .0207 | 8.3729 | .0047 | 635 | 25.1992 | .0199 | 8.5952 | .0045 |
| 588 | 24.2487 | .0206 | 8.3777 | .0048 | 636 | 25.2190 | .0198 | 8.5997 | .0045 |
| 589 | 24.2693 | .0206 | 8.3824 | .0047 | 637 | 25.2388 | .0198 | 8.6042 | .0045 |
| 590 | 24.2899 | .0205 | 8.3872 | .0047 | 638 | 25.2586 | .0198 | 8.6087 | .0045 |
| 591 | 24.3104 | .0205 | 8.3919 | .0047 | 639 | 25.2784 | .0198 | 8.6132 | .0045 |
| 592 | 24.3310 | .0205 | 8.3966 | .0047 | 640 | 25.2982 | .0197 | 8.6177 | .0045 |
| 593 | 24.3515 | .0206 | 8.4013 | .0048 | 641 | 25.3179 | .0198 | 8.6222 | .0045 |
| 594 | 24.3721 | .0205 | 8.4061 | .0047 | 642 | 25.3377 | .0198 | 8.6267 | .0045 |
| 595 | 24.3926 | .0205 | 8.4108 | .0047 | 643 | 25.3574 | .0197 | 8.6311 | .0044 |
| 596 | 24.4131 | .0204 | 8.4155 | .0047 | 644 | 25.3771 | .0197 | 8.6356 | .0045 |
| 597 | 24.4335 | .0205 | 8.4202 | .0047 | 645 | 25.3968 | .0197 | 8.6401 | .0044 |
| 598 | 24.4540 | .0204 | 8.4249 | .0047 | 646 | 25.4165 | .0196 | 8.6445 | .0045 |
| 599 | 24.4744 | .0204 | 8.4296 | .0047 | 647 | 25.4361 | .0197 | 8.6490 | .0044 |
| 600 | 24.4948 | .0205 | 8.4343 | .0047 | 648 | 25.4558 | .0196 | 8.6534 | .0045 |
| 601 | 24.5153 | .0203 | 8.4390 | .0046 | 649 | 25.4754 | .0196 | 8.6579 | .0044 |
| 602 | 24.5356 | .0204 | 8.4436 | .0047 | 650 | 25.4950 | .0197 | 8.6623 | .0045 |
| 603 | 24.5560 | .0204 | 8.4483 | .0047 | 651 | 25.5147 | .0195 | 8.6668 | .0044 |
| 604 | 24.5764 | .0203 | 8.4530 | .0046 | 652 | 25.5342 | .0196 | 8.6712 | .0044 |
| 605 | 24.5967 | .0203 | 8.4576 | .0047 | 653 | 25.5538 | .0196 | 8.6756 | .0045 |
| 606 | 24.6170 | .0203 | 8.4623 | .0047 | 654 | 25.5734 | .0195 | 8.6801 | .0044 |
| 607 | 24.6373 | .0203 | 8.4670 | .0046 | 655 | 25.5929 | .0195 | 8.6845 | .0044 |
| 608 | 24.6576 | .0203 | 8.4716 | .0046 | 656 | 25.6124 | .0196 | 8.6889 | .0044 |
| 609 | 24.6779 | .0202 | 8.4762 | .0047 | 657 | 25.6320 | .0195 | 8.6933 | .0044 |
| 610 | 24.6981 | .0203 | 8.4809 | .0046 | 658 | 25.6515 | .0194 | 8.6977 | .0044 |
| 611 | 24.7184 | .0202 | 8.4855 | .0046 | 659 | 25.6709 | .0195 | 8.7021 | .0044 |
| 612 | 24.7386 | .0202 | 8.4901 | .0046 | 660 | 25.6904 | .0195 | 8.7065 | .0044 |
| 613 | 24.7588 | .0202 | 8.4948 | .0046 | 661 | 25.7099 | .0194 | 8.7109 | .0044 |
| 614 | 24.7790 | .0201 | 8.4994 | .0046 | 662 | 25.7293 | .0194 | 8.7153 | .0044 |
| 615 | 24.7991 | .0202 | 8.5040 | .0046 | 663 | 25.7487 | .0194 | 8.7197 | .0044 |
| 616 | 24.8193 | .0201 | 8.5086 | .0046 | 664 | 25.7681 | .0194 | 8.7241 | .0044 |
| 617 | 24.8394 | | 8.5132 | | 665 | 25.7875 | | 8.7285 | |

| No. | Sqr. Rts. | Diff. | C. Rts. | Diff. | No. | Sqr. Rts. | Diff. | C. Rts. | Diff. |
|-----|-----------|-------|---------|-------|-----|-----------|-------|---------|-------|
| 665 | 25.7875 | .0194 | 8.7285 | .0043 | 713 | 26.7020 | .0187 | 8.9336 | .0042 |
| 666 | 25.8069 | .0194 | 8.7328 | .0044 | 714 | 26.7207 | .0187 | 8.9378 | .0042 |
| 667 | 25.8263 | .0193 | 8.7372 | .0044 | 715 | 26.7394 | .0187 | 8.9420 | .0041 |
| 668 | 25.8456 | .0194 | 8.7416 | .0043 | 716 | 26.7581 | .0187 | 8.9461 | .0042 |
| 669 | 25.8650 | .0193 | 8.7459 | .0044 | 717 | 26.7768 | .0187 | 8.9503 | .0042 |
| 670 | 25.8843 | .0193 | 8.7503 | .0043 | 718 | 26.7955 | .0187 | 8.9545 | .0041 |
| 671 | 25.9036 | .0193 | 8.7546 | .0044 | 719 | 26.8141 | .0187 | 8.9586 | .0042 |
| 672 | 25.9229 | .0193 | 8.7590 | .0043 | 720 | 26.8328 | .0186 | 8.9628 | .0041 |
| 673 | 25.9422 | .0193 | 8.7633 | .0044 | 721 | 26.8514 | .0186 | 8.9669 | .0042 |
| 674 | 25.9615 | .0192 | 8.7677 | .0043 | 722 | 26.8700 | .0186 | 8.9711 | .0041 |
| 675 | 25.9807 | .0193 | 8.7720 | .0043 | 723 | 26.8886 | .0186 | 8.9752 | .0041 |
| 676 | 26.0000 | .0192 | 8.7763 | .0044 | 724 | 26.9072 | .0186 | 8.9793 | .0042 |
| 677 | 26.0192 | .0192 | 8.7807 | .0043 | 725 | 26.9258 | .0185 | 8.9835 | .0041 |
| 678 | 26.0384 | .0192 | 8.7850 | .0043 | 726 | 26.9443 | .0185 | 8.9876 | .0041 |
| 679 | 26.0576 | .0192 | 8.7893 | .0043 | 727 | 26.9629 | .0185 | 8.9917 | .0041 |
| 680 | 26.0768 | .0191 | 8.7936 | .0043 | 728 | 26.9814 | .0185 | 8.9958 | .0042 |
| 681 | 26.0959 | .0192 | 8.7979 | .0043 | 729 | 27.0000 | .0185 | 9.0000 | .0041 |
| 682 | 26.1151 | .0191 | 8.8022 | .0043 | 730 | 27.0185 | .0185 | 9.0041 | .0041 |
| 683 | 26.1342 | .0191 | 8.8065 | .0043 | 731 | 27.0370 | .0184 | 9.0082 | .0041 |
| 684 | 26.1533 | .0192 | 8.8108 | .0043 | 732 | 27.0554 | .0185 | 9.0123 | .0041 |
| 685 | 26.1725 | .0191 | 8.8151 | .0043 | 733 | 27.0739 | .0185 | 9.0164 | .0041 |
| 686 | 26.1916 | .0190 | 8.8194 | .0043 | 734 | 27.0924 | .0184 | 9.0205 | .0041 |
| 687 | 26.2106 | .0191 | 8.8237 | .0043 | 735 | 27.1108 | .0185 | 9.0246 | .0041 |
| 688 | 26.2297 | .0191 | 8.8280 | .0042 | 736 | 27.1293 | .0184 | 9.0287 | .0041 |
| 689 | 26.2488 | .0190 | 8.8322 | .0043 | 737 | 27.1477 | .0184 | 9.0328 | .0040 |
| 690 | 26.2678 | .0190 | 8.8365 | .0043 | 738 | 27.1661 | .0184 | 9.0368 | .0041 |
| 691 | 26.2868 | .0190 | 8.8408 | .0042 | 739 | 27.1845 | .0184 | 9.0409 | .0041 |
| 692 | 26.3058 | .0190 | 8.8450 | .0043 | 740 | 27.2029 | .0184 | 9.0450 | .0041 |
| 693 | 26.3248 | .0190 | 8.8493 | .0042 | 741 | 27.2213 | .0183 | 9.0491 | .0040 |
| 694 | 26.3438 | .0190 | 8.8535 | .0043 | 742 | 27.2396 | .0184 | 9.0531 | .0041 |
| 695 | 26.3628 | .0190 | 8.8578 | .0042 | 743 | 27.2580 | .0183 | 9.0572 | .0041 |
| 696 | 26.3818 | .0189 | 8.8620 | .0043 | 744 | 27.2763 | .0183 | 9.0613 | .0040 |
| 697 | 26.4007 | .0189 | 8.8663 | .0042 | 745 | 27.2946 | .0184 | 9.0653 | .0041 |
| 698 | 26.4196 | .0189 | 8.8705 | .0043 | 746 | 27.3130 | .0183 | 9.0694 | .0040 |
| 699 | 26.4386 | .0189 | 8.8748 | .0042 | 747 | 27.3313 | .0182 | 9.0734 | .0041 |
| 700 | 26.4575 | .0189 | 8.8790 | .0042 | 748 | 27.3495 | .0183 | 9.0775 | .0040 |
| 701 | 26.4764 | .0188 | 8.8832 | .0042 | 749 | 27.3678 | .0183 | 9.0815 | .0041 |
| 702 | 26.4952 | .0188 | 8.8874 | .0043 | 750 | 27.3861 | .0182 | 9.0856 | .0040 |
| 703 | 26.5141 | .0188 | 8.8917 | .0042 | 751 | 27.4043 | .0183 | 9.0896 | .0040 |
| 704 | 26.5329 | .0189 | 8.8959 | .0042 | 752 | 27.4226 | .0182 | 9.0936 | .0041 |
| 705 | 26.5518 | .0188 | 8.9001 | .0042 | 753 | 27.4408 | .0182 | 9.0977 | .0040 |
| 706 | 26.5706 | .0188 | 8.9043 | .0042 | 754 | 27.4590 | .0182 | 9.1017 | .0040 |
| 707 | 26.5894 | .0188 | 8.9085 | .0042 | 755 | 27.4772 | .0182 | 9.1057 | .0040 |
| 708 | 26.6082 | .0188 | 8.9127 | .0042 | 756 | 27.4954 | .0182 | 9.1097 | .0040 |
| 709 | 26.6270 | .0188 | 8.9169 | .0042 | 757 | 27.5136 | .0181 | 9.1137 | .0040 |
| 710 | 26.6458 | .0187 | 8.9211 | .0042 | 758 | 27.5317 | .0182 | 9.1177 | .0041 |
| 711 | 26.6645 | .0188 | 8.9253 | .0041 | 759 | 27.5499 | .0181 | 9.1218 | .0040 |
| 712 | 26.6833 | .0187 | 8.9294 | .0042 | 760 | 27.5680 | .0182 | 9.1258 | .0040 |
| 713 | 26.7020 | | 8.9336 | | 761 | 27.5862 | | 9.1298 | |

| No. | Sqr. Rts. | Diff. | C. Rts. | Diff. | No. | Sqr. Rts. | Diff. | C. Rts. | Diff. |
|-----|-----------|-------|---------|-------|-----|-----------|-------|---------|-------|
| 761 | 27.5862 | .0181 | 9.1298 | .0040 | 809 | 28.4429 | .0175 | 9.3178 | .0038 |
| 762 | 27.6043 | .0181 | 9.1338 | .0039 | 810 | 28.4604 | .0176 | 9.3216 | .0039 |
| 763 | 27.6224 | .0181 | 9.1377 | .0040 | 811 | 28.4780 | .0176 | 9.3255 | .0038 |
| 764 | 27.6405 | .0181 | 9.1417 | .0040 | 812 | 28.4956 | .0175 | 9.3293 | .0038 |
| 765 | 27.6586 | .0181 | 9.1457 | .0040 | 813 | 28.5131 | .0175 | 9.3331 | .0039 |
| 766 | 27.6767 | .0180 | 9.1497 | .0040 | 814 | 28.5306 | .0176 | 9.3370 | .0038 |
| 767 | 27.6947 | .0181 | 9.1537 | .0040 | 815 | 28.5482 | .0175 | 9.3408 | .0038 |
| 768 | 27.7128 | .0180 | 9.1577 | .0039 | 816 | 28.5657 | .0175 | 9.3446 | .0038 |
| 769 | 27.7308 | .0180 | 9.1616 | .0040 | 817 | 28.5832 | .0174 | 9.3484 | .0038 |
| 770 | 27.7488 | .0180 | 9.1656 | .0040 | 818 | 28.6006 | .0175 | 9.3522 | .0038 |
| 771 | 27.7668 | .0180 | 9.1696 | .0039 | 819 | 28.6181 | .0175 | 9.3560 | .0039 |
| 772 | 27.7848 | .0180 | 9.1735 | .0040 | 820 | 28.6356 | .0174 | 9.3599 | .0038 |
| 773 | 27.8028 | .0180 | 9.1775 | .0040 | 821 | 28.6530 | .0175 | 9.3637 | .0038 |
| 774 | 27.8208 | .0180 | 9.1815 | .0039 | 822 | 28.6705 | .0174 | 9.3675 | .0039 |
| 775 | 27.8388 | .0179 | 9.1854 | .0040 | 823 | 28.6879 | .0175 | 9.3713 | .0037 |
| 776 | 27.8567 | .0180 | 9.1894 | .0039 | 824 | 28.7054 | .0174 | 9.3750 | .0038 |
| 777 | 27.8747 | .0179 | 9.1933 | .0039 | 825 | 28.7228 | .0174 | 9.3788 | .0038 |
| 778 | 27.8926 | .0179 | 9.1972 | .0040 | 826 | 28.7402 | .0174 | 9.3826 | .0038 |
| 779 | 27.9105 | .0179 | 9.2012 | .0039 | 827 | 28.7576 | .0173 | 9.3864 | .0038 |
| 780 | 27.9284 | .0179 | 9.2051 | .0039 | 828 | 28.7749 | .0174 | 9.3902 | .0038 |
| 781 | 27.9463 | .0179 | 9.2090 | .0040 | 829 | 28.7923 | .0174 | 9.3940 | .0037 |
| 782 | 27.9642 | .0179 | 9.2130 | .0039 | 830 | 28.8097 | .0173 | 9.3977 | .0038 |
| 783 | 27.9821 | .0179 | 9.2169 | .0039 | 831 | 28.8270 | .0174 | 9.4015 | .0038 |
| 784 | 28.0000 | .0178 | 9.2208 | .0039 | 832 | 28.8444 | .0173 | 9.4053 | .0038 |
| 785 | 28.0178 | .0178 | 9.2247 | .0040 | 833 | 28.8617 | .0173 | 9.4091 | .0037 |
| 786 | 28.0356 | .0179 | 9.2287 | .0039 | 834 | 28.8790 | .0173 | 9.4128 | .0038 |
| 787 | 28.0535 | .0178 | 9.2326 | .0039 | 835 | 28.8963 | .0173 | 9.4166 | .0037 |
| 788 | 28.0713 | .0178 | 9.2365 | .0039 | 836 | 28.9136 | .0173 | 9.4203 | .0038 |
| 789 | 28.0891 | .0178 | 9.2404 | .0039 | 837 | 28.9309 | .0173 | 9.4241 | .0037 |
| 790 | 28.1069 | .0176 | 9.2443 | .0039 | 838 | 28.9482 | .0172 | 9.4278 | .0038 |
| 791 | 28.1247 | .0177 | 9.2482 | .0039 | 839 | 28.9654 | .0173 | 9.4316 | .0037 |
| 792 | 28.1424 | .0178 | 9.2521 | .0039 | 840 | 28.9827 | .0173 | 9.4353 | .0038 |
| 793 | 28.1602 | .0178 | 9.2560 | .0039 | 841 | 29.0000 | .0172 | 9.4391 | .0037 |
| 794 | 28.1780 | .0177 | 9.2599 | .0038 | 842 | 29.0172 | .0172 | 9.4428 | .0038 |
| 795 | 28.1957 | .0177 | 9.2637 | .0039 | 843 | 29.0344 | .0172 | 9.4466 | .0037 |
| 796 | 28.2134 | .0177 | 9.2676 | .0039 | 844 | 29.0516 | .0172 | 9.4503 | .0037 |
| 797 | 28.2311 | .0177 | 9.2715 | .0039 | 845 | 29.0688 | .0172 | 9.4540 | .0037 |
| 798 | 28.2488 | .0177 | 9.2754 | .0039 | 846 | 29.0860 | .0172 | 9.4577 | .0038 |
| 799 | 28.2665 | .0177 | 9.2793 | .0038 | 847 | 29.1032 | .0172 | 9.4615 | .0037 |
| 800 | 28.2842 | .0177 | 9.2831 | .0039 | 848 | 29.1204 | .0172 | 9.4652 | .0037 |
| 801 | 28.3019 | .0177 | 9.2870 | .0039 | 849 | 29.1376 | .0171 | 9.4689 | .0037 |
| 802 | 28.3196 | .0176 | 9.2909 | .0038 | 850 | 29.1547 | .0172 | 9.4726 | .0038 |
| 803 | 28.3372 | .0176 | 9.2947 | .0039 | 851 | 29.1719 | .0171 | 9.4761 | .0040 |
| 804 | 28.3548 | .0177 | 9.2986 | .0038 | 852 | 29.1890 | .0171 | 9.4801 | .0037 |
| 805 | 28.3725 | .0176 | 9.3024 | .0039 | 853 | 29.2061 | .0171 | 9.4838 | .0037 |
| 806 | 28.3901 | .0176 | 9.3063 | .0038 | 854 | 29.2232 | .0171 | 9.4875 | .0037 |
| 807 | 28.4077 | .0176 | 9.3101 | .0039 | 855 | 29.2403 | .0171 | 9.4912 | .0037 |
| 808 | 28.4253 | .0176 | 9.3140 | .0038 | 856 | 29.2574 | .0171 | 9.4949 | .0037 |
| 809 | 28.4429 | .0176 | 9.3178 | | 857 | 29.2745 | | 9.4986 | |

| No. | Sqr. Rts. | Diff. | C. Rts. | Diff. | No. | Sqr. Rts. | Diff. | C. Rts. | Diff. |
|-----|-----------|-------|---------|-------|-----|-----------|-------|---------|-------|
| 857 | 29.2745 | .0171 | 9.4986 | .0037 | 905 | 30.0832 | .0166 | 9.6727 | .0036 |
| 858 | 29.2916 | .0171 | 9.5023 | .0036 | 906 | 30.0998 | .0166 | 9.6763 | .0035 |
| 859 | 29.3087 | .0170 | 9.5059 | .0037 | 907 | 30.1164 | .0166 | 9.6798 | .0036 |
| 860 | 29.3257 | .0171 | 9.5096 | .0037 | 908 | 30.1330 | .0166 | 9.6834 | .0035 |
| 861 | 29.3428 | .0170 | 9.5133 | .0037 | 909 | 30.1496 | .0166 | 9.6869 | .0036 |
| 862 | 29.3598 | .0170 | 9.5170 | .0037 | 910 | 30.1662 | .0165 | 9.6905 | .0036 |
| 863 | 29.3768 | .0170 | 9.5207 | .0037 | 911 | 30.1827 | .0166 | 9.6940 | .0036 |
| 864 | 29.3938 | .0170 | 9.5244 | .0036 | 912 | 30.1993 | .0165 | 9.6976 | .0035 |
| 865 | 29.4108 | .0170 | 9.5280 | .0037 | 913 | 30.2158 | .0166 | 9.7011 | .0035 |
| 866 | 29.4278 | .0170 | 9.5317 | .0037 | 914 | 30.2324 | .0165 | 9.7046 | .0036 |
| 867 | 29.4448 | .0170 | 9.5354 | .0036 | 915 | 30.2489 | .0165 | 9.7082 | .0035 |
| 868 | 29.4618 | .0170 | 9.5390 | .0037 | 916 | 30.2654 | .0166 | 9.7117 | .0036 |
| 869 | 29.4788 | .0169 | 9.5427 | .0037 | 917 | 30.2820 | .0165 | 9.7153 | .0035 |
| 870 | 29.4957 | .0170 | 9.5464 | .0036 | 918 | 30.2985 | .0165 | 9.7188 | .0035 |
| 871 | 29.5127 | .0169 | 9.5500 | .0037 | 919 | 30.3150 | .0165 | 9.7223 | .0035 |
| 872 | 29.5296 | .0169 | 9.5537 | .0036 | 920 | 30.3315 | .0164 | 9.7258 | .0036 |
| 873 | 29.5465 | .0169 | 9.5573 | .0037 | 921 | 30.3479 | .0165 | 9.7294 | .0035 |
| 874 | 29.5634 | .0169 | 9.5610 | .0036 | 922 | 30.3644 | .0165 | 9.7329 | .0035 |
| 875 | 29.5803 | .0169 | 9.5646 | .0036 | 923 | 30.3809 | .0164 | 9.7364 | .0035 |
| 876 | 29.5972 | .0169 | 9.5682 | .0037 | 924 | 30.3973 | .0165 | 9.7399 | .0035 |
| 877 | 29.6141 | .0169 | 9.5719 | .0036 | 925 | 30.4138 | .0164 | 9.7434 | .0035 |
| 878 | 29.6310 | .0169 | 9.5755 | .0037 | 926 | 30.4302 | .0164 | 9.7469 | .0035 |
| 879 | 29.6479 | .0168 | 9.5792 | .0036 | 927 | 30.4466 | .0164 | 9.7504 | .0035 |
| 880 | 29.6647 | .0169 | 9.5828 | .0036 | 928 | 30.4630 | .0165 | 9.7539 | .0036 |
| 881 | 29.6816 | .0168 | 9.5864 | .0036 | 929 | 30.4795 | .0164 | 9.7575 | .0035 |
| 882 | 29.6984 | .0169 | 9.5900 | .0037 | 930 | 30.4959 | .0163 | 9.7610 | .0044 |
| 883 | 29.7153 | .0168 | 9.5937 | .0036 | 931 | 30.5122 | .0164 | 9.7644 | .0035 |
| 884 | 29.7321 | .0168 | 9.5973 | .0036 | 932 | 30.5286 | .0164 | 9.7679 | .0035 |
| 885 | 29.7489 | .0168 | 9.6009 | .0036 | 933 | 30.5450 | .0164 | 9.7714 | .0035 |
| 886 | 29.7657 | .0168 | 9.6045 | .0036 | 934 | 30.5614 | .0163 | 9.7749 | .0035 |
| 887 | 29.7825 | .0168 | 9.6081 | .0036 | 935 | 30.5777 | .0164 | 9.7784 | .0035 |
| 888 | 29.7993 | .0168 | 9.6117 | .0036 | 936 | 30.5941 | .0163 | 9.7829 | .0035 |
| 889 | 29.8161 | .0167 | 9.6153 | .0037 | 937 | 30.6104 | .0163 | 9.7854 | .0035 |
| 890 | 29.8328 | .0168 | 9.6190 | .0036 | 938 | 30.6267 | .0164 | 9.7889 | .0034 |
| 891 | 29.8496 | .0167 | 9.6226 | .0036 | 939 | 30.6431 | .0163 | 9.7923 | .0035 |
| 892 | 29.8663 | .0168 | 9.6262 | .0035 | 940 | 30.6594 | .0163 | 9.7958 | .0035 |
| 893 | 29.8831 | .0167 | 9.6297 | .0036 | 941 | 30.6757 | .0163 | 9.7993 | .0035 |
| 894 | 29.8998 | .0167 | 9.6333 | .0036 | 942 | 30.6920 | .0163 | 9.8028 | .0034 |
| 895 | 29.9165 | .0167 | 9.6369 | .0036 | 943 | 30.7083 | .0162 | 9.8062 | .0035 |
| 896 | 29.9332 | .0167 | 9.6405 | .0036 | 944 | 30.7245 | .0163 | 9.8097 | .0034 |
| 897 | 29.9499 | .0167 | 9.6441 | .0036 | 945 | 30.7408 | .0163 | 9.8131 | .0035 |
| 898 | 29.9666 | .0167 | 9.6477 | .0036 | 946 | 30.7571 | .0162 | 9.8166 | .0035 |
| 899 | 29.9833 | .0167 | 9.6513 | .0035 | 947 | 30.7733 | .0162 | 9.8201 | .0034 |
| 900 | 30.0000 | .0168 | 9.6548 | .0036 | 948 | 30.7896 | .0162 | 9.8235 | .0035 |
| 901 | 30.0166 | .0167 | 9.6584 | .0036 | 949 | 30.8058 | .0162 | 9.8270 | .0034 |
| 902 | 30.0333 | .0166 | 9.6620 | .0036 | 950 | 30.8220 | .0162 | 9.8304 | .0035 |
| 903 | 30.0499 | .0166 | 9.6656 | .0035 | 951 | 30.8382 | .0162 | 9.8339 | .0034 |
| 904 | 30.0665 | .0167 | 9.6691 | .0036 | 952 | 30.8544 | .0162 | 9.8373 | .0035 |
| 905 | 30.0832 | | 9.6727 | | 953 | 30.8706 | | 9.8408 | |

able to
feet

| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |

MATHEMATICAL TABLES.

| Angle | C. Sin. | Diff. | No. | Spr. Sin. | Diff. |
|-------|---------|-------|-----|-----------|-------|
| 177 | 9.4906 | .0037 | 905 | 31.0000 | |
| 178 | 9.5023 | .0036 | 906 | 30.9999 | |
| 179 | 9.5059 | .0037 | 907 | 30.9998 | |
| 180 | 9.5095 | .0037 | 908 | 30.9997 | |
| 181 | 9.5133 | .0037 | 909 | 30.9996 | |
| 182 | 9.5170 | .0037 | 910 | 30.9995 | |
| 183 | 9.5207 | .0037 | 911 | 30.9994 | |
| 184 | 9.5244 | .0036 | 912 | 30.9993 | |
| 185 | 9.5280 | .0037 | 913 | 30.9992 | |
| 186 | 9.5317 | .0037 | 914 | 30.9991 | |
| 187 | 9.5354 | .0037 | 915 | 30.9990 | |
| 188 | 9.5390 | .0037 | 916 | 30.9989 | |
| 189 | 9.5427 | .0037 | 917 | 30.9988 | |
| 190 | 9.5464 | .0037 | 918 | 30.9987 | |
| 191 | 9.5500 | .0037 | 919 | 30.9986 | |
| 192 | 9.5537 | .0037 | 920 | 30.9985 | |
| 193 | 9.5573 | .0037 | 921 | 30.9984 | |
| 194 | 9.5610 | .0037 | 922 | 30.9983 | |
| 195 | 9.5646 | .0037 | 923 | 30.9982 | |
| 196 | 9.5683 | .0037 | 924 | 30.9981 | |
| 197 | 9.5719 | .0037 | 925 | 30.9980 | |
| 198 | 9.5756 | .0037 | 926 | 30.9979 | |
| 199 | 9.5792 | .0037 | 927 | 30.9978 | |
| 200 | 9.5829 | .0037 | 928 | 30.9977 | |
| 201 | 9.5865 | .0037 | 929 | 30.9976 | |
| 202 | 9.5902 | .0037 | 930 | 30.9975 | |
| 203 | 9.5938 | .0037 | 931 | 30.9974 | |
| 204 | 9.5975 | .0037 | 932 | 30.9973 | |
| 205 | 9.6011 | .0037 | 933 | 30.9972 | |
| 206 | 9.6048 | .0037 | 934 | 30.9971 | |
| 207 | 9.6084 | .0037 | 935 | 30.9970 | |
| 208 | 9.6121 | .0037 | 936 | 30.9969 | |
| 209 | 9.6157 | .0037 | 937 | 30.9968 | |
| 210 | 9.6194 | .0037 | 938 | 30.9967 | |
| 211 | 9.6230 | .0037 | 939 | 30.9966 | |
| 212 | 9.6267 | .0037 | 940 | 30.9965 | |
| 213 | 9.6303 | .0037 | 941 | 30.9964 | |
| 214 | 9.6340 | .0037 | 942 | 30.9963 | |
| 215 | 9.6376 | .0037 | 943 | 30.9962 | |
| 216 | 9.6413 | .0037 | 944 | 30.9961 | |
| 217 | 9.6449 | .0037 | 945 | 30.9960 | |
| 218 | 9.6486 | .0037 | 946 | 30.9959 | |
| 219 | 9.6522 | .0037 | 947 | 30.9958 | |
| 220 | 9.6559 | .0037 | 948 | 30.9957 | |
| 221 | 9.6595 | .0037 | 949 | 30.9956 | |
| 222 | 9.6632 | .0037 | 950 | 30.9955 | |

| No. | Sqr. Rta. | Diff. | C. Rta. | Diff. | No. | Sqr. Rta. | Diff. | C. Rta. | Diff. |
|-----|-----------|-------|---------|-------|------|-----------|-------|---------|-------|
| 953 | 30.8706 | .0162 | 9.8408 | .0034 | 977 | 31.2569 | .0160 | 9.9227 | .0034 |
| 954 | 30.8868 | .0162 | 9.8442 | .0034 | 978 | 31.2729 | .0160 | 9.9261 | .0034 |
| 955 | 30.9030 | .0162 | 9.8476 | .0035 | 979 | 31.2889 | .0160 | 9.9295 | .0033 |
| 956 | 30.9192 | .0162 | 9.8511 | .0634 | 980 | 31.3049 | .0160 | 9.9328 | .0034 |
| 957 | 30.9354 | .0161 | 9.8545 | .0034 | 981 | 31.3209 | .0159 | 9.9362 | .0034 |
| 958 | 30.9515 | .0162 | 9.8579 | .0035 | 982 | 31.3368 | .0160 | 9.9396 | .0034 |
| 959 | 30.9677 | .0161 | 9.8614 | .0034 | 983 | 31.3528 | .0159 | 9.9430 | .0033 |
| 960 | 30.9838 | .0162 | 9.8648 | .0034 | 984 | 31.3687 | .0160 | 9.9463 | .0034 |
| 961 | 31.0000 | .0161 | 9.8682 | .0034 | 985 | 31.3847 | .0159 | 9.9497 | .0034 |
| 962 | 31.0161 | .0161 | 9.8716 | .0035 | 986 | 31.4006 | .0159 | 9.9531 | .0033 |
| 963 | 31.0322 | .0161 | 9.8751 | .0034 | 987 | 31.4165 | .0159 | 9.9564 | .0034 |
| 964 | 31.0483 | .0161 | 9.8785 | .0034 | 988 | 31.4324 | .0159 | 9.9598 | .0033 |
| 965 | 31.0644 | .0161 | 9.8819 | .0034 | 989 | 31.4483 | .0159 | 9.9631 | .0034 |
| 966 | 31.0805 | .0161 | 9.8853 | .0034 | 990 | 31.4642 | .0159 | 9.9665 | .0034 |
| 967 | 31.0966 | .0160 | 9.8887 | .0034 | 991 | 31.4801 | .0159 | 9.9699 | .0033 |
| 968 | 31.1126 | .0161 | 9.8921 | .0034 | 992 | 31.4960 | .0159 | 9.9732 | .0034 |
| 969 | 31.1287 | .0161 | 9.8955 | .0034 | 993 | 31.5119 | .0158 | 9.9766 | .0033 |
| 970 | 31.1448 | .0160 | 9.8989 | .0034 | 994 | 31.5277 | .0159 | 9.9799 | .0034 |
| 971 | 31.1608 | .0161 | 9.9023 | .0034 | 995 | 31.5436 | .0158 | 9.9833 | .0033 |
| 972 | 31.1769 | .0160 | 9.9057 | .0034 | 996 | 31.5594 | .0159 | 9.9866 | .0033 |
| 973 | 31.1929 | .0160 | 9.9091 | .0034 | 997 | 31.5753 | .0158 | 9.9899 | .0034 |
| 974 | 31.2089 | .0160 | 9.9125 | .0034 | 998 | 31.5911 | .0158 | 9.9933 | .0033 |
| 975 | 31.2249 | .0160 | 9.9159 | .0034 | 999 | 31.6069 | .0158 | 9.9966 | .0034 |
| 976 | 31.2409 | .0160 | 9.9193 | .0034 | 1000 | 31.6227 | | 10.0000 | |
| 977 | 31.2569 | .0160 | 9.9227 | .0034 | | | | | |

T A B L E
CONTAINING
THE SURFACE AND SOLIDITY OF SPHERES,
The Edge or Dimensions of Equal Cubes,
THE LENGTHS OF EQUAL CYLINDERS,
AND THE
WEIGHT OF EQUAL QUANTITIES OF WATER IN AVOIRDUPOIS
LBS.

| Dia. | Surface. | Solidity. | Cube. | Cylinder. | Water in lbs. |
|-----------------|----------|-----------|--------|-----------|---------------|
| 1 in. | 3.1416 | .5236 | .8060 | .6666 | .0190 |
| $\frac{1}{16}$ | 3.5465 | .6280 | .8563 | .7082 | .0227 |
| $\frac{1}{8}$ | 3.9760 | .7455 | .9067 | .7500 | .0270 |
| $\frac{3}{16}$ | 4.4301 | .8767 | .9571 | .7917 | .0317 |
| $\frac{1}{4}$ | 4.9087 | 1.0226 | 1.0075 | .8333 | .0370 |
| $\frac{5}{16}$ | 5.4117 | 1.1838 | 1.0578 | .8750 | .0428 |
| $\frac{3}{8}$ | 5.9395 | 1.3611 | 1.1082 | .9166 | .0500 |
| $\frac{7}{16}$ | 6.4918 | 1.5553 | 1.1586 | .9583 | .0563 |
| $\frac{1}{2}$ | 7.0686 | 1.7671 | 1.2090 | 1.0000 | .0640 |
| $\frac{9}{16}$ | 7.6699 | 2.0000 | 1.2593 | 1.0416 | .0723 |
| $\frac{5}{8}$ | 8.2957 | 2.2467 | 1.3097 | 1.0833 | .0813 |
| $\frac{11}{16}$ | 8.9461 | 2.5161 | 1.3601 | 1.1349 | .0910 |
| $\frac{3}{4}$ | 9.6211 | 2.8061 | 1.4105 | 1.1666 | .1015 |
| $\frac{13}{16}$ | 10.3206 | 3.1176 | 1.4608 | 1.2083 | .1128 |
| $\frac{7}{8}$ | 11.0446 | 3.4514 | 1.5112 | 1.2500 | .1250 |
| $\frac{15}{16}$ | 11.7932 | 3.8081 | 1.5616 | 1.2916 | .1377 |
| 2 in. | 12.5664 | 4.1888 | 1.6020 | 1.3333 | .1516 |
| $\frac{1}{16}$ | 13.3640 | 4.5938 | 1.6633 | 1.3750 | .1662 |
| $\frac{1}{8}$ | 14.1862 | 5.0243 | 1.7127 | 1.4166 | .1818 |
| $\frac{3}{16}$ | 15.0330 | 5.4807 | 1.7631 | 1.4582 | .1982 |
| $\frac{1}{4}$ | 15.9043 | 5.9640 | 1.8135 | 1.5000 | .2160 |
| $\frac{5}{16}$ | 16.8000 | 6.4749 | 1.8638 | 1.5516 | .2342 |
| $\frac{3}{8}$ | 17.7205 | 7.0143 | 1.9142 | 1.5832 | .2540 |
| $\frac{7}{16}$ | 18.6655 | 7.5828 | 1.9646 | 1.6250 | .2743 |
| $\frac{1}{2}$ | 19.6350 | 8.1812 | 2.0150 | 1.6666 | .2960 |
| $\frac{9}{16}$ | 20.6290 | 8.8103 | 2.0653 | 1.7082 | .3187 |
| $\frac{5}{8}$ | 21.6475 | 9.4708 | 2.1157 | 1.7500 | .3426 |
| $\frac{11}{16}$ | 22.6907 | 10.1634 | 2.1661 | 1.7915 | .3676 |
| $\frac{3}{4}$ | 23.7583 | 10.8892 | 2.2165 | 1.8332 | .3939 |
| $\frac{13}{16}$ | 24.8505 | 11.6485 | 2.2668 | 1.8750 | .4213 |
| $\frac{7}{8}$ | 25.9672 | 12.4426 | 2.3172 | 1.9165 | .4501 |
| $\frac{15}{16}$ | 27.1085 | 13.2718 | 2.3676 | 1.9582 | .4800 |
| 3 in. | 28.2744 | 14.1372 | 2.4180 | 2.0000 | .5114 |
| $\frac{1}{16}$ | 29.4647 | 15.0392 | 2.4683 | 2.0415 | .5440 |
| $\frac{1}{8}$ | 30.6796 | 15.9790 | 2.5187 | 2.0832 | .5780 |
| $\frac{3}{16}$ | 31.9191 | 16.9570 | 2.5691 | 2.1250 | .6133 |
| $\frac{1}{4}$ | 33.1831 | 17.9742 | 2.6195 | 2.1665 | .6401 |
| $\frac{5}{16}$ | 35.3715 | 19.0311 | 2.6698 | 2.2082 | .6884 |
| $\frac{3}{8}$ | 35.7847 | 20.1289 | 2.7202 | 2.2500 | .7281 |
| $\frac{7}{16}$ | 37.1224 | 21.2680 | 2.7706 | 2.2915 | .7693 |
| $\frac{1}{2}$ | 38.4846 | 22.4493 | 2.8210 | 2.3332 | .8120 |
| $\frac{9}{16}$ | 39.8713 | 23.6735 | 2.8713 | 2.3750 | .8561 |
| $\frac{5}{8}$ | 41.2825 | 24.9415 | 2.9217 | 2.4166 | .9021 |
| $\frac{11}{16}$ | 42.7183 | 26.2539 | 2.9712 | 2.4582 | .9496 |
| $\frac{3}{4}$ | 44.1787 | 27.6117 | 3.0225 | 2.5000 | .9987 |
| $\frac{13}{16}$ | 45.6636 | 29.0102 | 3.0728 | 2.5415 | 1.0493 |
| $\frac{7}{8}$ | 47.1730 | 30.4659 | 3.1232 | 2.5832 | 1.1020 |
| $\frac{15}{16}$ | 48.7070 | 31.9640 | 3.1730 | 2.6250 | 1.1561 |

| Dia. | Surface. | Solidity. | Cube. | Cylinder. | Water in lbs. |
|-----------------|----------|-----------|--------|-----------|---------------|
| 4 in. | 50.2656 | 33.5104 | 3.2240 | 2.6665 | 1.1974 |
| $\frac{1}{16}$ | 51.8486 | 35.1058 | 3.2743 | 2.7082 | 1.2698 |
| $\frac{1}{8}$ | 53.4562 | 36.7511 | 3.3247 | 2.7500 | 1.3293 |
| $\frac{3}{16}$ | 55.0884 | 38.4471 | 3.3751 | 2.7915 | 1.3906 |
| $\frac{1}{4}$ | 56.7451 | 40.1944 | 3.4255 | 2.8332 | 1.4538 |
| $\frac{5}{16}$ | 58.4262 | 42.0461 | 3.4758 | 2.8750 | 1.5208 |
| $\frac{3}{8}$ | 60.1321 | 43.8463 | 3.5262 | 2.9165 | 1.5860 |
| $\frac{7}{16}$ | 61.8625 | 45.7524 | 3.5766 | 2.9582 | 1.6550 |
| $\frac{1}{2}$ | 63.6174 | 47.7127 | 3.6270 | 3.0000 | 1.7258 |
| $\frac{9}{16}$ | 65.3968 | 49.7290 | 3.6773 | 3.0415 | 1.7987 |
| $\frac{5}{8}$ | 67.2007 | 51.8006 | 3.7277 | 3.0832 | 1.8736 |
| $\frac{11}{16}$ | 69.0352 | 53.9290 | 3.7781 | 3.1250 | 1.9506 |
| $\frac{3}{4}$ | 70.8823 | 56.1151 | 3.8285 | 3.1665 | 2.0297 |
| $\frac{13}{16}$ | 72.7599 | 58.3595 | 3.8788 | 3.2080 | 2.1109 |
| $\frac{7}{8}$ | 74.6620 | 60.6629 | 3.9292 | 3.2500 | 2.1942 |
| $\frac{15}{16}$ | 76.5887 | 62.9261 | 3.9796 | 3.2913 | 2.2760 |
| 5 in. | 78.5400 | 65.4500 | 4.0300 | 3.3332 | 2.3673 |
| $\frac{1}{16}$ | 80.5157 | 67.9351 | 4.0803 | 3.3750 | 2.4572 |
| $\frac{1}{8}$ | 82.5160 | 70.4824 | 4.1307 | 3.4155 | 2.5453 |
| $\frac{3}{16}$ | 84.5409 | 73.0926 | 4.1811 | 3.4582 | 2.6438 |
| $\frac{1}{4}$ | 86.5903 | 75.7664 | 4.2315 | 3.5000 | 2.7605 |
| $\frac{5}{16}$ | 88.6641 | 78.5077 | 4.2818 | 3.5414 | 2.8396 |
| $\frac{3}{8}$ | 90.7627 | 81.3083 | 4.3322 | 3.5832 | 2.9407 |
| $\frac{7}{16}$ | 92.8858 | 84.1777 | 4.3820 | 3.6250 | 3.0447 |
| $\frac{1}{2}$ | 95.0334 | 87.1139 | 4.4330 | 3.6665 | 3.1509 |
| $\frac{9}{16}$ | 97.2053 | 90.1175 | 4.4633 | 3.7080 | 3.2595 |
| $\frac{5}{8}$ | 99.4021 | 93.1875 | 4.5337 | 3.7500 | 3.3706 |
| $\frac{11}{16}$ | 101.6233 | 96.3304 | 4.5841 | 3.7913 | 3.4843 |
| $\frac{3}{4}$ | 103.8691 | 99.5412 | 4.6345 | 3.8330 | 3.6004 |
| $\frac{13}{16}$ | 106.1394 | 102.8225 | 4.6848 | 3.8750 | 3.7191 |
| $\frac{7}{8}$ | 108.4342 | 106.1754 | 4.7352 | 3.9163 | 3.8404 |
| $\frac{15}{16}$ | 110.7536 | 109.5973 | 4.7856 | 3.9580 | 3.9641 |
| 6 in. | 113.0976 | 113.0976 | 4.8360 | 4.0000 | 4.0907 |
| $\frac{1}{16}$ | 115.4660 | 116.6688 | 4.8863 | 4.0417 | 4.2200 |
| $\frac{1}{8}$ | 117.8590 | 120.3139 | 4.9367 | 4.0833 | 4.3517 |
| $\frac{3}{16}$ | 120.2771 | 124.0374 | 4.9871 | 4.1250 | 4.4874 |
| $\frac{1}{4}$ | 122.7187 | 127.8320 | 5.0375 | 4.1666 | 4.6236 |
| $\frac{5}{16}$ | 125.1852 | 131.7053 | 5.0878 | 4.2083 | 4.7638 |
| $\frac{3}{8}$ | 127.6765 | 135.6563 | 5.1382 | 4.2500 | 4.9067 |
| $\frac{7}{16}$ | 130.1923 | 139.6854 | 5.1886 | 4.2917 | 5.0524 |
| $\frac{1}{2}$ | 132.7326 | 143.7936 | 5.2390 | 4.3332 | 5.2010 |
| $\frac{9}{16}$ | 135.2974 | 147.9815 | 5.2893 | 4.3750 | 5.3525 |
| $\frac{5}{8}$ | 137.8867 | 152.2499 | 5.3377 | 4.4165 | 5.5069 |
| $\frac{11}{16}$ | 140.5006 | 156.5997 | 5.3901 | 4.4583 | 5.6786 |
| $\frac{3}{4}$ | 143.1391 | 161.0315 | 5.4405 | 4.5000 | 5.8245 |
| $\frac{13}{16}$ | 145.8021 | 167.5461 | 5.4908 | 4.5416 | 6.0601 |
| $\frac{7}{8}$ | 148.4896 | 170.1682 | 5.5412 | 4.5832 | 6.1550 |
| $\frac{15}{16}$ | 151.2017 | 174.8270 | 5.5916 | 4.6250 | 6.3235 |

| Dia. | Surface. | Solidity. | Cube. | Cylinder. | Water in lbs. |
|-----------------|----------|-----------|--------|-----------|---------------|
| 7 in. | 153.9384 | 179.5948 | 5.6420 | 4.6665 | 6.4960 |
| $\frac{1}{16}$ | 156.6995 | 184.4484 | 5.6923 | 4.7082 | 6.6725 |
| $\frac{1}{8}$ | 159.4852 | 189.3882 | 5.7427 | 4.7500 | 6.8502 |
| $\frac{3}{16}$ | 162.2955 | 194.1165 | 5.7931 | 4.7915 | 7.0212 |
| $\frac{1}{4}$ | 165.1303 | 199.5325 | 5.8435 | 4.8332 | 7.2171 |
| $\frac{5}{16}$ | 167.9895 | 204.7371 | 5.8938 | 4.8750 | 7.4053 |
| $\frac{3}{8}$ | 170.8735 | 210.0331 | 5.9442 | 4.9166 | 7.5970 |
| $\frac{7}{16}$ | 173.7520 | 215.4172 | 5.9946 | 4.9582 | 7.7916 |
| $\frac{1}{2}$ | 176.7150 | 220.8957 | 6.0450 | 5.0000 | 7.9897 |
| $\frac{9}{16}$ | 179.6725 | 226.7240 | 6.0953 | 5.0415 | 8.2006 |
| $\frac{5}{8}$ | 182.6545 | 232.1235 | 6.1467 | 5.0832 | 8.3960 |
| $\frac{11}{16}$ | 185.6611 | 237.8883 | 6.1961 | 5.1250 | 8.6044 |
| $\frac{3}{4}$ | 188.6923 | 243.7276 | 6.2465 | 5.1665 | 8.8157 |
| $\frac{13}{16}$ | 191.7480 | 249.4720 | 6.2968 | 5.2082 | 9.0234 |
| $\frac{7}{8}$ | 194.8282 | 255.7121 | 6.3472 | 5.2500 | 9.2491 |
| $\frac{15}{16}$ | 197.9330 | 261.9673 | 6.3976 | 5.2913 | 9.4753 |
| 8 in. | 201.0624 | 268.0832 | 6.4480 | 5.3330 | 9.6965 |
| $\frac{1}{16}$ | 204.2162 | 274.4156 | 6.4983 | 5.3750 | 9.9260 |
| $\frac{1}{8}$ | 207.3946 | 280.8469 | 6.5487 | 5.4164 | 10.1583 |
| $\frac{3}{16}$ | 210.5976 | 287.3780 | 6.5991 | 5.4581 | 10.3944 |
| $\frac{1}{4}$ | 213.8251 | 294.0095 | 6.6495 | 5.5000 | 10.6343 |
| $\frac{5}{16}$ | 217.0770 | 300.7422 | 6.6998 | 5.5414 | 10.8778 |
| $\frac{3}{8}$ | 220.3537 | 307.5771 | 6.7502 | 5.5831 | 11.1250 |
| $\frac{7}{16}$ | 223.6549 | 314.5147 | 6.8006 | 5.6250 | 11.3760 |
| $\frac{1}{2}$ | 226.9806 | 321.5555 | 6.8510 | 5.6664 | 11.6306 |
| $\frac{9}{16}$ | 230.3308 | 328.7012 | 6.9013 | 5.7080 | 11.8891 |
| $\frac{5}{8}$ | 233.7055 | 335.9517 | 6.9517 | 5.7500 | 12.1514 |
| $\frac{11}{16}$ | 237.1048 | 343.3079 | 7.0021 | 5.7913 | 12.4170 |
| $\frac{3}{4}$ | 240.5287 | 350.7710 | 7.0525 | 5.8330 | 12.6874 |
| $\frac{13}{16}$ | 243.9771 | 358.3412 | 7.1028 | 5.8750 | 12.9612 |
| $\frac{7}{8}$ | 247.4500 | 366.0199 | 7.1532 | 5.9163 | 13.2390 |
| $\frac{15}{16}$ | 250.9475 | 373.8073 | 7.2036 | 5.9580 | 13.5206 |
| 9 in. | 254.4696 | 381.7017 | 7.2540 | 6.0000 | 13.8062 |
| $\frac{1}{16}$ | 258.0261 | 389.7118 | 7.3043 | 6.0417 | 14.0959 |
| $\frac{1}{8}$ | 261.5872 | 397.8306 | 7.3547 | 6.0833 | 14.3895 |
| $\frac{3}{16}$ | 265.1829 | 406.0613 | 7.4051 | 6.1250 | 14.6872 |
| $\frac{1}{4}$ | 268.8031 | 414.4048 | 7.4555 | 6.1667 | 14.9890 |
| $\frac{5}{16}$ | 272.4477 | 421.2907 | 7.5058 | 6.2083 | 15.2381 |
| $\frac{3}{8}$ | 276.1171 | 431.4361 | 7.5562 | 6.2500 | 15.6050 |
| $\frac{7}{16}$ | 279.8110 | 440.1294 | 7.6066 | 6.2916 | 15.9195 |
| $\frac{1}{2}$ | 283.5294 | 448.9215 | 7.6570 | 6.3333 | 16.2375 |
| $\frac{9}{16}$ | 287.2723 | 457.8500 | 7.7073 | 6.3750 | 16.5604 |
| $\frac{5}{8}$ | 291.0397 | 466.8763 | 7.7557 | 6.4166 | 16.6869 |
| $\frac{11}{16}$ | 294.8310 | 476.0304 | 7.8081 | 6.4582 | 17.2180 |
| $\frac{3}{4}$ | 298.4483 | 485.3035 | 7.8585 | 6.5000 | 17.5534 |
| $\frac{13}{16}$ | 302.4894 | 494.6932 | 7.9088 | 6.5415 | 17.8931 |
| $\frac{7}{8}$ | 306.3550 | 504.2094 | 7.9592 | 6.5832 | 18.2373 |
| $\frac{15}{16}$ | 310.9452 | 513.8436 | 8.0096 | 6.6250 | 18.5857 |

| Dia. | Surface. | Solidity. | Cube. | Cylinder. | Water in lbs. |
|-----------------|----------|-----------|---------|-----------|---------------|
| 10 in. | 314.1600 | 523.6000 | 8.0600 | 6.6666 | 18.6786 |
| $\frac{1}{16}$ | 318.0992 | 533.4789 | 8.1103 | 6.7083 | 19.2960 |
| $\frac{1}{8}$ | 322.0630 | 543.4814 | 8.1607 | 6.7500 | 19.6577 |
| $\frac{3}{16}$ | 326.0514 | 553.6081 | 8.2111 | 6.7916 | 20.0240 |
| $\frac{1}{4}$ | 330.0643 | 563.8603 | 8.2615 | 6.8333 | 20.3948 |
| $\frac{5}{16}$ | 334.1016 | 574.2371 | 8.3118 | 6.8750 | 20.6682 |
| $\frac{3}{8}$ | 338.1637 | 584.7415 | 8.3622 | 6.9166 | 21.1501 |
| $\frac{7}{16}$ | 342.2503 | 595.3677 | 8.4126 | 6.9582 | 21.5344 |
| $\frac{1}{2}$ | 346.3614 | 606.1318 | 8.4630 | 7.0000 | 21.9238 |
| $\frac{9}{16}$ | 350.4970 | 617.0207 | 8.5133 | 7.0416 | 22.3176 |
| $\frac{5}{8}$ | 354.6571 | 628.0387 | 8.5637 | 7.0833 | 22.7162 |
| $\frac{11}{16}$ | 358.8418 | 639.1871 | 8.6141 | 7.1250 | 23.1194 |
| $\frac{3}{4}$ | 363.0511 | 650.4666 | 8.6645 | 7.1666 | 23.5274 |
| $\frac{13}{16}$ | 367.2849 | 661.8580 | 8.7148 | 7.2082 | 23.9394 |
| $\frac{7}{8}$ | 371.5432 | 673.4222 | 8.7652 | 7.2500 | 24.3577 |
| $\frac{15}{16}$ | 375.8261 | 685.0997 | 8.8156 | 7.2915 | 24.7801 |
| 11 in. | 380.1336 | 696.9116 | 8.8660 | 7.3330 | 25.2073 |
| $\frac{1}{16}$ | 384.4655 | 708.9106 | 8.9163 | 7.3750 | 25.6414 |
| $\frac{1}{8}$ | 388.8220 | 720.9409 | 8.9667 | 7.4165 | 26.0764 |
| $\frac{3}{16}$ | 393.2031 | 733.1599 | 9.0171 | 7.4582 | 26.5184 |
| $\frac{1}{4}$ | 397.6087 | 745.5004 | 9.0675 | 7.5000 | 26.9667 |
| $\frac{5}{16}$ | 402.0387 | 758.0104 | 9.1178 | 7.5414 | 27.4162 |
| $\frac{3}{8}$ | 406.4935 | 770.6440 | 9.1682 | 7.5832 | 27.8742 |
| $\frac{7}{16}$ | 410.7728 | 783.5787 | 9.2186 | 7.6250 | 28.3420 |
| $\frac{1}{2}$ | 415.4766 | 796.3301 | 9.2690 | 7.6664 | 28.8033 |
| $\frac{9}{16}$ | 420.0049 | 809.3844 | 9.3193 | 7.7080 | 29.2754 |
| $\frac{5}{8}$ | 424.5576 | 822.5807 | 9.3697 | 7.7500 | 29.7527 |
| $\frac{11}{16}$ | 429.1351 | 835.9695 | 9.4201 | 7.7913 | 30.2370 |
| $\frac{3}{4}$ | 433.7371 | 849.4035 | 9.4705 | 7.8330 | 30.7229 |
| $\frac{13}{16}$ | 438.3636 | 863.0283 | 9.5208 | 7.8750 | 31.2157 |
| $\frac{7}{8}$ | 443.0146 | 876.7999 | 9.5722 | 7.9163 | 31.8883 |
| $\frac{15}{16}$ | 447.6902 | 890.7070 | 9.6216 | 7.9580 | 32.2169 |
| 12 in. | 452.3904 | 904.7808 | 9.6720 | 8.0000 | 32.7259 |
| $\frac{1}{16}$ | 471.4363 | 962.5158 | 9.8735 | 8.1666 | 34.8142 |
| $\frac{1}{8}$ | 490.8750 | 1022.656 | 10.0750 | 8.3332 | 36.9886 |
| $\frac{3}{16}$ | 506.7064 | 1085.251 | 10.2765 | 8.5000 | 39.2535 |
| 13 in. | 530.9304 | 1150.337 | 10.4780 | 8.6666 | 41.6077 |
| $\frac{1}{16}$ | 551.5471 | 1218.000 | 10.6790 | 8.8332 | 44.0551 |
| $\frac{1}{8}$ | 572.5566 | 1288.252 | 10.8810 | 9.0000 | 46.5961 |
| $\frac{3}{16}$ | 593.9587 | 1361.346 | 11.0825 | 9.1665 | 49.2399 |
| 14 in. | 615.7536 | 1436.758 | 11.2840 | 9.3332 | 51.9675 |
| $\frac{1}{16}$ | 637.9411 | 1515.106 | 11.4855 | 9.5000 | 54.8014 |
| $\frac{1}{8}$ | 660.5214 | 1596.260 | 11.6870 | 9.6665 | 57.7367 |
| $\frac{3}{16}$ | 683.4943 | 1680.265 | 11.8885 | 9.8332 | 60.7751 |
| 15 in. | 706.8600 | 1767.150 | 12.0900 | 10.0000 | 64.0178 |
| $\frac{1}{16}$ | 730.6183 | 1856.988 | 12.2915 | 10.1666 | 67.1672 |
| $\frac{1}{8}$ | 754.7694 | 1949.821 | 12.4930 | 10.3332 | 70.5250 |
| $\frac{3}{16}$ | 779.3131 | 2045.697 | 12.6940 | 10.5000 | 73.9929 |
| 16 in. | 804.2496 | 2144.665 | 12.8960 | 10.6666 | 77.5725 |

TABLE OF RECIPROCAL

FOR OBTAINING DECIMAL EQUIVALENTS.

| No. | Recip. | No. | Recip. | No. | Recip. | No. | Recip. | No. | Recip. |
|-----|----------|-----|---------|-----|---------|-----|---------|-----|---------|
| 1 | 1.000000 | 51 | .019607 | 101 | .009900 | 151 | .006623 | 201 | .004975 |
| 2 | .500000 | 52 | .019231 | 102 | .009803 | 152 | .006579 | 202 | .004951 |
| 3 | .333333 | 53 | .018868 | 103 | .009709 | 153 | .006536 | 203 | .004927 |
| 4 | .250000 | 54 | .018519 | 104 | .009616 | 154 | .006494 | 204 | .004901 |
| 5 | .200000 | 55 | .018182 | 105 | .009522 | 155 | .006451 | 205 | .004879 |
| 6 | .166667 | 56 | .017857 | 106 | .009433 | 156 | .006411 | 206 | .004855 |
| 7 | .142857 | 57 | .017543 | 107 | .009345 | 157 | .006370 | 207 | .004831 |
| 8 | .125000 | 58 | .017242 | 108 | .009258 | 158 | .006329 | 208 | .004807 |
| 9 | .111111 | 59 | .016949 | 109 | .009174 | 159 | .006290 | 209 | .004785 |
| 10 | .100000 | 60 | .016667 | 110 | .009091 | 160 | .006250 | 210 | .004762 |
| 11 | .090909 | 61 | .016396 | 111 | .009010 | 161 | .006211 | 211 | .004740 |
| 12 | .083333 | 62 | .016129 | 112 | .008928 | 162 | .006172 | 212 | .004716 |
| 13 | .076923 | 63 | .015873 | 113 | .008850 | 163 | .006135 | 213 | .004695 |
| 14 | .071429 | 64 | .015625 | 114 | .008771 | 164 | .006097 | 214 | .004673 |
| 15 | .066667 | 65 | .015385 | 115 | .008695 | 165 | .006061 | 215 | .004651 |
| 16 | .062500 | 66 | .015151 | 116 | .008620 | 166 | .006025 | 216 | .004630 |
| 17 | .058823 | 67 | .014923 | 117 | .008548 | 167 | .005990 | 217 | .004609 |
| 18 | .055556 | 68 | .014706 | 118 | .008475 | 168 | .005955 | 218 | .004588 |
| 19 | .052632 | 69 | .014492 | 119 | .008405 | 169 | .005921 | 219 | .004566 |
| 20 | .050000 | 70 | .014286 | 120 | .008333 | 170 | .005887 | 220 | .004546 |
| 21 | .047619 | 71 | .014085 | 121 | .008264 | 171 | .005854 | 221 | .004525 |
| 22 | .045455 | 72 | .013889 | 122 | .008196 | 172 | .005821 | 222 | .004505 |
| 23 | .043478 | 73 | .013696 | 123 | .008130 | 173 | .005789 | 223 | .004485 |
| 24 | .041667 | 74 | .013513 | 124 | .008065 | 174 | .005748 | 224 | .004465 |
| 25 | .040000 | 75 | .013333 | 125 | .008000 | 175 | .005715 | 225 | .004444 |
| 26 | .038462 | 76 | .013158 | 126 | .007936 | 176 | .005682 | 226 | .004425 |
| 27 | .037038 | 77 | .012987 | 127 | .007875 | 177 | .005650 | 227 | .004406 |
| 28 | .035715 | 78 | .012820 | 128 | .007812 | 178 | .005618 | 228 | .004386 |
| 29 | .034483 | 79 | .012659 | 129 | .007752 | 179 | .005586 | 229 | .004366 |
| 30 | .033333 | 80 | .012500 | 130 | .007693 | 180 | .005556 | 230 | .004346 |
| 31 | .032258 | 81 | .012346 | 131 | .007634 | 181 | .005524 | 231 | .004329 |
| 32 | .031250 | 82 | .012195 | 132 | .007576 | 182 | .005495 | 232 | .004311 |
| 33 | .030303 | 83 | .012048 | 133 | .007519 | 183 | .005464 | 233 | .004292 |
| 34 | .029412 | 84 | .011904 | 134 | .007463 | 184 | .005434 | 234 | .004273 |
| 35 | .028572 | 85 | .011765 | 135 | .007408 | 185 | .005406 | 235 | .004255 |
| 36 | .027778 | 86 | .011628 | 136 | .007352 | 186 | .005376 | 236 | .004238 |
| 37 | .027028 | 87 | .011494 | 137 | .007298 | 187 | .005347 | 237 | .004220 |
| 38 | .026316 | 88 | .011364 | 138 | .007247 | 188 | .005320 | 238 | .004201 |
| 39 | .025642 | 89 | .011235 | 139 | .007196 | 189 | .005292 | 239 | .004184 |
| 40 | .025000 | 90 | .011111 | 140 | .007143 | 190 | .005264 | 240 | .004167 |
| 41 | .024390 | 91 | .010989 | 141 | .007093 | 191 | .005235 | 241 | .004150 |
| 42 | .023819 | 92 | .010870 | 142 | .007042 | 192 | .005208 | 242 | .004132 |
| 43 | .023255 | 93 | .010753 | 143 | .006994 | 193 | .005182 | 243 | .004116 |
| 44 | .022727 | 94 | .010639 | 144 | .006944 | 194 | .005155 | 244 | .004098 |
| 45 | .022222 | 95 | .010527 | 145 | .006896 | 195 | .005129 | 245 | .004081 |
| 46 | .021739 | 96 | .010417 | 146 | .006850 | 196 | .005102 | 246 | .004065 |
| 47 | .021276 | 97 | .010310 | 147 | .006802 | 197 | .005076 | 247 | .004048 |
| 48 | .020833 | 98 | .010204 | 148 | .006756 | 198 | .005051 | 248 | .004033 |
| 49 | .020408 | 99 | .010101 | 149 | .006712 | 199 | .005026 | 249 | .004016 |
| 50 | .020000 | 100 | .010000 | 150 | .006667 | 200 | .005000 | 250 | .004000 |

The numbers in the table are the denominators of the fraction, hence, multiply the reciprocal of the denominator by the numerator of the fraction, and the product is the decimal equivalent.

Thus, suppose the decimal equivalent of $\frac{7}{16}$ be required,

Reciprocal of 16 = $.0625 \times 7 = .4375$ its decimal equivalent.

T A B L E
CONTAINING
THE WEIGHT OF COLUMNS OF WATER,
EACH ONE FOOT IN LENGTH,
AND OF VARIOUS DIAMETERS,
IN LBS. AVOIRDUPOIS.

| Dia. | Weight. | Dia. | Weight. | Dia. | Weight. |
|---------------|---------|---------------|---------|---------------|----------|
| 3 in. | 3.0672 | 9 in. | 27.5120 | 15 in. | 76.7004 |
| $\frac{1}{2}$ | 3.3288 | $\frac{1}{2}$ | 28.3848 | $\frac{1}{2}$ | 77.9844 |
| $\frac{3}{4}$ | 3.6000 | $\frac{1}{2}$ | 29.1672 | $\frac{1}{2}$ | 79.2792 |
| $\frac{1}{2}$ | 3.8820 | $\frac{1}{2}$ | 29.9604 | $\frac{1}{2}$ | 80.5836 |
| $\frac{1}{2}$ | 4.1748 | $\frac{1}{2}$ | 30.7656 | $\frac{1}{2}$ | 81.9000 |
| $\frac{1}{2}$ | 4.4784 | $\frac{1}{2}$ | 31.5824 | $\frac{1}{2}$ | 83.2260 |
| $\frac{1}{2}$ | 4.7928 | $\frac{1}{2}$ | 32.4060 | $\frac{1}{2}$ | 84.5628 |
| $\frac{1}{2}$ | 5.1180 | $\frac{1}{2}$ | 33.2424 | $\frac{1}{2}$ | 85.9104 |
| 4 in. | 5.4540 | 10 in. | 34.0884 | 16 in. | 87.2688 |
| $\frac{1}{2}$ | 5.7996 | $\frac{1}{2}$ | 34.9464 | $\frac{1}{2}$ | 88.6368 |
| $\frac{1}{2}$ | 6.1572 | $\frac{1}{2}$ | 35.8152 | $\frac{1}{2}$ | 90.0168 |
| $\frac{1}{2}$ | 6.5244 | $\frac{1}{2}$ | 36.6936 | $\frac{1}{2}$ | 91.4176 |
| $\frac{1}{2}$ | 6.9024 | $\frac{1}{2}$ | 37.5828 | $\frac{1}{2}$ | 92.8080 |
| $\frac{1}{2}$ | 7.2912 | $\frac{1}{2}$ | 38.4828 | $\frac{1}{2}$ | 94.2192 |
| $\frac{1}{2}$ | 7.6908 | $\frac{1}{2}$ | 39.3936 | $\frac{1}{2}$ | 95.6412 |
| $\frac{1}{2}$ | 8.1012 | $\frac{1}{2}$ | 40.3152 | $\frac{1}{2}$ | 97.0740 |
| 5 in. | 8.5212 | 11 in. | 41.2476 | 17 in. | 98.5176 |
| $\frac{1}{2}$ | 8.9532 | $\frac{1}{2}$ | 42.1908 | $\frac{1}{2}$ | 99.9720 |
| $\frac{1}{2}$ | 9.3948 | $\frac{1}{2}$ | 43.1436 | $\frac{1}{2}$ | 101.4372 |
| $\frac{1}{2}$ | 9.8484 | $\frac{1}{2}$ | 44.1084 | $\frac{1}{2}$ | 102.9120 |
| $\frac{1}{2}$ | 10.3126 | $\frac{1}{2}$ | 45.0828 | $\frac{1}{2}$ | 104.3968 |
| $\frac{1}{2}$ | 10.7856 | $\frac{1}{2}$ | 46.0680 | $\frac{1}{2}$ | 105.8952 |
| $\frac{1}{2}$ | 11.2704 | $\frac{1}{2}$ | 47.0640 | $\frac{1}{2}$ | 107.4024 |
| $\frac{1}{2}$ | 11.7660 | $\frac{1}{2}$ | 48.0708 | $\frac{1}{2}$ | 108.9204 |
| 6 in. | 12.2712 | 12 in. | 49.0884 | 18 in. | 110.4492 |
| $\frac{1}{2}$ | 12.7884 | $\frac{1}{2}$ | 50.1168 | $\frac{1}{2}$ | 111.9888 |
| $\frac{1}{2}$ | 13.3152 | $\frac{1}{2}$ | 51.1548 | $\frac{1}{2}$ | 113.5392 |
| $\frac{1}{2}$ | 13.8540 | $\frac{1}{2}$ | 52.2048 | $\frac{1}{2}$ | 115.0992 |
| $\frac{1}{2}$ | 14.4024 | $\frac{1}{2}$ | 53.2644 | $\frac{1}{2}$ | 116.6712 |
| $\frac{1}{2}$ | 14.9616 | $\frac{1}{2}$ | 54.3348 | $\frac{1}{2}$ | 118.2528 |
| $\frac{1}{2}$ | 15.5316 | $\frac{1}{2}$ | 55.4760 | $\frac{1}{2}$ | 119.8452 |
| $\frac{1}{2}$ | 16.1124 | $\frac{1}{2}$ | 56.4804 | $\frac{1}{2}$ | 121.4484 |
| 7 in. | 16.7028 | 13 in. | 57.6108 | 19 in. | 123.0624 |
| $\frac{1}{2}$ | 17.3052 | $\frac{1}{2}$ | 58.7244 | $\frac{1}{2}$ | 124.6872 |
| $\frac{1}{2}$ | 17.9172 | $\frac{1}{2}$ | 59.8476 | $\frac{1}{2}$ | 126.3228 |
| $\frac{1}{2}$ | 18.5412 | $\frac{1}{2}$ | 60.9828 | $\frac{1}{2}$ | 127.9680 |
| $\frac{1}{2}$ | 19.1748 | $\frac{1}{2}$ | 62.1276 | $\frac{1}{2}$ | 129.6252 |
| $\frac{1}{2}$ | 19.8192 | $\frac{1}{2}$ | 63.2832 | $\frac{1}{2}$ | 131.5320 |
| $\frac{1}{2}$ | 20.4744 | $\frac{1}{2}$ | 64.4496 | $\frac{1}{2}$ | 132.9696 |
| $\frac{1}{2}$ | 21.1404 | $\frac{1}{2}$ | 65.6268 | $\frac{1}{2}$ | 134.6580 |
| 8 in. | 21.8172 | 14 in. | 66.8148 | 20 in. | 136.3562 |
| $\frac{1}{2}$ | 22.5036 | $\frac{1}{2}$ | 68.0136 | $\frac{1}{2}$ | 138.0672 |
| $\frac{1}{2}$ | 23.2020 | $\frac{1}{2}$ | 69.2220 | $\frac{1}{2}$ | 139.7880 |
| $\frac{1}{2}$ | 23.9100 | $\frac{1}{2}$ | 70.4424 | $\frac{1}{2}$ | 141.5194 |
| $\frac{1}{2}$ | 24.6288 | $\frac{1}{2}$ | 71.6724 | $\frac{1}{2}$ | 143.2608 |
| $\frac{1}{2}$ | 25.3524 | $\frac{1}{2}$ | 72.9120 | $\frac{1}{2}$ | 145.0128 |
| $\frac{1}{2}$ | 26.0988 | $\frac{1}{2}$ | 74.1648 | $\frac{1}{2}$ | 146.7756 |
| $\frac{1}{2}$ | 26.8500 | $\frac{1}{2}$ | 75.4272 | $\frac{1}{2}$ | 148.5492 |

| Dia. | Weight. | Dia. | Weight. | Dia. | Weight. |
|---------------|----------|---------------|----------|---------------|----------|
| 21 in. | 150.2376 | 27 in. | 248.5116 | 33 in. | 371.2344 |
| $\frac{1}{8}$ | 152.1288 | $\frac{1}{8}$ | 250.8180 | $\frac{1}{8}$ | 374.0520 |
| $\frac{1}{4}$ | 153.9348 | $\frac{1}{4}$ | 253.1252 | $\frac{1}{4}$ | 376.8004 |
| $\frac{3}{8}$ | 155.7396 | $\frac{3}{8}$ | 255.4632 | $\frac{3}{8}$ | 379.4592 |
| $\frac{1}{2}$ | 157.5780 | $\frac{1}{2}$ | 257.8008 | $\frac{1}{2}$ | 382.5684 |
| $\frac{5}{8}$ | 159.4152 | $\frac{5}{8}$ | 260.1504 | $\frac{5}{8}$ | 385.4292 |
| $\frac{3}{4}$ | 161.2644 | $\frac{3}{4}$ | 262.5096 | $\frac{3}{4}$ | 388.2996 |
| $\frac{7}{8}$ | 163.1220 | $\frac{7}{8}$ | 264.8796 | $\frac{7}{8}$ | 391.1820 |
| 22 in. | 164.9928 | 28 in. | 267.2616 | 34 in. | 394.0740 |
| $\frac{1}{8}$ | 166.8732 | $\frac{1}{8}$ | 269.6532 | $\frac{1}{8}$ | 396.9768 |
| $\frac{1}{4}$ | 168.7632 | $\frac{1}{4}$ | 272.0544 | $\frac{1}{4}$ | 399.8928 |
| $\frac{3}{8}$ | 170.6652 | $\frac{3}{8}$ | 275.6672 | $\frac{3}{8}$ | 402.8088 |
| $\frac{1}{2}$ | 172.5780 | $\frac{1}{2}$ | 276.8916 | $\frac{1}{2}$ | 405.7500 |
| $\frac{5}{8}$ | 174.5004 | $\frac{5}{8}$ | 279.3252 | $\frac{5}{8}$ | 408.6948 |
| $\frac{3}{4}$ | 176.4336 | $\frac{3}{4}$ | 281.7706 | $\frac{3}{4}$ | 411.4116 |
| $\frac{7}{8}$ | 178.3776 | $\frac{7}{8}$ | 284.2260 | $\frac{7}{8}$ | 414.6180 |
| 23 in. | 180.3324 | 29 in. | 286.6920 | 35 in. | 417.5952 |
| $\frac{1}{8}$ | 182.2980 | $\frac{1}{8}$ | 289.1688 | $\frac{1}{8}$ | 420.5844 |
| $\frac{1}{4}$ | 184.2744 | $\frac{1}{4}$ | 291.6564 | $\frac{1}{4}$ | 423.5832 |
| $\frac{3}{8}$ | 186.2616 | $\frac{3}{8}$ | 294.1548 | $\frac{3}{8}$ | 426.5928 |
| $\frac{1}{2}$ | 188.2584 | $\frac{1}{2}$ | 296.5548 | $\frac{1}{2}$ | 429.6120 |
| $\frac{5}{8}$ | 190.2672 | $\frac{5}{8}$ | 299.1828 | $\frac{5}{8}$ | 432.6432 |
| $\frac{3}{4}$ | 192.2856 | $\frac{3}{4}$ | 301.7124 | $\frac{3}{4}$ | 435.6840 |
| $\frac{7}{8}$ | 194.3184 | $\frac{7}{8}$ | 304.2540 | $\frac{7}{8}$ | 438.7368 |
| 24 in. | 196.3548 | 30 in. | 306.8052 | 36 in. | 441.7992 |
| $\frac{1}{8}$ | 198.4056 | $\frac{1}{8}$ | 309.3672 | $\frac{1}{8}$ | 444.9573 |
| $\frac{1}{4}$ | 200.4672 | $\frac{1}{4}$ | 311.9400 | $\frac{1}{4}$ | 448.1678 |
| $\frac{3}{8}$ | 203.5384 | $\frac{3}{8}$ | 314.5224 | $\frac{3}{8}$ | 460.4105 |
| $\frac{1}{2}$ | 204.6216 | $\frac{1}{2}$ | 317.1168 | 37 in. | 466.6960 |
| $\frac{5}{8}$ | 206.7144 | $\frac{5}{8}$ | 319.7220 | $\frac{1}{8}$ | 473.0240 |
| $\frac{3}{4}$ | 208.8192 | $\frac{3}{4}$ | 322.3368 | $\frac{1}{4}$ | 479.3946 |
| $\frac{7}{8}$ | 210.9336 | $\frac{7}{8}$ | 324.9624 | $\frac{3}{8}$ | 485.8078 |
| 25 in. | 213.0588 | 31 in. | 327.6000 | 38 in. | 492.2637 |
| $\frac{1}{8}$ | 215.1948 | $\frac{1}{8}$ | 330.2472 | $\frac{1}{8}$ | 498.7621 |
| $\frac{1}{4}$ | 217.3416 | $\frac{1}{4}$ | 332.9052 | $\frac{1}{4}$ | 505.3032 |
| $\frac{3}{8}$ | 219.4980 | $\frac{3}{8}$ | 335.5728 | $\frac{3}{8}$ | 511.9979 |
| $\frac{1}{2}$ | 221.6664 | $\frac{1}{2}$ | 338.2524 | 39 in. | 518.4132 |
| $\frac{5}{8}$ | 223.8444 | $\frac{5}{8}$ | 340.9428 | $\frac{1}{8}$ | 525.1821 |
| $\frac{3}{4}$ | 226.0344 | $\frac{3}{4}$ | 343.6428 | $\frac{1}{4}$ | 531.8936 |
| $\frac{7}{8}$ | 228.2340 | $\frac{7}{8}$ | 346.3536 | $\frac{3}{8}$ | 538.6478 |
| 26 in. | 230.4444 | 32 in. | 349.0764 | 40 in. | 545.4445 |
| $\frac{1}{8}$ | 232.6644 | $\frac{1}{8}$ | 351.8088 | $\frac{1}{8}$ | 552.2839 |
| $\frac{1}{4}$ | 234.8576 | $\frac{1}{4}$ | 354.5520 | $\frac{1}{4}$ | 559.1659 |
| $\frac{3}{8}$ | 237.1404 | $\frac{3}{8}$ | 357.3048 | $\frac{3}{8}$ | 566.0904 |
| $\frac{1}{2}$ | 239.3928 | $\frac{1}{2}$ | 360.0696 | 41 in. | 573.0577 |
| $\frac{5}{8}$ | 241.6572 | $\frac{5}{8}$ | 362.8452 | $\frac{1}{2}$ | 587.1199 |
| $\frac{3}{4}$ | 243.9312 | $\frac{3}{4}$ | 365.6304 | 42 in. | 601.3526 |
| $\frac{7}{8}$ | 246.2160 | $\frac{7}{8}$ | 368.4276 | 50 in. | 799.2426 |

The preceding tables are rendered of great utility by means of the following:—

| The weight of Water | being | 1. |
|-----------------------|-------|------|
| _____ Copper | = | 8.8 |
| _____ Brass | = | 8.4 |
| _____ Iron, cast | = | 7.2 |
| _____ Lead | = | 11.3 |
| _____ Zinc | = | 7.2 |
| _____ Gun metal | = | 8.7 |
| _____ Sand | = | 1.5 |
| _____ Coal | = | 1.25 |
| _____ Brick | = | 2.0 |
| _____ Stone | = | 2.5 |
| _____ Timber, average | = | 0.85 |

EXAMPLE.—Suppose it be required to ascertain the weight of a cast iron pipe $26\frac{1}{4}$ inches outside and $23\frac{5}{8}$ inside, the length being $6\frac{1}{2}$ feet.

Opposite $26\frac{1}{4}$ in the table is

$$234,8576 \times 7.2 \times 6.5 = 10991.135$$

And opposite $23\frac{5}{8}$ in the table is

$$192.2856 \times 7.2 \times 6.5 = 8998.966 \text{ subtract}$$

$$1992.169 \text{ lbs. Avs.}$$

And in a similar manner the weight of a column or pipe of another material can easily be obtained.